

**WEYERHAESUER COMPANY – Pine Hill, AL**

**Ambient TRS Study – Phase II**

**April 2002**

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# Ambient TRS Study – Phase II

## Pine Hill, Alabama

April 2002

### Executive Summary

#### Overview

This report documents the results and findings of the second phase of an investigation to identify sources of TRS emissions that have a ground level impact on Weyerhaeuser's Pine Hill, Alabama pulp and paper complex. Phase I of the TRS ambient study focused on establishing baseline conditions prior to implementation and start-up of the MACT related projects. This first phase measurements were conducted on February 6-14, 2001.

The objective of Phase II is to quantify the reductions in TRS emissions resulting from the implementation of the MACT program. Phase II measurements were conducted from November 29 through December 9, 2001.

#### Results

- Implementation of MACT program has removed approximately 80 lb/hr of TRS from entering the wastewater treatment system. This accounts for approximately 11 % of the total ground level TRS emissions from the mill. This TRS would presumably be stripped to the atmosphere at the ASB if left in the system.
- The TRS emission rate changed between Phase I and Phase II at the following major TRS emission sources:

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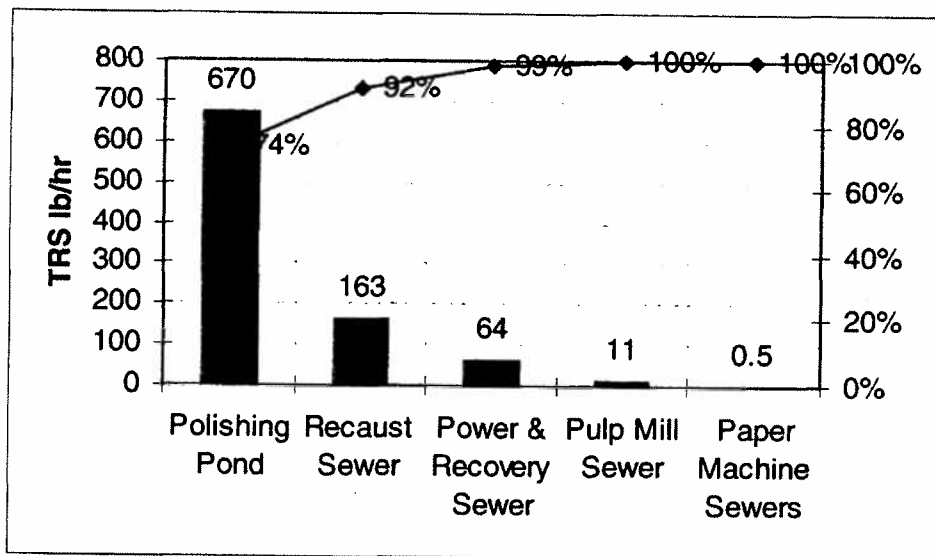
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TRS Emission Source	Type of Sample Taken	TRS Emission Rate( lb/hr)		Percent Change from Phase I to Phase II
		Phase I average (range)	Phase II average (range)	
Polishing Pond	Air	540 (30-2300)	488 (10-2644)	- 10%
ASB	Air	270 (one sample)	not estimated	na
ASB	Effluent	113 (5-359)	195 (102-282)	+ 72%
Polishing Pond Inlet	Air	41 (one sample)	19 (10-33)	- 54%
Pulp Mill	Air	23 (17-32)	not estimated	na
Step Aerator	Air	17 (one sample)	8 (one sample)	- 53%
Primary Clarifier	Air	7 (5-12)	not estimated	na
Primary Clarifier	Effluent	no sample taken	3 (one sample)	na
<b>Total</b>		<b>741</b>	<b>713</b>	<b>- 4%</b>

- The figure below shows the amount of TRS coming from the various sources, including generation in the polishing pond. The polishing pond is the major contributor of TRS.





## ***Conclusions***

1. The MACT program resulted in a modest reduction of 80 lb/hr of TRS in the wastewater system. The mill continues to process over 700 lb/hr through the wastewater system.
2. The two most significant sources of ground level TRS emissions include the following:
  - *Polishing pond*
  - *ASB*
3. The major contributors of TRS to the wastewater treatment system include:
  - Sulfides in the recaust sewer.
  - Sulfide generation in the polishing pond due to anaerobic biological activity.
  - Note: Sulfide generation or oxidation in the ASB was not quantified during this phase of the study.

## ***Recommendations***

1. Develop means of reducing H<sub>2</sub>S generation in the polishing pond. This may include adding aeration capacity at the wastewater treatment system. (Note: Additional control of the H<sub>2</sub>S generation in other areas of the wastewater treatment system, e.g. ASB, primary clarifier, etc. may be required to address a total mill TRS reduction program).
2. Reduce and control the amount of TRS and high pH containing material going to the recaust sewer.
3. Evaluate effect of implementing items 1 and 2 above. This may involve documenting reduced ambient TRS impacts with the ENSR met station, and/or measuring the TRS emission reduction from the major sources using the air dispersion model approach.



## 1.0 Introduction and Background

### 1.1 Overview

The Weyerhaeuser Pine Hill, Alabama pulp and paper facility recently implemented a program to comply with the mandated Maximum Achievable Control Technology (MACT) regulation. The MACT regulation requires the collection and destruction of regulated hazardous air pollutants (HAP).

MACT technology includes collection, separation, and incineration of methanol from various process areas. Total reduced sulfur (TRS) compounds are coincidentally collected, treated, and destroyed along with the methanol. Compliance with the MACT regulation is expected to reduce TRS emissions and lower ambient TRS concentrations throughout the mill.

Two major capital projects were undertaken as part of the MACT program. The following are the two newly installed systems:

- *Condensate steam stripper system* – This system collects foul condensate from selected pulp mill process areas. The condensate is stripped with steam to remove the HAP. The HAP are sent to the noncondensable gas (NCG) thermal oxidizer for destruction.
- *Noncondensable gas thermal oxidizer* – The NCG thermal oxidizer destroys the HAP from the condensate stripper and other NCG streams from the pulp mill.

Because the MACT projects are expected to measurably reduce TRS emissions, the Pine Hill facility commissioned a study to quantify the reduction. Prior to startup of the MACT projects, an initial study was conducted to identify where ground level TRS compound were released in the mill and estimate ground level TRS emission rates prior to implementation of MACT. This first phase included onsite testing during February 6-14, 2001. The results of this study were published in an internal Weyerhaeuser report titled "*Weyerhaeuser Co. – Pine Hill, Al. Ambient TRS Study – February 2001*".

After the startup of the MACT equipment, Phase II of the study was conducted to document the reduction of TRS emissions. Phase II was conducted nine months later, during November 29<sup>th</sup> through December 9<sup>th</sup>, 2001.

This report documents the results of Phase II of the TRS study conducted at the Weyerhaeuser Pine Hill facility.



## 1.2 *Study Objectives*

The primary objective of Phase II is to document the decrease in TRS emissions resulting from the implementation of the MACT program. As part of this documentation, the primary goals include the following:

- Compare the TRS mass emission rates between Phase I and Phase II to quantify the reductions.
- Quantify the reduction in TRS emissions from the major sources.
- Identify key opportunities that will assist in minimizing or eliminating ground level TRS emissions.



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## 2.0 Methodology

### 2.1 Overview

Changes in emissions before and after MACT were assessed by two methods: estimating emissions from ground level sources by back modeling of ambient TRS concentrations measured downwind of pertinent unit operations, and measuring TRS compounds in sewers that have the potential to be stripped during waste water treatment operations.

**Back modeling techniques** - Ambient TRS concentrations at the Pine Hill facility were monitored using a mobile air sampling station. The mobile station was strategically positioned to allow direct TRS measurements from the suspected various TRS emission sources. The mobile station recorded pertinent meteorological data at each sampling location.

The TRS concentration information was used in an EPA approved air dispersion model to calculate the emission rate from each source. The emission rates were then compared between Phase I and Phase II to determine whether a change occurred as a result of the MACT program.

**Wastewater TRS measurements** - Wastewater from selected sewers were collected daily for analysis of TRS components to identify sources of reduced sulfur compounds being released from the effluent treatment systems. The samples were analyzed for: hydrogen sulfide (H<sub>2</sub>S), methyl mercaptan (MeSH), dimethyl sulfide (DMS) and dimethyl disulfide (DMDS). Flow data was obtained for the corresponding streams from the mill and used to calculate mass flow of TRS compounds.

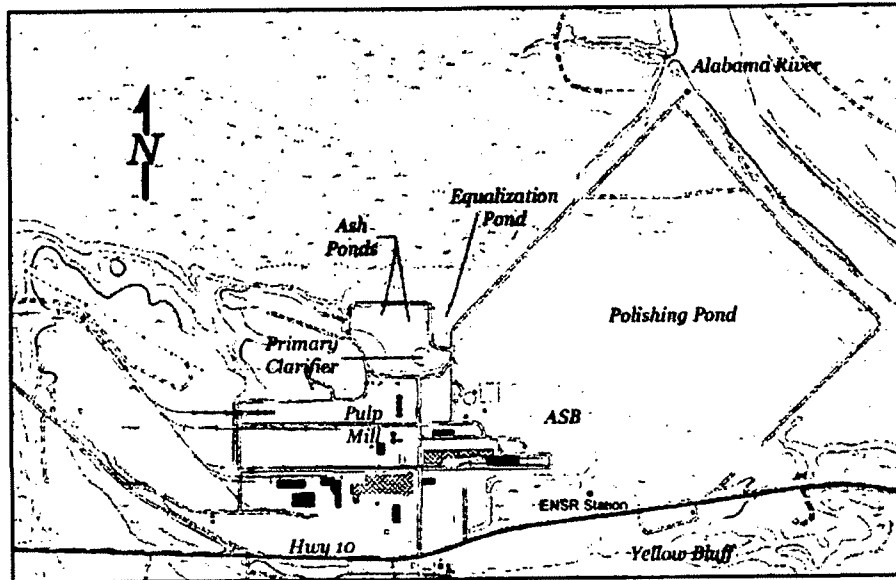
### 2.2 Air Monitoring Methodology

#### 2.2.1 Pine Hill Facility Overview

An overview of the Weyerhaeuser Pine Hill pulp and paper facility is shown in Figure 2-1. In addition, Figure 2-1 also shows the primary areas of interest for the TRS study.



Figure 2-1. Pine Hill Pulp and Paper Facility



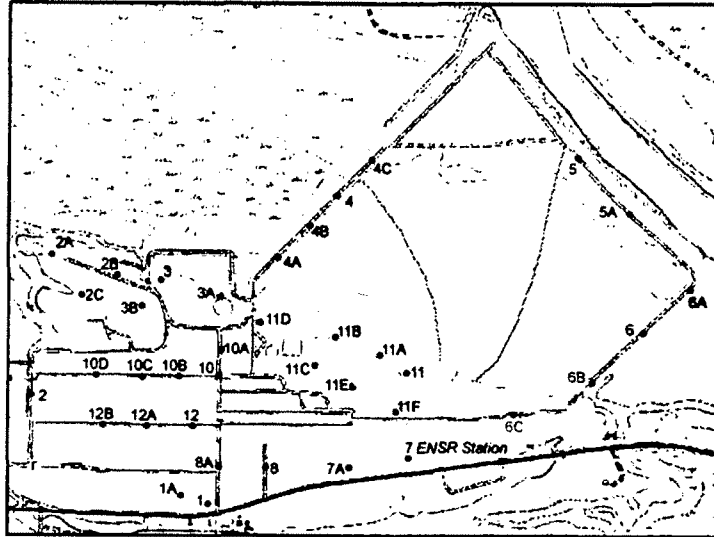
### 2.2.2 Mobile Air Monitoring Station

A mobile air monitoring station was used to collect ambient air data for the TRS study. The mobile station consisted of a two-person vehicle traveling throughout the mill collecting air data at selected sites. The data was collected on a routine schedule, normally in the early morning. The team collected air data at 38 selected locations. Figure 2-2 shows the 38 different sites. The locations of these sites were mapped to +/- 10 feet using a global positioning system (GPS) instrument.





Figure 2-2. Mobile Station Test Site Locations



The 38 sampling sites were chosen to represent a cross-section of the TRS emissions from the entire facility. At each sampling site the following information was collected:

- *Wind direction*
- *Wind speed*
- *H<sub>2</sub>S concentration*
- *Atmospheric stability class information (obtained from ENSR station)*

The 38 locations were sampled nine different times over the eleven-day test period between November 29<sup>th</sup> and December 9<sup>th</sup>, 2001. In addition to the nine routine sampling sets, additional air data was collected during the following periods:

- *During the interior polishing pond liquid sampling test period - air monitoring data was collected along the perimeter of the polishing pond.*
- *During high wind periods - data was collected at multiple inline locations (aligned with the source) to validate the dispersion model parameters.*
- *During favorable wind periods – data was collected along the mill’s fenceline (these locations were typically along the mill’s southern fenceline).*



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## 2.3 *Air Dispersion Model*

TRS mass emission rates can be estimated using the TRS concentration data and an ambient air dispersion model. The EPA approved SCREEN1 Dispersion Model was used to estimate the mass emission rates. The SCREEN1 model normally uses mass emission rates, associated physical information (source area, terrain type) and climatic data inputs (release height, wind speed, solar radiation level) to calculate ground level concentrations. For this study, the ground level concentrations from the mobile monitoring station were used to back-calculate the predicted mass rate from each emission source.

The model's input parameters have been tuned by matching model predictions with measured TRS concentrations at various locations downwind of the source. Also, only TRS data that was obtained during the appropriate climatic stability class were modeled. Stability class categories are used to describe the level of air turbulence. The most widely used category is the Pasquill Stability Classes A, B, C, D, E and F. Class A denotes the most unstable or most turbulent conditions, and Class F denotes the most stable or least turbulent conditions. Climatic conditions with a Class C and D was considered to be a stable atmospheric condition. The criteria for a Class C stability rating includes the following:

- *Stable air flow*, with minimal vertical mixing of the air
- *Steady winds*, with a minimum of around 5 mph
- *Steady wind direction*

Using the appropriate stability class ensures that TRS mixing from other sources is minimized. Therefore, only TRS emissions from the selected source are accounted for in the estimate.

### 2.3.1 **Precision and Accuracy of the Air Dispersion Model Approach**

The use of the SCREEN1 air dispersion model to estimate TRS emission rates from area sources includes several assumptions. For example, the SCREEN1 model is not suited to area sources where changes in the model configuration, such as assumed plume widths, can result in a factor of 2 or 3 difference. However, calibration of the model using multiple point readings will greatly reduce the uncertainty in the modeled results. These readings are taken at different distances from the source along the same downwind line.

Therefore, the results provided in this report should be viewed as relative values, mainly for comparison purposes, and not necessarily absolute numbers. Where possible, results are shown as averages with the ranges of readings.



## 2.4 *Wastewater Testing Methodology*

### 2.4.1 Daily Wastewater Samples

During both phases of the TRS study, grab wastewater samples were taken daily at selected locations throughout the mill. Phase II collected samples at the following twelve locations:

- *Pulp mill sewer*
- *Power & recovery sewer*
- *Recaust area sewer*
- *No. 1 paper machine sewer*
- *No. 2 paper machine sewer*
- *Ash pond overflow*
- *Primary clarifier inlet*
- *Primary clarifier outlet*
- *Inlet to ASB*
- *Discharge from ASB*
- *Discharge of the step aerator*
- *Discharge of the polishing pond*

The daily samples were tested for the following constituents:

- Total sulfide (as H<sub>2</sub>S)
- Methyl mercaptan (MeSH)
- Dimethyl sulfide (DMS )
- Dimethyl disulfide (DMDS)



## 3.0 TRS Source Identification

### 3.1 *Overview*

TRS emission sources were identified using the wind direction data from the mobile air station. By using the wind direction, TRS sources upwind of the mobile station can be readily identified.

### 3.2 *Source Identification Using the Mobile Station*

One of the major benefits of using a mobile station is its ability to directly identify the TRS sources during most atmospheric conditions. This is because the mobile station can place itself in a downwind position next to the suspected TRS source. Therefore, any TRS detected can be attributed to the suspected source if the other atmospheric conditions are suitable, e.g. appropriate wind stability class.

The mobile station was found to work extremely well in identifying the emission sources. Only in cases where wind turbulence around a structure or building became a factor, at low wind speeds, and winds from variable directions did source identification prove more difficult. For example, several sampling sites were located in and around the pulp digester and washing area. Although wind directions and H<sub>2</sub>S readings identified the pulp mill area, specific TRS point sources could not be identified. This was due to the buildings in this area, which would mix and channel the wind. Consequently, precise point source identification around the pulp mill area was not often possible.

### 3.3 *Major TRS Emission Sources*

Sources contributing to in-mill ground level ambient TRS were identified by measuring H<sub>2</sub>S concentrations wind speed and wind direction at selected locations throughout the facility. Mill maps with the raw data can be found in Appendix A and Appendix B.

During Phase II, the sources with the highest downwind TRS concentrations during stable atmospheric conditions are shown in Table 3-1. Note that the concentrations for each source are affected by multiple variables including wind speed, atmospheric stability (vertical mixing and consistency of wind direction), terrain and structures, and distance between the source and measurement point.



Table 3-1 Major Ground Level TRS Emission Sources

<b>Emission Source</b>	<b>Average TRS Concentration (measured as ppb H<sub>2</sub>S)</b>	<b>Median TRS Concentration (measured as ppb H<sub>2</sub>S)</b>	<b>Number of Measurements</b>
<i>Step Aerator</i>	1222	1583	3
<i>Polishing Pond</i>	726	529	66
<i>ASB</i>	376	169	32
<i>Primary Clarifier Area</i>	97	22	8
<i>Ash Pond</i>	33	24	5
<i>Pulp Mill Area</i>	13	13	2
<i>Recaustisizing Area</i>	10	10	2
<i>Equalization Basin Area</i>	7	7	1

Note that these TRS measurements were taken during normal operation. Abnormal conditions, e.g. spills, startups, shutdowns, etc. would likely cause higher readings at the localized affected area.



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## 4.0 TRS Emission Quantification

### 4.1 *Overview*

During Phase II, ambient TRS concentrations were measured from selected sample site locations. The concentration values were used in the EPA approved SCREEN1 air dispersion model to estimate the TRS emission rates from the various emission sources.

Although numerous TRS concentration measurements were taken over the eleven-day Phase II period, only a limited number could be used in the SCREEN1 model. Due to unacceptable climatic conditions, i.e. non-Class C or D atmospheric stability ratings or unfavorable wind directions, most of the measurements could not be used.

### 4.2 *Primary Clarifier TRS Emissions*

Unfavorable climatic conditions existed during the study period such that no valid TRS data could be collected from the primary clarifier area. Unfavorable climatic conditions could include situations such as incorrect wind direction, or inadequate wind stability class rating. Therefore, no TRS concentration data was available to estimate the TRS emission rates with the dispersion model.

### 4.3 *ASB TRS Emissions*

Unfavorable climatic conditions existed during the study period such that no valid TRS data could be collected from the ASB. Therefore, no TRS concentration data was available to estimate the TRS emission rates with the dispersion model.

### 4.4 *Pulp Mill TRS Emissions*

Unfavorable climatic conditions existed during the study period such that no valid TRS data could be collected from the pulp mill area. Therefore, no TRS concentration data was available to estimate the TRS emission rates with the dispersion model.

### 4.5 *Polishing Pond TRS Emissions*

TRS concentration measurements were taken from selected locations around the polishing pond. These measurements were used in the air dispersion model to predict the emission rates.

Similar to Phase I, three sections of the Pond were modeled separately. The modeled areas were designated as A, B and C. These areas are shown in Figure 4-1.



**Figure 4-1. Polishing Pond Modeled Areas**



Area C represents the inlet to the polishing pond. Area B is the northeast corner of the pond. Due to the internal curtain arrangement in the pond the effluent accumulates in this corner prior to entering the main pond area. Area A represents the main polishing pond region. The pond discharges near the lower east end of the pond into the Alabama River.



#### 4.5.1 Polishing Pond - Modeling Results

Table 4-1 shows the air dispersion results for the three polishing pond areas. TRS emissions from Area A ranged from 123 to 2264 lb/hr, with an average of 621 lb/hr. Area C, the polishing pond inlet, ranged 10 to 33 lb/hr and averaged 19 lb/hr. No TRS emission rates were estimated for Area B due to unsuitable climatic data.

**Table 4-1. Polishing Pond Modeling Results**

Date	Time	Sample Location	Wind speed (mph)	Stability Class	Distance from source (ft)	Modeled Width (ft)	Measured H <sub>2</sub> S (ppb)	Estimated H <sub>2</sub> S Emissions (lb/hr)
<b>Area A (East pond area)</b>								
11/30	6:23	6	2.9	D	1660	2500	1438	248
11/30	15:48	6	2.5	D	1660	2500	843	123
11/30	6:26	6-2	2.7	D	1660	2500	1473	234
11/30	6:30	6a	2.9	D	1660	2500	850	147
11/30	15:41	6b	2.9	D	1660	2500	1190	206
11/30	6:18	6d	3.4	D	1660	2500	1027	204
12/8	13:50	6b	6.7	C	1660	2500	2400	1837
12/8	13:55	6e	9.3	C	1660	2500	2467	2644
12/8	13:25	6b	3.4	C	1660	2500	1640	628
<b>Area B (West pond area) No estimates made because Area B could not be isolated during Phase II</b>								
<b>Area C (Inlet area of pond)</b>								
12/9	10:12	11h	11.1	C	390	300	630	33
12/9	10:25	11i	3.8	C	390	300	670	16
12/9	12:23	11a	7.0	C	390	300	490	16
12/9	10:28	11j	4.0	C	390	300	513	10

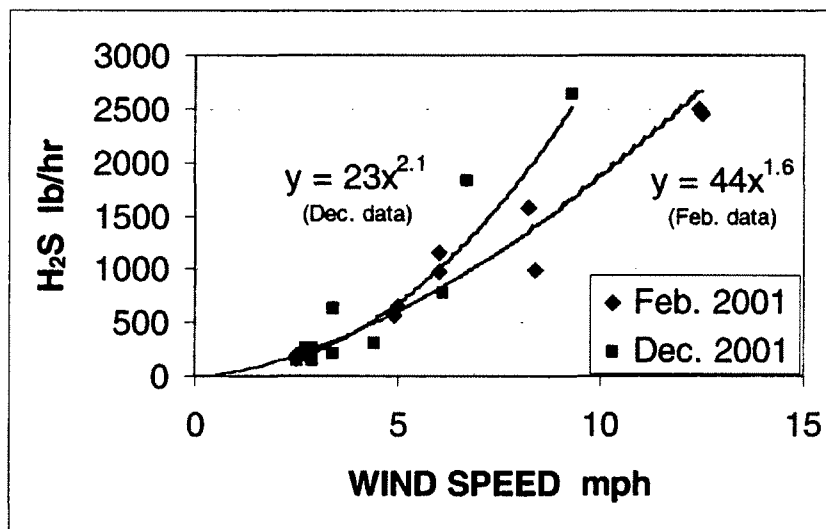




#### 4.5.2 Polishing Pond - TRS Emission Dependence on Wind Speed

As previously discovered in Phase I, TRS emission rates from the polishing pond are significantly affected by wind speed above the pond. This relationship is shown in Figure 4-2.

Figure 4-2. Polishing Pond Emission Rate as a Function of Wind Speed



As Figure 4-2 clearly shows the higher the wind speed the greater the emission rate. It shows that the TRS emission rate exponentially increases as a function of the wind speed.

The Phase II (December 2001) relationship shown in Figure 4-2 was used to estimate the average emission rate from the polishing pond. Note that if only the ambient TRS measurements were used with this relationship, the results would over estimate the emission rates because the ambient measurements were taken only on windy days (>5 mph). Therefore, the results would only represent the results on the right side of the relationship curve.

Therefore, to provide a more representative overall TRS emission rate, the TRS emissions equation ( $y = 23x^{2.1}$ ) was used with the ENSR station wind speed data for the entire month of December. The average TRS emission rate was calculated to be approximately 517 lb/hr. This value is consistent with the 488 lb/hr estimated with the modeling results for the polishing pond.



## 5.0 Wastewater Studies

### 5.1 Overview

Samples of wastewater from various process areas entering and leaving the wastewater treatment system were collected and analyzed for TRS compounds. The purpose of the sampling was to identify sources of TRS entering the wastewater treatment system and points of potential loss from the wastewater treatment system. The methods used, data collected and data reduction are contained in the Appendix.

### 5.2 Process Sewer TRS Constituents

The TRS entering the sewer is made up of mostly sulfides, with smaller amounts of methyl mercaptan, methyl disulfide, and dimethyl disulfide. Table 5-1 shows the composition of TRS in the sewers entering the effluent treatment system.

Table 5-1. TRS Constituents in Sewers

Process Sewer	Average TRS (lb/hr as H <sub>2</sub> S)	H <sub>2</sub> S (%)	MESH (%)	DMS (%)	DMDS (%)
<i>Recaust Sewer<sup>1</sup></i>	163	89	10	1	0
<i>Power and Recovery Sewer</i>	64	66	11	2	21
<i>Pulp Mill Sewer</i>	11	96	2	1	1
<i>#2 Paper Machine Sewer</i>	0.5	42	16	0	42
<i>#1 Paper Machine Sewer</i>	Unknown <sup>2</sup>	na	na	na	na
<b>Average</b>		<b>73</b>	<b>10</b>	<b>1</b>	<b>16</b>

<sup>1</sup> The recaust sewer delivers approximately 575 lb/hr TRS to the ash pond. Most the TRS is oxidized in the ash pond, whereby only 163 lb/hr enters the ASB.

<sup>2</sup> no wastewater flow rate measured for #1 PM sewer.

### 5.3 Major TRS Contributors

As previously shown in Table 3-1, the wastewater treatment system can emit elevated levels of TRS to the atmosphere. This TRS is introduced into the wastewater system by two means. As shown in Table 5-1, substantial amounts of TRS are brought in through the process sewers. The other means of TRS entering the wastewater system is H<sub>2</sub>S generation in the polishing pond. Note that H<sub>2</sub>S generation in the ASB can also occur. However, during this study the H<sub>2</sub>S generation rate from the ASB was not quantified.



Table 5-2 shows the quantity of TRS generated in the polishing pond. This value is added to the estimated amount of TRS emitted to the atmosphere to predict the total H<sub>2</sub>S generation rate in the pond.

**Table 5-2 TRS Generation in the Polishing Pond**

Polishing Pond Location	Average TRS (lb/hr as H <sub>2</sub> S)
<i>Polishing Pond Inlet</i>	32
<i>Polishing Pond Outlet</i>	214
TRS Increase in the Liquid	182
TRS Emitted to the Atmosphere	488
<b>Total TRS Generated</b>	<b>670</b>

H<sub>2</sub>S is generated when sulfate and thiosulfite in the wastewater is reduced to sulfide. The generation rate is believed to be dependent upon several factors such as the oxygen level in the wastewater, BOD concentration, etc.

All of the TRS found in the wastewater treatment system is either introduced by the process sewers or generated in the polishing pond. Figure 5-1 shows the relative amounts of TRS that can be expected from the process sewers and polishing pond generation.

**Figure 5-1. Sources of TRS to the Wastewater Treatment System**

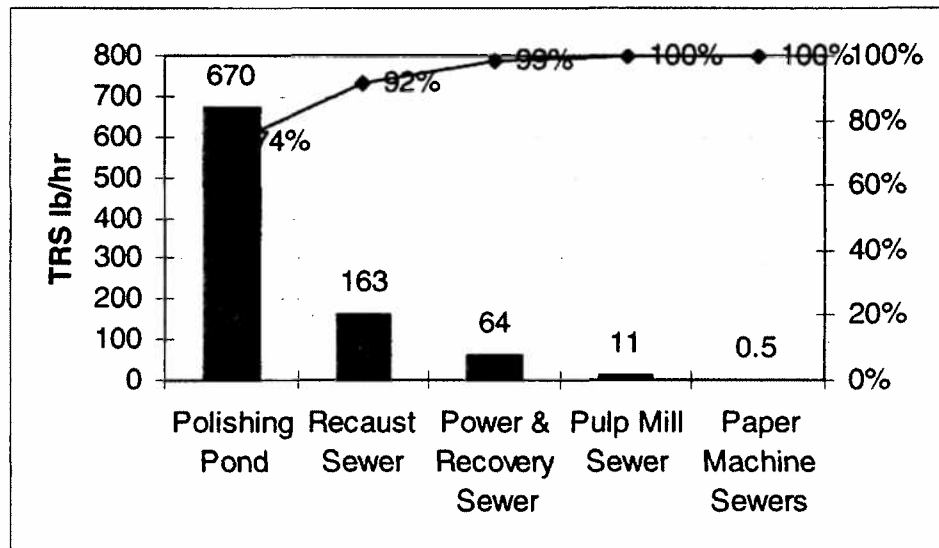




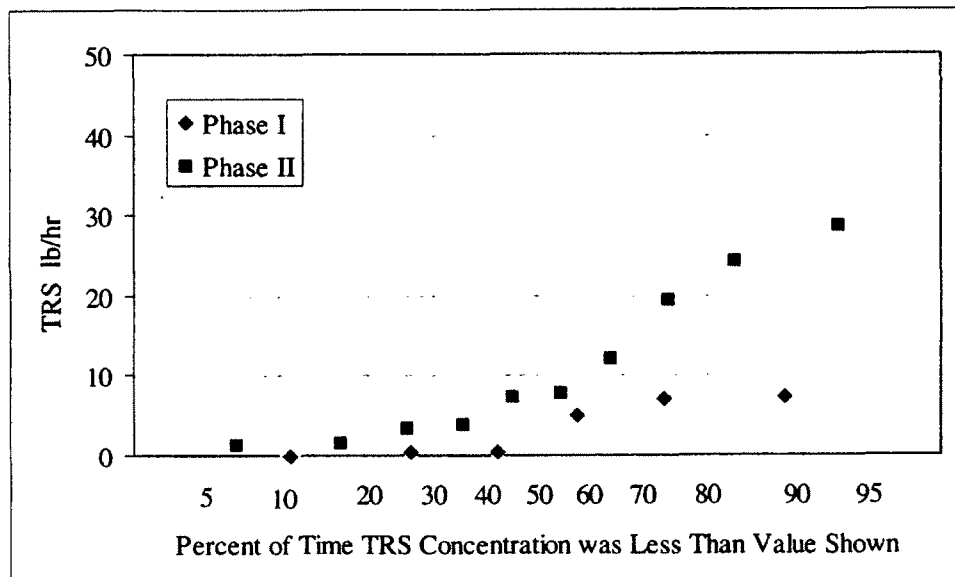
Figure 5-1 shows that 51% of the TRS in the wastewater treatment system is generated in the polishing pond. The recaust sewer contributes another 43%. The remaining 6% of the TRS is attributed to the other process sewers, e.g. power & recovery, pulp mill and the two paper machine sewers.

As previously mentioned, H<sub>2</sub>S generation in the ASB may occur. Operating conditions at the ASB, such as soluble BOD content, pH and DO concentration, will influence the generation rate. However, this study did not quantify the H<sub>2</sub>S generation rate at the ASB.

#### 5.4 Process Sewers - TRS Mass Flows

The TRS mass flow in the pulp mill, power and recovery, and recaust sewers were measured during both Phase I and Phase II. A comparison between the two phases are summarized Figures 5-2 through 5-4 for the different sewers.

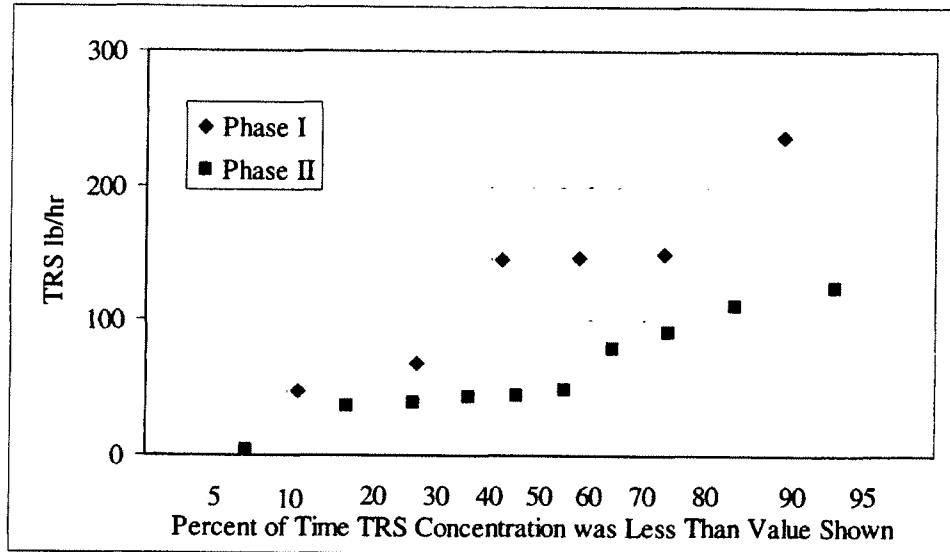
Figure 5-2. Pulp Mill Sewer - TRS Mass Flow



The pulp mill sewer showed an increase in the TRS mass flow from Phase I to Phase II. The data showed that there was an increase of around 5 lb/hr during average operating periods, and as much as 2 to 3 times higher during abnormally high TRS mass flow episodes.



Figure 5-3. Power & Recovery Sewer - TRS Mass Flow

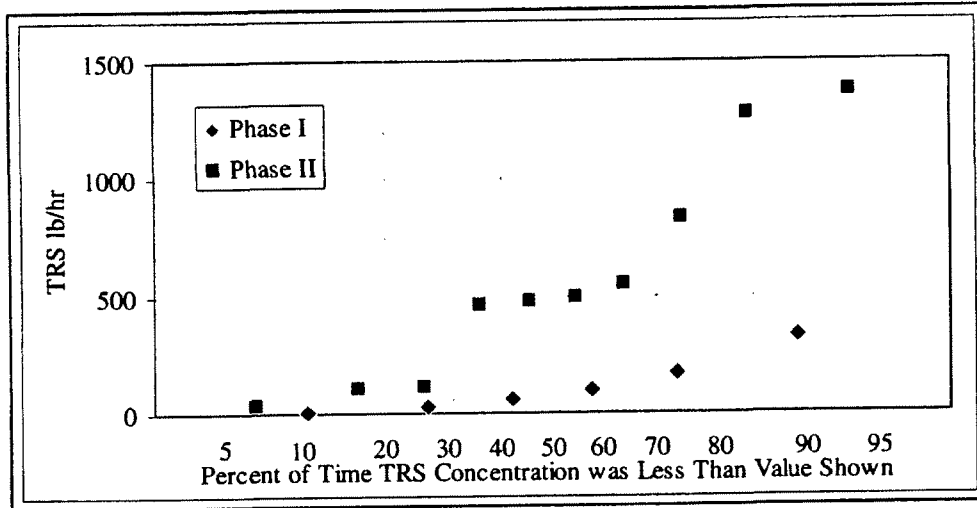


The power and recovery process sewer experienced a decrease in the TRS mass flow from Phase I and Phase II. As Figure 5-3 shows, there is an overall decrease of approximately 70-80 lb/hr of TRS in the sewer.

It is estimated that virtually all of this reduction can be attributed to the installation of the condensate steam stripper system. The stripper system processes selected contaminated condensate streams from the pulp mill area. As will be discussed later, an evaluation of the steam stripper system will show a reduction of approximately 80 lb/hr of TRS. Prior to the steam stripper, this TRS would have entered the power and recovery sewer and eventually entered the wastewater treatment system.



Figure 5-4. Reicast Sewer - TRS Mass Flow



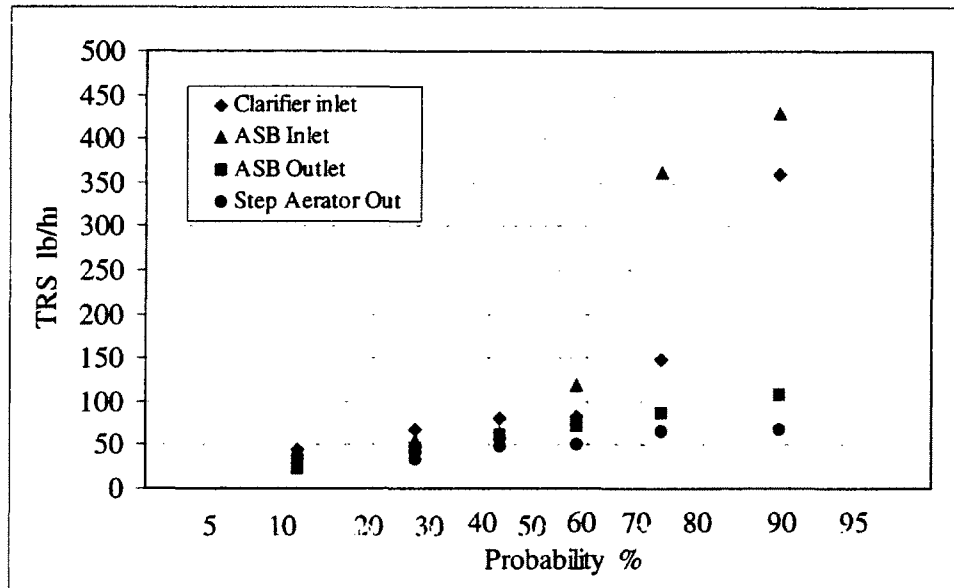
As Figure 5-4 shows, the reicast sewer showed an increase in the TRS mass flow between Phase I to Phase II. The reicast sewer experiences very significant releases of TRS containing material during average operating periods, and exceptionally high releases during high release periods. The reicast sewer is the main contributor of TRS to the effluent treatment system from the process sewers.

### 5.5 Wastewater Treatment System - TRS Mass Flows

The TRS mass flows were also measured at various points in the wastewater treatment system. Figures 5-5 and 5-6 show the TRS mass flow measurements during Phase I and Phase II respectively.



Figure 5-5. Phase I - Wastewater Treatment System TRS Mass Flow



Most of the sulfide compounds entering the ASB will be stripped to the atmosphere by the aeration system. Therefore, the difference in the mass of the sulfide entering and leaving the ASB provides a close approximation of the TRS emissions from the ASB.

However, the sulfide differential across the ASB does not fully account for the  $H_2S$  generation that maybe occurring in the ASB. TRS generation in the ASB is a function of various operational conditions, such as soluble BOD content, pH, and DO concentration. Therefore, the TRS air emissions from the ASB include the TRS introduced by the process sewers and the generated TRS.

However, the TRS generation rate in the ASB was not quantified during this study. Therefore, the estimated TRS emissions from the ASB, using only the TRS water data, may underestimate the air emission rates.



Figure 5-6. Phase II - Wastewater Treatment System TRS Mass Flow

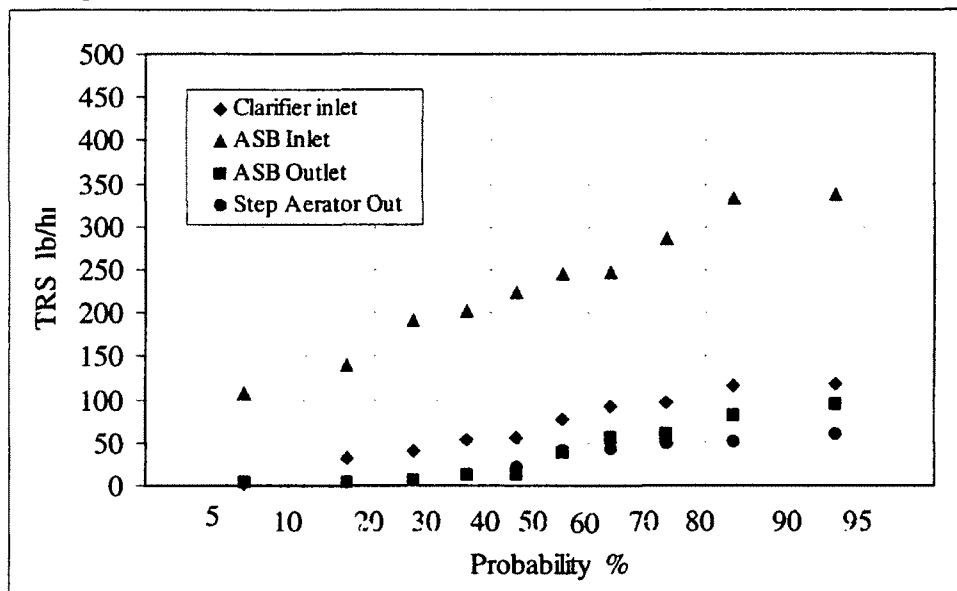


Figure 5-6 also shows large losses of TRS between the ASB inlet and outlet. Similar to Phase I, this reduction is attributed to TRS losses to the atmosphere caused by the aeration system. Therefore, most of the difference in the TRS levels at the ASB inlet versus outlet is attributed to atmospheric losses.

The TRS in the ASB influent increased around 80 lb/hr in the Phase II study. The reason for the higher TRS mass flow is due to the greater amount of TRS entering from the recaust sewer. The TRS mass flow levels from the recaust sewer increased on average over 350 lb/hr during Phase II, as compared to Phase I. Although approximately 72% of this TRS appears to be oxidized in the ash pond, because the total mass flow was larger during Phase II, this resulted in an increase of TRS to the ASB.





## 6.0 TRS Source Reduction and Evaluation

### 6.1 Overview

The implementation of the MACT program at the Pine Hill facility is expected to reduce the overall TRS emissions from the mill. Phase I of the TRS study established baseline ambient TRS mill concentrations prior to the MACT program. The objective of Phase II is to document the TRS reductions after implementation of the MACT program.

Although Phase II measured a reduction in the overall ambient TRS concentration at the Pine Hill facility, only a portion of this could be attributed to the MACT program. As will be discussed in the following sections, there are several other key factors that have a significant impact on the ambient TRS concentrations at the mill.

### 6.2 Phase I and Phase II TRS Comparison

TRS emission rates for Phase I and Phase II were estimated using the air dispersion model approach, and effluent liquid tests. These emissions rates, along with the percent change before and after the MACT program, are shown in Table 6-1.

Table 6-1. Phase I and II TRS Emission Rate Comparison

TRS Emission Source	Type of Sample Taken	TRS Emission Rate (lb/hr)		Percent Change from Phase I to Phase II
		Phase I average (range)	Phase II average (range)	
Polishing Pond	Air	540 (30-2300)	488 (10-2644)	- 10%
ASB	Air	270 (one sample)	not estimated <sup>1</sup>	na
ASB	Effluent	113 (5-359)	195 (102-282)	+ 72%
Polishing Pond Inlet	Air	41 (one sample)	19 (10-33)	- 54%
Pulp Mill	Air	23 (17-32)	not estimated <sup>1</sup>	na
Step Aerator	Air	17 (one sample)	8 (one sample)	- 53%
Primary Clarifier	Air	7 (5-12)	not estimated <sup>1</sup>	na
Primary Clarifier	Effluent	no sample taken	3 (one sample)	na
<b>Total</b>		<b>741</b>	<b>713</b>	<b>- 4%</b>

<sup>1</sup> not estimated – No TRS emission rate was calculated due to unsuitable climatic conditions, inadequate wind stability class rating, or possible TRS emission mixing from other sources.



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A description of the TRS emissions from the major sources shown in Table 6-1 is provided below:

**Polishing Pond** – During Phase I the polishing pond was found to be the largest TRS emission source. It emitted an average of 540 lb/hr (with a range of 30 to 2300 lb/hr) during Phase I. During Phase II the emission rate was estimated to be 488 lb/hr (range of 10-2644 lb/hr). This represented an average 10 % decrease in mass emissions between the two phases.

The polishing pond continuously receives large quantities of sulfur compounds (e.g. sulfide, thiosulfite, and sulfate) from the process sewers. These sulfur compounds can convert to H<sub>2</sub>S and be released to the atmosphere. Some of the key factors that influence TRS releases from the polishing pond include:

- pH of the wastewater
- Wind speed above the wastewater
- Dissolved oxygen (DO) concentration
- Biological oxygen demand (BOD) content
- Total sulfur based material concentration

And as previously shown, TRS generation in the pond is significant. The 488 lb/hr only represents the airborne portion of the TRS. A total of approximately 670 lb/hr is being generated in the pond.

**ASB** – During Phase I, the TRS emissions from the ASB were estimated to be around 270 lb/hr. The SCREEN1 dispersion model was used with the ambient air data to make this estimate. During Phase II, unsuitable wind conditions did not allow acceptable ambient air results for the use of the SCREEN1 model.

However, TRS tests were performed on the wastewater entering the ASB during both Phases. The influent tests showed 113 lb/hr of TRS for Phase I and 195 lb/hr for Phase II. This represented a 72% increase. Much of this increase was due to the increase in TRS from the recaust sewer between Phase I and Phase II.

**Polishing Pond Inlet** – The polishing pond inlet is the region located at the southwest end of the polishing pond, at the inlet piping to the polishing pond from the ASB. TRS measurements were taken at the locations shown in Figure 2-2 as test sites 11, 11a and 11b.

A comparison between Phase I and Phase II showed a 54 % decrease in the TRS emission rate, from 41 lb/hr to 19 lb/hr.



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***Pulp Mill*** – During Phase I, the TRS emission rate from the pulp mill was estimated to be 23 lb/hr. Unfortunately, no suitable TRS measurements were taken during Phase II. Either unacceptable climatic conditions, inadequate wind stability class rating, or TRS emission interference from other sources prevented taking suitable TRS measurements from the pulp mill area.

As a consequence no Phase I and Phase II TRS emission rate comparison was conducted.

***Primary Clarifier*** – Phase I of the TRS study estimated the emission rate from the primary clarifier to be approximately 7 lb/hr. Again, no suitable ambient air data was available to conduct a SCREEN1 model estimate.

However, as a relative comparison, a wastewater test for TRS was conducted on the effluent. It showed 3 lb/hr TRS for Phase II.

### **6.3 *Implementation of the MACT Program***

The Pine Hill facility installed a condensate steam stripper system and NCG thermal oxidizer to comply with the MACT regulation. The primary purpose of this new equipment is to remove and destroy HAP (including TRS) that is contained in the pulp mill foul condensate.

The foul condensate is collected from selected processes throughout the pulp mill and stored in the steam stripper feed tank. The condensate is fed at an average rate of 400 gallons per minute (gpm) to the stripper distillation column. Virtually all of the TRS is removed from the condensate by the steam stripper.

The Pine Hill stripper feed condensate has an average concentration of 401 ppm TRS. Table 6-2 compares this concentration to condensate located at other Weyerhaeuser facilities.



**Table 6-2. Stripper Feed TRS Concentration Comparison**

<i>Facility</i>	<i>TRS Compounds</i>				<i>Total TRS (ppm)</i>
	<i>H<sub>2</sub>S (ppm)</i>	<i>MeSH (ppm)</i>	<i>DMS (ppm)</i>	<i>DMDS (ppm)</i>	
<i>Pine Hill</i>	<b>198</b>	<b>170</b>	<b>21</b>	<b>12</b>	<b>401</b>
<i>Columbus, MS</i>	130	39	265	139	573
<i>New Bern, NC</i>	61	99	132	503	795
<i>Valliant, OK</i>	460	215	47	183	905
<i>Plymouth, NC</i>	214	258	348	271	1091
<b>Average (not including Pine Hill)</b>	<b>216</b>	<b>153</b>	<b>198</b>	<b>274</b>	<b>841</b>

H<sub>2</sub>S = hydrogen sulfide  
MeSH = methyl mercaptan

DMS = dimethyl sulfide  
DMDS = dimethyl disulfide

As Table 6-2 shows, the TRS concentration in the Pine Hill stripper feed is less than half the average concentration of the other four Weyerhaeuser facilities. The data also shows that the Pine Hill condensate contains considerably less dimethyl sulfide (DMS) and dimethyl disulfide (DMDS) than the other facilities. The primary reason for this difference is because the Pine Hill stripper system does not receive the underflow from the turpentine decanter. Typical decanter underflow contains high concentrations of DMS and DMDS. It is expected that if the decanter underflow was sent to the stripper feed tank, the total TRS concentration would be closer to the average TRS concentration found at other Weyerhaeuser mills.

Before the condensate steam stripper was installed, the stripper condensate would have entered the power and recovery sewer, and eventually ended up at the wastewater treatment system. As a result, much of the TRS contained in the condensate could be emitted to the atmosphere from either the process sewer or wastewater treatment system.

With an average concentration of 401 ppm and a flow rate of 400 gpm, the stripper condensate contains approximately 80 lb/hr of TRS. Note that this is comparable to the 70 lb/hr estimated from the TRS mass flow measurements from the power and recovery sewer evaluation.



## 7.0 Conclusions

Based on the Phase I and Phase II ambient TRS study results, the following conclusions have been developed:

1. The MACT program resulted in a modest reduction of 80 lb/hr of TRS in the wastewater system. The mill continues to process over 700 lb/hr through the wastewater system.
2. The two most significant sources of ground level TRS emissions include the following:
  - *Polishing pond*
  - *ASB*
3. The major contributors of TRS to the wastewater treatment system include:
  - Sulfides in the recaust sewer.
  - Sulfide generation in the polishing pond due to anaerobic biological activity.
  - Note: Sulfide generation or oxidation in the ASB was not quantified during this phase of the study.



## 8.0 Recommendations

1. Develop means of reducing H<sub>2</sub>S generation in the polishing pond. This may include adding aeration capacity at the wastewater treatment system. (Note: Additional control of the H<sub>2</sub>S generation in other areas of the wastewater treatment system, e.g. ASB, primary clarifier, etc. may be required to address a total mill TRS reduction program).
2. Reduce and control the amount of TRS and high pH containing material going to the recaust sewer.
3. Evaluate effect of implementing items 1 and 2 above. This may involve documenting reduced ambient TRS impacts with the ENSR met station, and/or measuring the TRS emission reduction from the major sources using the air dispersion model approach.

# **Appendix**

*H<sub>2</sub>S Measurements*  
*Field Data*  
*Emission Models*  
*ENSR Weather Summary*  
*Phase II Process Sewer Flow Data*  
*Wastewater Lab Test Results*

**PINE HILL TRS STUDY - PHASE II**

# **H<sub>2</sub>S Measurements**



Pine Hill - Ambient H <sub>2</sub> S Odor Study Data										November / December 2001 Tests
Site	2001.4 Test Period		Jerome - ambient measurements				Wind (360°)		Air Temp	Weather Conditions and Comments - Observations
ID #	Date	Time	H <sub>2</sub> S ppb			AVG	direction	mph	°F	
6C	30-Nov	6:04	10	9	9	9	210	1.4	51	slight mill odor
6B	30-Nov	6:13	260	500	340	367	40 S	0.2		ASB
6B-2	30-Nov	6:18	1100	1400	580	1027	320	3.4		From inlet PP
6B-3	30-Nov	6:20	1400	1100	1006	1169	330	1.8		
6	30-Nov	6:23	1500	1114	1700	1438	330	2.9		
6-2	30-Nov	6:26	1400	1118	1900	1473	320	2.7		
6A	30-Nov	6:30	580	570	1400	850	320	2.9		
5A	30-Nov	6:34	510	420	660	528	210	2.7		4th reading - 520 ppb
5	30-Nov	6:40	68	50	32	50	215	1.7		
4C	30-Nov	6:45	3	3	3	3	--	0.0		
4	30-Nov	6:51	3	3	3	3	-- S	0.4		Road - mid pt
4B	30-Nov	6:55	3	3	3	3	--	0.0		
4A	30-Nov	6:58	3	3	3	3	0	1.9		
3C	30-Nov	7:01	120	260	190	190	45	3.9		Clar - strong
11D	30-Nov	7:03	52	48	450	183	330	4.5		Clar
11C	30-Nov	7:08	11	9	9	10	330	3.0		Kiln - upwind
11B	30-Nov	7:11	54	23	27	35	350	5.7		
11A	30-Nov	7:13	19	9	10	13	340	7.7		
11	30-Nov	7:16	2000	2400	400	1600	340	2.4		Riffler
11F	30-Nov	7:21	17	21	54	31	330	1.4		Across all ASB
11E	30-Nov	7:25	46	30	30	35	320	1.9		Inlet ASB
3	30-Nov	7:40	12	12	3	9	215	3.8		
3A	30-Nov	7:43	3	6	8	6	240	3.6		
8B	30-Nov	7:47	3	3	6	4	330	5.1		
10A	30-Nov	7:50	3	3	3	3	330	5.1		
10	30-Nov	7:53	3	3	3	3	355	6.9		
10B	30-Nov	7:55	3	3	3	3	330	5.3		
10C	30-Nov	7:57	3	4	4	4	325	4.4		
10D	30-Nov	7:59	3	3	3	3	325	3.2		
12	30-Nov	8:01	3	3	3	3	220	1.6		
8	30-Nov	8:20	3	3	3	3	280	6.1		
8A	30-Nov	8:22	3	3	3	3	260	10.1		
7A	30-Nov	8:27	3	3	3	3	200	1.7		
7	30-Nov	8:31	2	2	2	2	270	5.1		ENSR
1A	30-Nov	8:40	2	2	2	2	200	5.3		
2	30-Nov	8:44	2	2	2	2	260	3.4		
2A	30-Nov	8:47	3	3	3	3	240	6.4		
2B	30-Nov	8:49	3	5	6	5	280	8.4		
2C	30-Nov	8:52	3	6	6	5	270	2.8		

**WEATHER : 11/30/01 - 1/2**

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Cloudy, cool and windy with winds from the NW mostly light and variable. Occasional wind gusts in a straight line on a short-term basis.

D class to 08:00, then C

Mostly, groundlevel winds swirling quite a bit making

**Pine Hill - Ambient H<sub>2</sub>S Odor Study Data**

**November / December 2001 Tests**

Site ID #	2001.4 Test Period		Jerome - ambient measurements				Wind (360°)		Air Temp	Weather Conditions and Comments - Observations
	Date	Time	H <sub>2</sub> S ppb			AVG	direction	mph	°F	
7	30-Nov	15:13	22	5	7	11	300	1.6	65	Winds twitchy
11E	30-Nov	15:17	120	55	54	76	350	1.2		
11C	30-Nov	15:20	6	14	54	25	320	2.7		Winds SW to N
11B	30-Nov	15:23	7	5	6	6	0	2.5		No odor
11A	30-Nov	15:26	11	60	50	40	320	1.4		Very slight PP
11	30-Nov	15:29	160	29	56	82	20	2.0		Strong organic odor, not H <sub>2</sub> S
11F	30-Nov	15:32	120	23	22	55	320	4.0		Strong organic odor, not H <sub>2</sub> S
6C	30-Nov	15:35	72	68	68	69	270	0.5		Dead Air
6B	30-Nov	15:38	580	520	680	593	300	0.4		PP odor
6B-1	30-Nov	15:41	670	1400	1500	1190	320	2.9		PP odor
6	30-Nov	15:44	1900	1200	1300	1467	350	5.1		strong PP odor
6-1	30-Nov	15:46	660	1400	660	907	340	2.3		strong PP odor
6	30-Nov	15:48	1500	460	570	843	320	2.5		strong PP odor
5A	30-Nov	15:51	4	3	5	4	--	0.0		
5	30-Nov	15:53	4	4	3	4	340	1.9		
4C	30-Nov	15:56	3	3	3	3	330	0.1		
4	30-Nov	15:58	3	3	3	3	340	0.6		
4B	30-Nov	16:01	3	3	3	3	10	0.9		
4A	30-Nov	16:04	23	20	120	54	350	0.2		
11D	30-Nov	16:05	107	150	54	104	0	2.0		Clar on + off ENE
11E	30-Nov	16:08	16	58	47	40	330	2.1		Clarifier -winds direct from clarifier but vapor plume going West due to wind swirl in bowl
3A	30-Nov	16:12	8	9	4	7	40	3.0		
3	30-Nov	16:14	100	140	5	82	350	1.8		Stinky ash pond
2B	30-Nov	16:18	3	3	2	3	0	1.3		
2A	30-Nov	16:20	3	2	3	3	0	2.1		
2C	30-Nov	16:23	8	5	7	7	340	1		Cross BL storage
2	30-Nov	16:26	3	3	3	3	10	0.7		
1	30-Nov	16:30	3	3	3	3	320	2.7		
12	30-Nov	16:34	18	28	27	24	70	2.8		Main stacks all N
10B	30-Nov	16:40	8	8	8	8	90 S	0.1		
10C	30-Nov	16:42	5	15	4	8	270	1.2		Oily smell
10D	30-Nov	16:43	4	4	3	4	--	0.0		
10	30-Nov	16:45	18	29	15	21	10	1.0		Clar odor
10A	30-Nov	16:47	11	2	5	6	340	1.0		slight clar
8	30-Nov	16:55	4	4	4	4	45	2.3		
8A	30-Nov	17:00	15	15	10	13	340	2.2		
8B	30-Nov	17:10	8	4	4	5	0	1.9		Thru mill
7C	30-Nov	17:11	56	230	200	162	0	1.3		

**WEATHER : 11/30/01 - 2/2**  
 Sunny and mild with very light, variable winds mostly from the NW then turning predominantly N / NE after 16:20  
 C class, then D class after 17:00  
 groundlevel winds very light, swirling and from variable

GLADNEY-WY032320

**Pine Hill - Ambient H<sub>2</sub>S Odor Study Data**

**November / December 2001 Tests**

Site ID #	2001.4 Test Period		Jerome - ambient measurements				Wind (360°)		Air Temp	Weather Conditions and Comments - Observations
	Date	Time	H <sub>2</sub> S ppb			AVG	direction	mph	°F	
6C	1-Dec	5:46	300	330	330	320	320	0.2	39	Odor present but non-directional
6B	1-Dec	5:50	350	410	420	393	--	0.0		
6	1-Dec	5:52	460	550	540	517	--	0.0		
6A	1-Dec	5:57	350	350	310	337	--	0.0		
5A	1-Dec	6:00	14	12	28	18	--	0.0		
5	1-Dec	6:03	1	1	1	1	40	0.2		
4C	1-Dec	6:07	1	1	1	1	200	0.0		
4	1-Dec	6:09	0	0	0	0	--	0.0		
4B	1-Dec	6:12	1	1	1	1	350	1.1		
4A	1-Dec	6:14	1	1	1	1	--	1.0		
11D	1-Dec	6:19	180	110	26	105	60	0.2		
11E	1-Dec	6:25	240	140	19	133	--	0.0		
11F	1-Dec	6:28	130	230	190	183	320	0.2		
11	1-Dec	6:30	250	240	190	227	280	0.5		
11A	1-Dec	6:34	72	77	110	86	--	0.0		
11B	1-Dec	6:36	52	57	49	53	320	0.5		
11C	1-Dec	6:39	21	35	48	35	320	0.1		
7	1-Dec	6:44	15	14	12	14	240	0.6		
7A	1-Dec	6:51	8	10	10	9	--	0.0		
12	1-Dec	6:56	3	3	3	3	260	1.4		
12A	1-Dec	6:59	3	3	3	3	260	1.4		
12B	1-Dec	7:00	7	7	2	5	220	0.5		
2	1-Dec	7:04	2	2	1	2	--	0.0		
2C	1-Dec	7:07	2	2	2	2	300	1.2		
2A	1-Dec	7:10	3	0	0	1	340	1.2		
2B	1-Dec	7:13	3	0	0	1	350	0.3		
3	1-Dec	7:15	11	2	11	8	0	2.0		
3A	1-Dec	7:19	3	3	28	11	10	2.4		
3B	1-Dec	7:23	21	14	14	16	340	1.0		
10A	1-Dec	7:26	140	128	50	106	345	1.3		Clarifier
10	1-Dec	7:28	170	120	140	143	20	2.0		No mill odor
10B	1-Dec	7:31	8	8	8	8	--	0.0		
10C	1-Dec	7:34	6	3	3	4	300	2.0		
10D	1-Dec	7:36	4	4	3	4	60	0.9		
1	1-Dec	7:41	11	12	12	12	--	0.0		
8	1-Dec	8:24	180	140	170	163	30	1.0		ASB/PP
8A	1-Dec	8:27	140	50	190	127	60	0.5		PP

**WEATHER : 12/01/01 - 1/1**  
 Cold and foggy with no ground level winds at most locations.  
 Non-directional swirling when short term light wind gusts arise  
 D class, turning C after 7:00 - 7:30

Pine Hill - Ambient H <sub>2</sub> S Odor Study Data										November / December 2001 Tests
Site ID #	2001.4 Test Period		Jerome - ambient measurements				Wind (360°)		Air Temp	Weather Conditions and Comments - Observations
	Date	Time	H <sub>2</sub> S ppb			AVG	direction	mph	°F	
7	2-Dec	5:33	155	260	310	242	50	0.1	45	ENSR
6C	2-Dec	5:37	300	230	190	240	--	0.0		
6B	2-Dec	5:40	190	510	56	252	--	0.0		Dead air along trees
6	2-Dec	5:45	170	52	52	91	--	0.0		Dead calm
6A	2-Dec	5:50	950	510	780	747	320	0.5		Breeze - moves odor
5A	2-Dec	5:56	9	4	4	6	10	0.2		
5	2-Dec	5:58	4	4	2	3	320	0.2		
4C	2-Dec	6:02	0	0	0	0	--	0.0		
4	2-Dec	6:04	0	0	2	1	20	0.6		
4B	2-Dec	6:08	2	2	2	2	0	0.1		
4A	2-Dec	6:10	340	210	240	263	350	0.1		H2S smell
4D	2-Dec	6:15	110	350	550	337	290	0.9		Clear
11D	2-Dec	6:17	43	43	32	39	270	0.1		Mill
11B	2-Dec	6:23	110	98	140	116	--	0.0		
11A	2-Dec	6:25	110	83	100	98	350	0.5		Old outfall
11	2-Dec	6:27	170	110	150	143	320	0.9		Riffler
11F	2-Dec	6:32	140	140	130	137	10	3.4		Across ASB
11G	2-Dec	6:35	40	200	222	154	340	2.3		
11C	2-Dec	6:38	200	230	250	227	280	1.2		
10	2-Dec	6:42	14	12	12	13	10	2.6		Clear
10A	2-Dec	6:45	8	9	9	9	0	3.8		
10E	2-Dec	6:48	150	130	44	108	0	2.4		Clear Direct 10E/10F
10F	2-Dec	6:51	21	53	52	42	350	1.2		Further down
3B	2-Dec	6:54	58	52	50	53	320	0.6		
3	2-Dec	7:00	3	3	5	4	350	1.7		Ash pond outfall
2B	2-Dec	7:02	2	2	3	2	280	0.5		
2A	2-Dec	7:06	3	2	4	3	300	0.7		
2C	2-Dec	7:08	4	0	2	2	270	0.6		
2	2-Dec	7:11	2	2	2	2	--	0.0		
12B	2-Dec	7:15	2	2	2	2	260	2.5		
12A	2-Dec	7:17	2	2	2	2	260	3.2		
12	2-Dec	7:19	2	6	7	5	250	0.1		
12C	2-Dec	7:23	14	16	11	14	0	0.8		
10D	2-Dec	7:24	2	1	1	1	310	1.5		
10C	2-Dec	7:26	1	1	2	1	270	3.4		
10B	2-Dec	7:29	2	2	3	2	270	1.3		
1	2-Dec	7:35	2	2	3	2	230	1.8		
8	2-Dec	7:40	3	3	3	3	250	2		
8A	2-Dec	7:42	1	1		1	300	1.0		

**WEATHER : 12/02/01 - 1/1**  
 Cool and calm, with predominantly very light and variable winds from Northerly direction when measureable. D class to 7:00 - 7:30 inversion early. Mostly dead, calm air. When a short-term breeze arises it is gusty and variable in direction.

GLADNEY-WY032322

**Pine Hill - Ambient H<sub>2</sub>S Odor Study Data**

**November / December 2001 Tests**

Site ID #	2001.4 Test Period		Jerome - ambient measurements				Wind (360°)		Air Temp	Weather Conditions and Comments - Observations
	Date	Time	H <sub>2</sub> S ppb			AVG	direction	mph	°F	
7	3-Dec	6:03	65	60	75	67	--	0.0	43	
6C	3-Dec	6:06	73	--	--	73	--	0.0		Truck ex
6B	3-Dec	6:13	110	111	140	120	--	0.0		
6	3-Dec	6:15	150	160	160	157	--	0.0		Vapor sitting over PP, not moving off
6A	3-Dec	6:18	47	57	64	56	--	0.0		
5A	3-Dec	6:21	150	140	140	143	350	0.3		
5	3-Dec	6:24	34	31	16	27	--	0.0		
4C	3-Dec	6:32	0	0	0	0	--	0.0		
4	3-Dec	6:34	1	1	0	1	--	0.0		
4B	3-Dec	6:37	0	0	0	0	280	0.1		
4A	3-Dec	6:40	0	0	0	0	--	0.0		
11D	3-Dec	6:48	150	106	180	145	--	0.0		
11B	3-Dec	6:53	111	110	75	99	--	0.0		
11A	3-Dec	6:56	560	420	480	487	--	0.0		Stinks like PP
11	3-Dec	6:59	730	720	750	733	--	0.0		
11F	3-Dec	7:03	6	6	9	7	--	0.0		
11E	3-Dec	7:06	720	760	730	737	320	1.1		Stinky ASB
11C	3-Dec	7:08	590	490	540	540	280	2.4		
7A	3-Dec	7:12	12	10	7	10	320	0.3		
8A	3-Dec	7:33	3	3	2	3	--	0.0		
8	3-Dec	7:35	3	5	5	4	140	1.0		Drove down highway 10 minimal odor
12A	3-Dec	7:40	3	3	2	3	--	0.0		
10	3-Dec	7:42	2	2	6	3	--	0.0		
3A	3-Dec	7:55	12	4	8	8	--	0.0		
7	3-Dec	8:04	5	4	5	5	--	0.0		End - no wind
4B	3-Dec	11:39	200	--	--	200	25	2.5	74	gust across pp
4Ba	3-Dec	11:33	130	--	--	130	25	2.9		gust across pp
4A	3-Dec	11:44	150	--	--	150	25	3.0		gust across pp
No measurable wind at remaining sample points										

**WEATHER : 12/03/01 - 1/2**  
 .....  
 Cool and calm with almost no ground level winds at all  
 considerable odor in some in-mill locations but non-directional D class until 7:00 - 7:30 inversion early

**WEATHER : 12/03/01 - 2/2**  
 .....  
 PolishPond water Sparge Trial Round 1  
 Very sunny and warm after cooler AM, with very calm afternoon winds after dead air all day. Some occasional, variable gusts now, few and far between C class stability

GLADNEY-WY032323

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Pine Hill - Ambient H <sub>2</sub> S Odor Study Data										November / December 2001 Tests
Site ID #	2001.4 Test Period		Jerome - ambient measurements				Wind (360°)		Air Temp	Weather Conditions and Comments - Observations
	Date	Time	H <sub>2</sub> S ppb			Avg	direction	mph	°F	
7	4-Dec	14:05	6	6	6	6	100	4.1	75	Strong solar rad
6C	4-Dec	14:10	110	150	120	127	90	1.5		
6B	4-Dec	14:11	11	8	8	9	105	2.5		
6D	4-Dec	14:18	580	530	170	427	10	1.8		PP odor
6	4-Dec	14:21	110	5	2	39	180	0.5		wind variable + twitchy
6A	4-Dec	14:23	118	510	200	276	350	1.1		wind variable + twitchy
5A	4-Dec	14:27	8	8	8	8	30	0.5		
5	4-Dec	14:31	8	8	8	8	50	0.6		
4C	4-Dec	14:35	67	4	4	25	90	3.0		
4	4-Dec	14:39	270	220	130	207	95	4.3		Funky wind + stink
4B	4-Dec	14:42	510	270	180	320	80	4.1		Funkadelic
4D	4-Dec	14:46	520	540	210	423	90	3.5		Ditto - Wind steadier
4A	4-Dec	14:50	1008	1200	540	916	95	6.1		Weaker sun now
4E	4-Dec	14:57	520	540	410	490	100	4.4		
11D	4-Dec	15:00	190	170	140	167	90	3.9		
11G	4-Dec	15:10	120	150	500	257	70	3.6		ASB + PP
11H	4-Dec	15:15	1300	2700	1700	1900	75	4.1		Across ASB incl R
11I	4-Dec	15:20	430	260	300	330	75	5.3		11i @ corner of store room
11J	4-Dec	15:23	290	500	520	437	75	2.3		Mid of Str room
11K	4-Dec	15:26	270	280	210	253	80	5.2		11K end of Str room
11L	4-Dec	15:29	170	120	120	137	80	2.1		11L near PH sewer
11B	4-Dec	15:36	520	500	570	530	80	3.6		Pol pond
11A	4-Dec	15:41	270	570	540	460	85	2.8		
11	4-Dec	15:45	250	110	147	169	100	3.3		
11M	4-Dec	15:50	560	490	400	483	85	2.9		
11F	4-Dec	15:54	12	12	8	11	95	2.4		Low road data 1600 - 1815
11N	4-Dec	16:09	210	510	530	417	65	5.7		PP
4F	4-Dec	16:20	530	670	670	623	95	3.3		All PP from east along ash pond outer road - distant PP read
4G	4-Dec	16:23	1300	1400	1490	1397	95	4.9		All PP from east along ash pond outer road - distant PP read
4H	4-Dec	16:30	1200	1100	500	933	85	1.9		All PP from east along ash pond outer road - distant PP read
2	4-Dec	16:38	17	9	9	12	80	3.7		
9	6-Dec	11:28	1800	320	940	1020	220	3.7	76	16R0456425-3537826
9a	6-Dec	11:39	500	200	880	527	210	1.2		16R0456373-3537874
8	6-Dec	11:53	780	950	500	743	220	1.8		"
7	6-Dec	12:08	540	580	1400	840	280	2.1		0456335-353795
6	6-Dec	12:29	560	650	1100	770	180	4.0		0456034-3538227
6a	6-Dec	12:34	880	410	320	537	190	2.5		0455934-3538370
6b	6-Dec	12:53	200	140	810	383	140	1.5		0455784-3536548
5	6-Dec	13:15	1100	750	860	983	140	1.9		0455426-3538198
4	6-Dec	13:38	420	200	510	377	180	1.5		0455451-3538232
3	6-Dec	14:01	350	300	460	370	200	2.5		0455229-3538008
2	6-Dec	14:08	350	410	830	530	190	1.9		0455134-3537911
1	6-Dec	14:12	110	420	850	460	200	1.4	80	"

**WEATHER : 12/04/01 - 1/1**  
 Very clear, warm day with a steady breeze and a full winter sun.  
 Inversion early  
 C class, turning D / inversion after 17:00  
 Strong solar radiation  
 winds predominantly from Easterly direction

**WEATHER : 12/06/01 - 1/1**  
 Pond Study and Sparge tests second round  
 Sunny, clear, very warm, with light winds with occasional gusts  
 C class, turning D 16:30-17:00  
 wind direction mostly from S/SW

GLADNEY-WY032324

Pine Hill - Ambient H <sub>2</sub> S Odor Study Data										November / December 2001 Tests
Site	2001.4 Test Period		Jerome - ambient measurements				Wind (360°)		Air Temp	Weather Conditions and Comments - Observations
ID #	Date	Time	H <sub>2</sub> S ppb			AVG	direction	mph	°F	
7	8-Dec	13:11	12	60	20	31	280	7.0	74	paper mach+pm smell
7a	8-Dec	13:14	400	340	210	317	270	7.7		ASB isolated
7b	8-Dec	13:18	730	670	440	613	300	6.9		ASB further up road
7c	8-Dec	13:20	2100	1270	1300	1557	280	7.9		ASB -edge
6c	8-Dec	13:22	260	220	520	333	270	3.9		
6b	8-Dec	13:25	520	2600	1800	1640	300	3.4		PP - off inlet area
6d	8-Dec	13:50	3200	1200	2800	2400	310	6.7		Nasty
6	8-Dec	13:32	2800	1500	2300	2200	360	7.0		Nasty
6e	8-Dec	13:35	2200	2400	2800	2467	330	9.3		Nasty
6a	8-Dec	13:37	1800	1700	630	1377	350	6.0		Not as bad
5a	8-Dec	13:43	6	7	7	7	20	2.7		Fresh as a daisy
5	8-Dec	13:45	6	6	5	6	320	2.5		
4c	8-Dec	13:48	4	5	5	5	300	2.3		
4	8-Dec	13:52	5	5	5	5	810	1.5		
4b	8-Dec	13:55	4	5	4	4	300	0.3		
4a	8-Dec	13:57	4	4	4	4	270	2.5		smells clean
4D	8-Dec	13:59	60	54	130	81	310	3.6		Ash P
4E	8-Dec	14:03	120	160	120	133	350	5.3		Ash P - more +
4F	8-Dec	14:04	140	150	120	137	330	8.2		Clar direct
11D	8-Dec	14:07	70	23	53	49	330	3.2		clar - on edge
11G	8-Dec	14:11	16	10	12	13	320	2.9		clar - on edge at times
11C	8-Dec	14:16	6	6	6	6	280	5.2		straight clar/mill
11B	8-Dec	14:18	52	14	15	27	340	4.0		good clar smell on + off
11A	8-Dec	14:22	520	550	520	530	360	8.4		right over outfall
11H	8-Dec	14:26	540	620	570	577	350	2.1		pp
11	8-Dec	14:28	1400	2000	1200	1533	320	3.9		Riff
11I	8-Dec	14:30	580	610	200	463	10	3.2		pp
3A	8-Dec	15:21	6	16	50	24	260	5.2		full sun again - low angle
3	8-Dec	15:24	2	3		3	270	4.2		
2B	8-Dec	15:27	4	4		4	290	2.9		blk liq smell
2A	8-Dec	15:30	4	4		4	280	4.0		
2C	8-Dec	15:33	3	3		3	260	3.4		
2	8-Dec	15:35	3	4		4	260	1.1		
10D	8-Dec	15:38	4	4		4	270	3.7		
10	8-Dec	15:40	6	6		6	300	9.8		
10A	8-Dec	15:42	7	8	7	7	320	6.2		
10E	8-Dec	15:44	16	16	13	15	300	3.8		
10F	8-Dec	15:47	8	2		5	300	0.8		
8B	8-Dec	16:21	52	6	5	21	280	1.9		

**WEATHER : 12/08/01 - 1/1**  
 .....  
 Fairly stable climate - Mostly  
 cloudy, windy day, warm, with  
 good gusts of steady direction  
 and speed  
 C class, close to D, inversion  
 early  
 Wind from W through the N/E

GLADNEY-WY032325



**Pine Hill - Ambient H<sub>2</sub>S Odor Study Data**

**November / December 2001 Tests**

Site ID #	2001.4 Test Period		Jerome - ambient measurements				Wind (360°)		Air Temp	Weather Conditions and Comments - Observations	
	Date	Time	H <sub>2</sub> S ppb			AVG	direction	mph	°F		
7A	9-Dec	9:10	160	240	270	223	30	4.0	56	pp	<b>WEATHER : 12/09/01 - 1/1</b> + asb edge at end Cloudy, cool and windy P mill along _____ Very stable conditions with low clouds, little solar strength and steady winds from N/NE strong D class early, tending to C after 10:00
7B	9-Dec	9:12	138	270	500	303	50	2.7			
7c	9-Dec	9:15	280	340	240	287	20	2.3			
7D	9-Dec	9:18	130	130	230	163	350	2.8		p + asb	
?	9-Dec	9:30	3	14	14	10	360	9.8		P mill along _____	
7	9-Dec	9:57	230	200	140	190	360	3.3		ensr	
6D	9-Dec	10:01	500	420	580	500	300	2.4		pp - asb _____	
11G	9-Dec	10:09	1008	610	1116	911	30	2.3		pp	
11H	9-Dec	10:12	580	580	730	630	20	11.1		pp	
11B	9-Dec	10:19	160	180	180	173	10	5.0		pp	
11A	9-Dec	10:20	240	220	180	213	340	3.5		pp	
11i	9-Dec	10:25	510	710	790	670	350	3.8		pp	
11J	9-Dec	10:28	500	490	550	513	360	4.0			
11	9-Dec	10:30	520	530	550	533	360	4.2		R + PP - no H25 smell. Organic	
11k	9-Dec	10:33	580	720	670	657	30	2.2		pp	
11F	9-Dec	10:35	230	400	420	350	10	6.9		ASB + PP - no H25 - organic	
11L	9-Dec	10:37	430	160	150	247	360	5.5		ASB + PP	
11m	9-Dec	10:41	290	200	190	227	360	5.9		ASB + PP	
11n	9-Dec	10:43	1400	2700	1114	1738	10	5.0		Not bad	
11c	9-Dec	10:46	490	500	1111	700	10	3.8		Stinkier - funky	
10e	9-Dec	11:48	380	360	170	303	10	7.1		less pungent	
10f	9-Dec	11:52	48	59	8	38	350	4.3		clar	
10g	9-Dec	11:55	11	14	10	12	10	2.1		not much odor	
1a	9-Dec	12:03	10	9	4	8	350	7.8		not much odor, right downwind	
1	9-Dec	12:06	9	10	23	14	10	4.8		thru mill	
1C	9-Dec	12:09	27	57	10	31	20	3.9		"	
7a	9-Dec	12:13	69	64		67	340	1.3		pulp mill smell	
7e	9-Dec	12:16	120	130	130	127	10	4.0		ASB	
11k	9-Dec	12:20	290	510	320	373	350	5.5		ASB	
11i	9-Dec	12:23	500	590	380	490	360	7.0		PP	
11a	9-Dec	12:26	280	440	130	283	360	8.6		PP	
11b	9-Dec	12:29	170	120	150	147	10	3.7			
3c	9-Dec	12:34	17	21		19	350	0.3		EQ Pond	
3a	9-Dec	12:36	41	25	78	48	350	7.1		Ash - E	
3	9-Dec	12:39	9	5	4	6	360	3.3		Ash - W - stinky	

GLADNEY-WY032326



**All H2S Measurements from identifiable source, over 1 mph wind**

Polishing Pond H2S Readings ; P=full reach E or W edge. P-O=Outfall Area only										
P-I=Inlet Area measured on south shore, N wind										
LOC	DATE	TIME	1	2	3	AVG	A	MPH	F	S
6B-2	30-Nov	6:18	1100	1400	580	1027	320	3.4	51	P
6B-3	30-Nov	6:20	1400	1100	1008	1169	330	1.8	51	P
6	30-Nov	6:23	1500	1114	1700	1438	330	2.9	51	P
6-2	30-Nov	6:26	1400	1118	1900	1473	320	2.7	51	P
6A	30-Nov	6:30	580	570	1400	850	320	2.9	51	P
5A	30-Nov	6:34	510	420	660	528	210	2.7	51	P-O
5	30-Nov	6:40	68	50	32	50	215	1.7	51	P
11D	30-Nov	7:03	52	48	450	183	330	4.5	51	P
11	30-Nov	7:16	2000	2400	400	1600	340	2.4	51	P
11	30-Nov	15:29	180	29	56	82	20	2.0	65	P
11F	30-Nov	15:32	120	23	22	55	320	4.0	65	P
6B-1	30-Nov	15:41	670	1400	1500	1190	320	2.9	65	P
6	30-Nov	15:44	1900	1200	1300	1467	350	5.1	65	P-O
6-1	30-Nov	15:46	660	1400	660	907	340	2.3	65	P-O
6	30-Nov	15:48	1500	460	570	843	320	2.5	65	P
11D	30-Nov	16:05	107	150	54	104	0	2.0	65	P
6D	4-Dec	14:18	580	530	170	427	10	1.8	75	P
4	4-Dec	14:39	270	220	130	207	95	4.3	75	P
4B	4-Dec	14:42	510	270	180	320	80	4.1	75	P
4D	4-Dec	14:46	520	540	210	423	90	3.5	75	P
4A	4-Dec	14:50	1008	1200	540	916	95	6.1	75	P
4E	4-Dec	14:57	520	540	410	490	100	4.4	75	P
11G	4-Dec	15:10	120	150	500	257	70	3.6	75	P
11H	4-Dec	15:15	1300	2700	1700	1900	75	4.1	75	P
11I	4-Dec	15:20	430	260	300	330	75	5.3	75	P
11J	4-Dec	15:23	290	500	520	437	75	2.3	75	P
11K	4-Dec	15:26	270	280	210	253	80	5.2	75	P
11L	4-Dec	15:29	170	120	120	137	80	2.1	75	P
11B	4-Dec	15:36	520	500	570	530	80	3.6	75	P
11A	4-Dec	15:41	270	570	540	460	85	2.8	75	P
11N	4-Dec	16:09	210	510	530	417	65	5.7	75	P

**Polishing Pond H2S Readings (continued)**

LOC	DATE	TIME	1	2	3	AVG	A	MPH	F	S
4F	4-Dec	16:20	530	670	670	623	95	3.3	75	P
4G	4-Dec	16:23	1300	1400	1490	1397	95	4.9	75	P-O
4H	4-Dec	16:30	1200	1100	500	933	85	1.9	75	P
5	6-Dec	13:15	1100	750	860	983	140	1.9	76	P
4	6-Dec	13:38	420	200	510	377	180	1.5	76	P
6c	8-Dec	13:22	260	220	520	333	270	3.9	74	P
6b	8-Dec	13:25	520	2600	1800	1640	300	3.4	74	P
6	8-Dec	13:32	2600	1500	2300	2200	360	7.0	74	P-O
6e	8-Dec	13:35	2200	2400	2800	2467	330	9.3	74	P
6a	8-Dec	13:37	1800	1700	630	1377	350	6.0	74	P-O
6d	8-Dec	13:50	3200	1200	2800	2400	310	6.7	74	P
11A	8-Dec	14:22	520	550	520	530	360	8.4	74	P
11H	8-Dec	14:26	540	620	570	577	350	2.1	74	P
7B	9-Dec	9:12	138	270	500	303	50	2.7	56	P
6D	9-Dec	10:01	500	420	580	500	300	2.4	56	P
11G	9-Dec	10:09	1008	610	1116	911	30	2.3	56	P
11H	9-Dec	10:12	580	580	730	630	20	11.1	56	P-I
11B	9-Dec	10:19	160	180	180	173	10	5.0	56	P
11A	9-Dec	10:20	240	220	180	213	340	3.5	56	P
11i	9-Dec	10:25	510	710	790	670	350	3.8	56	P-I
11J	9-Dec	10:28	500	490	550	513	360	4.0	56	P-I
11	9-Dec	10:30	520	530	550	533	360	4.2	56	P
11k	9-Dec	10:33	580	720	670	657	30	2.2	56	P
11L	9-Dec	10:37	430	160	150	247	360	5.5	56	P
11c	9-Dec	10:46	490	500	1111	700	10	3.8	56	P
11k	9-Dec	12:20	290	510	320	373	350	5.5	56	P
11i	9-Dec	12:23	500	590	360	490	360	7.0	56	P-I
11a	9-Dec	12:26	280	440	130	283	360	8.6	56	P
11b	9-Dec	12:29	170	120	150	147	10	3.7	56	P

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avg 726  
med 529

P-I = Polishing Pond Inlet Area	avg	576	med	572
P-O = Polishing Pond Outlet Area	avg	1312	med	1387

**Clarifier H2S Readings - NOTE: Ash Pond Background it Clarifier measurements from NW through NE**

LOC	DATE	TIME	1	2	3	AVG	A	MPH	F	S
10	30-Nov	7:53	3	3	3	3	355	6.9	51	C/A
10	30-Nov	16:45	18	29	15	21	10	1.0	65	C/A
10A	30-Nov	16:47	11	2	5	6	340	1.0	65	C/A
3	6-Dec	14:01	350	300	460	370	200	2.5	76	C
3A	8-Dec	15:21	6	16	50	24	260	5.2	74	C
10e	9-Dec	11:48	380	360	170	303	10	7.1	56	C/A
10f	9-Dec	11:52	48	59	8	38	350	4.3	56	C/A
10g	9-Dec	11:55	11	14	10	12	10	2.1	56	C/A
8						average	97			
						median	22			

**ASB H2S Readings - note: some background concentration from Polishing Pond likely at most sample points, a points, as noted, include background from Riffler emissions. Wind swirls around ASB burn, mixing ASB and Pond emissions from W/NW**

LOC	DATE	TIME	1	2	3	AVG	A	MPH	F	S
11F	30-Nov	7:21	17	21	54	31	330	1.4	51	ASB/P
11F	30-Nov	7:21	17	21	54	31	330	1.4	51	ASB/P
11E	30-Nov	7:25	46	30	30	35	320	1.9	51	ASB/P
11E	30-Nov	7:25	46	30	30	35	320	1.9	51	ASB/P
11E	30-Nov	15:17	120	55	54	76	350	1.2	65	ASB/P
11E	30-Nov	15:17	120	55	54	76	350	1.2	65	ASB/P
11E	30-Nov	16:08	16	58	47	40	330	2.1	65	ASB/P
11E	30-Nov	16:08	16	58	47	40	330	2.1	65	ASB/P
7C	30-Nov	17:11	56	230	200	162	0	1.3	65	ASB/P
11D	4-Dec	15:00	190	170	140	167	90	3.9	75	ASB/P
11D	4-Dec	15:00	190	170	140	167	90	3.9	75	ASB/P
11	4-Dec	15:45	250	110	147	169	100	3.3	75	ASB
11	4-Dec	15:45	250	110	147	169	100	3.3	75	ASB
11M	4-Dec	15:50	560	490	400	483	85	2.9	75	ASB/P
11M	4-Dec	15:50	560	490	400	483	85	2.9	75	ASB/P
7	6-Dec	12:08	540	580	1400	840	280	2.1	76	ASB/P
7	8-Dec	13:11	12	60	20	31	280	7.0	74	ASB/P
7a	8-Dec	13:14	400	340	210	317	270	7.7	74	ASB/P
7c	8-Dec	13:20	2100	1270	1300	1557	280	7.9	74	ASB/P
11	8-Dec	14:28	1400	2000	1200	1533	320	3.9	74	P/RIF
11	8-Dec	14:28	1400	2000	1200	1533	320	3.9	74	P/RIF
11l	8-Dec	14:30	580	610	200	463	10	3.2	74	ASB/P
7A	9-Dec	9:10	160	240	270	223	30	4.0	56	ASB/P
7c	9-Dec	9:15	280	340	240	287	20	2.3	56	ASB/P
7D	9-Dec	9:18	130	130	230	163	350	2.8	56	ASB/P
7	9-Dec	9:57	230	200	140	190	360	3.3	56	ASB/P
11F	9-Dec	10:35	230	400	420	350	10	6.9	56	ASB/P
11m	9-Dec	10:41	290	200	190	227	360	5.9	56	ASB/P
11m	9-Dec	10:41	290	200	190	227	360	5.9	56	ASB/P
11n	9-Dec	10:43	1400	2700	1114	1738	10	5.0	56	ASB/P
7a	9-Dec	12:13	69	64	-	67	340	1.3	56	ASB/P
7e	9-Dec	12:16	120	130	130	127	10	4.0	56	ASB/P
32						average	376			
						median	169			

**Equalization Basin Readings - at edge**

LOC	DATE	TIME	1	2	3	AVG	A	MPH	F	S
3A	30-Nov	16:12	8	9	4	7	40	3.0	65	EQ
1						average	7			
						median	7			

**Ash Pond Area Readings at edge**

LOC	DATE	TIME	1	2	3	AVG	A	MPH	F	S
3	30-Nov	16:14	100	140	5	82	350	1.8	65	ASH
3a	9-Dec	12:36	41	25	78	48	350	7.1	56	ASH
3	9-Dec	12:39	9	5	4	6	360	3.3	56	ASH
3						average	45			
						median	48			

**PulpMill, PowerHouse, Evaporator Area Readings**

LOC	DATE	TIME	1	2	3	AVG	A	MPH	F	S
1	9-Dec	12:06	9	10	23	14	10	4.8	56	M
1a	9-Dec	12:03	10	9	4	8	350	7.8	56	M
1A	9-Dec	9:30	3	14	14	10	360	9.8	56	M
8B	8-Dec	16:21	52	6	5	21	280	1.9	74	M
8B	30-Nov	7:47	3	3	6	4	330	5.1	51	M
8A	30-Nov	17:00	15	15	10	13	340	2.2	65	M
12	30-Nov	16:34	18	28	27	24	70	2.8	65	pulp
12	30-Nov	8:01	3	3	3	3	220	1.6	51	Recov
7 combined area						average	12			
						median	12			

**Recausticizing Area Readings - downwind, through area**

LOC	DATE	TIME	1	2	3	AVG	A	MPH	F	S
10	8-Dec	15:40				6	300	9.8	74	R
10E	8-Dec	15:44				15	300	3.8	74	R
2						average	11			
						median	11			

## **List of Emission Models**

**Polishing Pond Measurements**

MAP LOC	2001 DATE	SAMPLE TIME	H <sub>2</sub> S ppb				Wind Data		Temp °F	Model	RATE Lbs/Hr
			Readings			avg	A°	mph			
4	4-Dec	14:39	270	220	130	207	95	4.3	75		
4A	4-Dec	14:50	1008	1200	540	916	95	6.1	75	2P	
4B	4-Dec	14:42	510	270	180	320	80	4.1	75		
4D	4-Dec	14:46	520	540	210	423	90	3.5	75		
4E	4-Dec	14:57	520	540	410	490	100	4.4	75	5P	
4F	4-Dec	16:20	530	670	670	623	95	3.3	75		
4G	4-Dec	16:23	1300	1400	1490	1397	95	4.9	75		
5A	30-Nov	6:34	510	420	660	528	210	2.7	51		
6	30-Nov	6:23	1500	1114	1700	1438	330	2.9	51	9P	
6	30-Nov	15:44	1900	1200	1300	1467	350	5.1	65		
6	30-Nov	15:48	1500	460	570	843	320	2.5	65	11p	
6	8-Dec	13:32	2800	1500	2300	2200	360	7.0	74		
6-1	30-Nov	15:46	660	1400	660	907	340	2.3	65		
6-2	30-Nov	6:26	1400	1118	1900	1473	320	2.7	51	14p	
6A	30-Nov	6:30	580	570	1400	850	320	2.9	51	15p	
6a	8-Dec	13:37	1800	1700	630	1377	350	6.0	74		
6B-1	30-Nov	15:41	670	1400	1500	1190	320	2.9	65	17p	
6c	8-Dec	13:22	260	220	520	333	270	3.9	74		
6d	8-Dec	13:50	3200	1200	2800	2400	310	6.7	74	19p	
6e	8-Dec	13:35	2200	2400	2800	2467	330	9.3	74	20p	
7A	9-Dec	9:10	160	240	270	223	30	4.0	56		
11	4-Dec	15:45	250	110	147	169	100	3.3	75		
11A	4-Dec	15:41	270	570	540	460	85	2.8	75		
11A	9-Dec	10:20	240	220	180	213	340	3.5	56		
11a	9-Dec	12:26	280	440	130	283	360	8.6	56		
11B	4-Dec	15:36	520	500	570	530	80	3.6	75		
11B	9-Dec	10:19	160	180	180	173	10	5.0	56		
11b	9-Dec	12:29	170	120	150	147	10	3.7	56		
11D	4-Dec	15:00	190	170	140	167	90	3.9	75		
11G	9-Dec	10:09	1008	610	1116	911	30	2.3	56		
11H	8-Dec	14:26	540	620	570	577	350	2.1	74		
11H	9-Dec	10:12	580	580	730	630	20	11.1	56	32p	
11I	8-Dec	14:30	580	610	200	463	10	3.2	74		
11i	9-Dec	10:25	510	710	790	670	350	3.8	56	34p	
11i	9-Dec	12:23	500	590	380	490	360	7.0	56	35p	
11J	9-Dec	10:28	500	490	550	513	360	4.0	56	36p	
11k	9-Dec	10:33	580	720	670	657	30	2.2	56		
11k	9-Dec	12:20	290	510	320	373	350	5.5	56		
11M	4-Dec	15:50	560	490	400	483	85	2.9	75		
11N	4-Dec	16:09	210	510	530	417	65	5.7	75		
6b	8-Dec	13:25	520	2600	1800	1640	300	3.4	74	41p	
6B-2	30-Nov	6:18	1100	1400	580	1027	320	3.4	51	42p	
11	30-Nov	7:16	2000	2400	400	1600	340	2.4	51		
11	8-Dec	14:28	1400	2000	1200	1533	320	3.9	74		
11	9-Dec	10:30	520	530	550	533	360	4.2	56		
11A	8-Dec	14:22	520	550	520	530	360	8.4	74		

note: shaded areas; 32p, 34p, 35p and 36p line up to include the Polish Pond inlet area only, 300' W, from 320'

46

avg 810  
med 555

avg	613
med	248

**ASB Measurements - no models, potential for some background concentration from Pol Pond**

MAP LOC	2001 DATE	SAMPLE TIME	H <sub>2</sub> S ppb				Wind Data		Temp °F	Model	RATE Lbs/Hr
			Readings			avg	A°	mph			
7a	8-Dec	13:14	400	340	210	317	270	7.7	74		
7b	8-Dec	13:18	730	670	440	613	300	6.9	74		
7B	9-Dec	9:12	138	270	500	303	50	2.7	56		
11E	30-Nov	7:25	46	30	30	35	320	1.9	51		
11H	4-Dec	15:15	1300	2700	1700	1900	75	4.1	75		
11I	4-Dec	15:20	430	260	300	330	75	5.3	75		
11J	4-Dec	15:23	290	500	520	437	75	2.3	75		
11K	4-Dec	15:26	270	280	210	253	80	5.2	75		
11L	4-Dec	15:29	170	120	120	137	80	2.1	75		
10			avg				481	med		317	

**Clarifier Measurements - no models, potential for background concentration from Ash Pond**

MAP LOC	2001 DATE	SAMPLE TIME	H <sub>2</sub> S ppb				Wind Data		Temp °F	Model	RATE Lbs/Hr
			Readings			avg	A°	mph			
3C	30-Nov	7:01	120	260	190	190	45	3.9	51		
4F	8-Dec	14:04	140	150	120	137	330	8.2	74		
10	2-Dec	6:42	14	12	12	13	10	2.6	45		
10E	2-Dec	6:48	150	130	44	108	0	2.4	45		
10e	9-Dec	11:48	380	360	170	303	10	7.1	56		
10f	9-Dec	11:52	48	59	8	38	350	4.3	56		
11D	30-Nov	7:03	52	48	450	183	330	4.5	51		
11E	30-Nov	16:08	16	58	47	40	330	2.1	65		
11G	2-Dec	6:35	40	200	222	154	340	2.3	45		
9			avg				130	med		137	

**Ash Pond Area Measurements - no models**

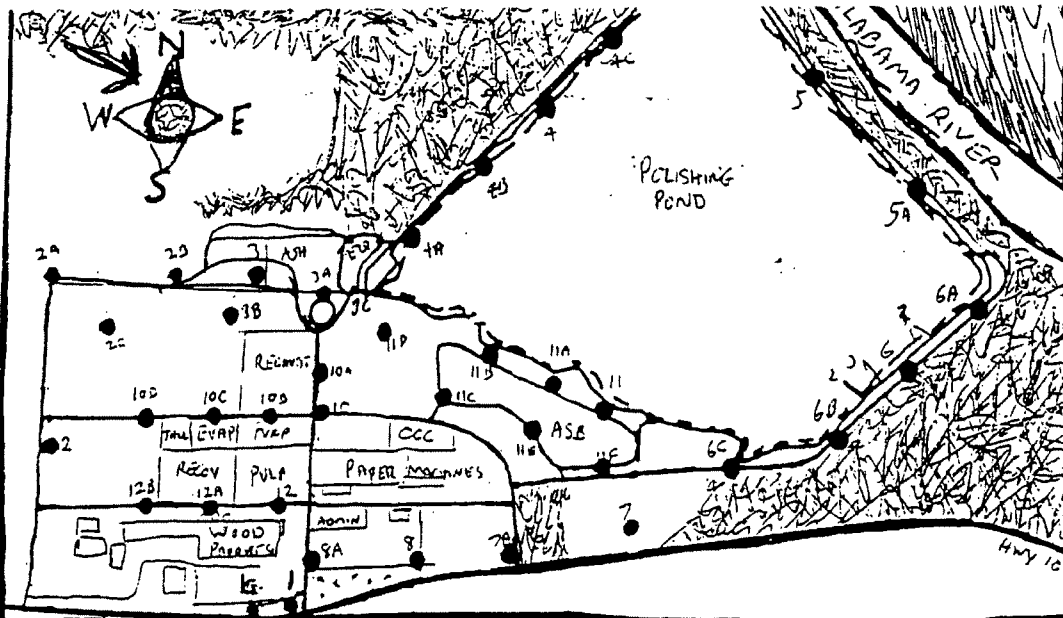
MAP LOC	2001 DATE	SAMPLE TIME	H <sub>2</sub> S ppb				Wind Data		Temp °F	Model	RATE Lbs/Hr
			Readings			avg	A°	mph			
3	9-Dec	12:39	9	5	4	6	360	3.3	56		
3A	30-Nov	16:12	8	9	4	7	40	3.0	65		
3A	8-Dec	15:21	6	16	50	24	260	5.2	74		
3a	9-Dec	12:36	41	25	78	48	350	7.1	56		
4D	8-Dec	13:59	60	54	130	81	310	3.6	74		
5			avg				33	med		24	





**PINE HILL TRS STUDY - PHASE II**

**Field Data**



Pine Hill Odor Study

DATE: 11/30/01

general weather conditions today

CLOUDY, COOL  
WINDS LIGHT  
+ VARIABLE

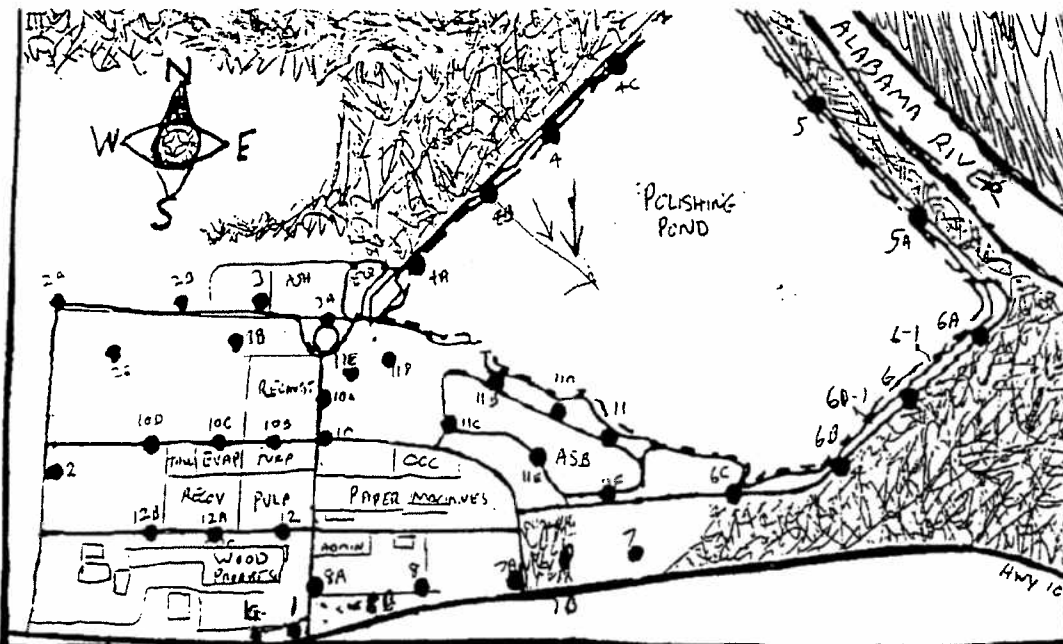
NW direction  
PRODOM

D

S = SWirling

POINT #	SAMPLE TIME	HYDROGEN SULFIDE - ppb				WIND		TEMP °F	Round: 1/2
		a	b	c	avg	dir	mph		
6C	0604	10	9	9		210	1.4	notes and observations: SLT MILD ASB FROM INLET PY	
6B	0615	260	580	540		40 S	0.2		
6B-2	0618	1100	1400	580	1027	320	3.4		
6A-3	0620	1400	1120	1006	1169	330	1.8		
6	0623	1500	1114	1200	1438	330	2.9		
6-2	0626	1400	1118	1900	1475	320	2.7		
6A	0630	580	570	1400		320	2.9		
5A	0634	510	420	660	520	210	2.7		
5	0640	68	5	5		215	1.7		
4C	0645						0		
4	0651	3	3	3		S	0.4	ROAD - MILD PT	
4B	0655	3	3	3			0		
4A	0658	3	3	3		0	1.9		
3C	0701	170	260	190		45	3.9	CLAR - STRONG	
HD	0703	52	48	450		330	4.5	CLAR	
11C	0708	11	9	9		330	3.0	KILN - UP	
11B	0711	54	23	27		350	5.7		
11A	0715	79	9	10		340	2.7		
11	0716	2000	2400	410		340	2.9	RIFFLER	
11E	0721	17	21	54		330	1.4	ACROSS ALL ASB	
11E	0725	46	30	30		320	1.9	INLET ASB	
3	0740	17	42	3		215	3.8		
3A	0743	3	6	8		240	3.6		
3B	0747	3	3	6		330	5.1		
6A	0750	3	3	3		330	5.1		
10	0753	3	3	3		355	6.9		
10B	0755	3	3	3		330	5.3		
10C	0757	3	4	4		325	4.4		
10D	0759	3	3	3		325	3.2		
12	0801	3	3	3		220	1.6		
8	0820	3	3	3		280	6.7		
8A	0822	3	5	3		260	10.1		
7A	0827	3	3	3		200	1.7		
7	0831	2	2	2		370	5.1	ENVA	
1a	0840	2	2	2		200	5.3		
2	0844	2	2	2		260	3.4		
2A	0847	3	3	3		240	6.4		
2B	0849	3	5	6		480	8.4		
2C	0852	3	6	6		270	2.8		

Data Entered SM



Pine Hill Odor Study

DATE: 11/30/01

general weather conditions today

SUNNY, MILD  
LT WINDS CLEAR  
SOME CUSTS

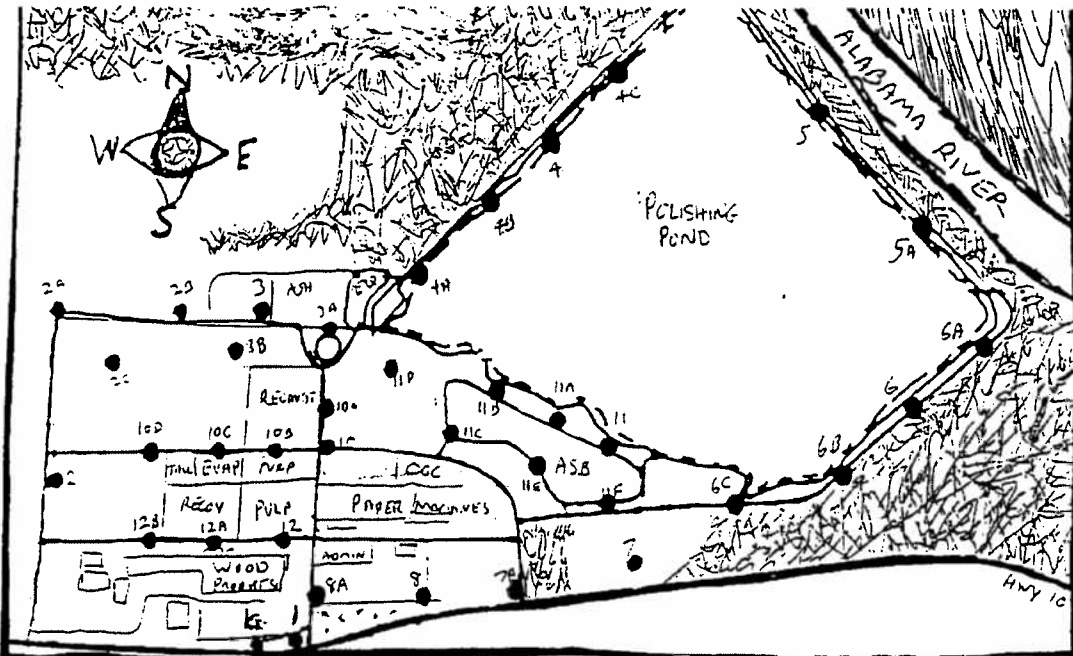
RAW plumes  
ALL W/NW  
LATER, AFTER  
1620 mm N

C

POINT #	SAMPLE TIME	HYDROGEN SULFIDE - ppb				WIND		TEMP °F	Round: 272
		a	b	c	avg	dir	mph		
7	1513	22	5	7		300	1.6	notes and observations: WINDS TWITCHY WIND SW TO N NO ODOOR NEAR SLT PP STRONG ORGANIC ODOOR, NOT H2S ↓ ↓ ↓ DEAD AIR PP ODOOR "  CLEAR - ONT OFF LINE WINDS DIRTY FROM CLEAR BUT PINE GOING WEST DUE TO WIND SWIRL IN GULL  STINKY ASB POND CROSS OL STAR - ORGANIC  MAIN STICKS MIL N only smell CLEAR ODOOR SLT CLEAR  THIN MIL	
11E	1513	120	5	54		350	1.7		
11C	1520	6	14	54		320	2.7		
11B	1523	7	5	7		0	2.5		
11F	1526	11	60	50		320	1.4		
11	1529	160	29	56		20	2.0		
11F	1532	120	23	22		320	4.0		
6C	1535	72	68	68		320	0.5		
6C	1538	580	520	680		300	0.4		
6A-1	1541	170	1400	1500		220	2.9		
6	1544	1500	1200	1300		350	5.1		
6-1	1546	660	1400	660		340	2.3		
6	1548	1500	460	570		320	2.5		
5A	1551	4	3	3			0		
5	1553	4	4	3		340	1.9		
4C	1556	3	3	3		330	0.1		
4	1558	3	3	3		340	0.6		
4B	1601	3	3	3		10	0.9		
4D	1604	23	20	120		350	0.2		
11D	1605	107	150	54		0	2.0		
11E	1608	16	58	47		320	2.1		
3A	1612	8	9	4		40	3.0		
3	1614	100	140	5		350	1.8		
2B	1618	3	3	3		0	1.3		
2A	1620	3	2	3		0	2.1		
2C	1623	8	5	7		340	1.0		
2	1626	3	3	3		10	0.7		
1	1630	3	3	3		320	2.7		
12	1634	18	28	27		70	2.8		
10A	1640	8	8	8		40	0.1		
10E	1642	5	5	4		270	1.2		
10D	1642	4	4	3			0		
10	1645	18	29	15		10	1.0		
10A	1647	11	2	5		340	1.0		
8	1655	4	4	4		45	2.3		
8A	1700	15	15	10		340	2.2		
10B	1710	8	4	4		0	1.9		
7E	1711	56	230	200		0	1.2		

2

D.L. F. L. S. S. S.



Pine Hill Odor Study

DATE: 12/1/01

general weather conditions today

COOL, FOGGY  
NO WIND AT  
GROUND LEVEL  
FOG HEAVIER  
AT DAYBREAK

POINT #	SAMPLE TIME	HYDROGEN SULFIDE - ppb				WIND		TEMP °F
		a	b	c	avg	dir	mph	
6C	0646	300	300	350		320	0.2	
6B	0650	350	400	420			0	
6A	0652	400	350	540			0	
5A	0657	350	350	310			0	
5	0659	4	12	28		40	0.2	
4C	0659	1	1	1		200	0	
4	0659	0	0	0			0	
4B	0659	1	1	1		350	1.1	
4A	0659	1	1	1			0	
11D	0659	180	110	26		60	0.2	
11E	0625	240	140	19			0	
11F	0628	330	230	190		320	0.2	
11	0630	250	240	190		240	0.5	
11A	0634	32	77	110			0	
11B	0634	52	57	49		320	0.5	
11C	0634	21	35	48		320	0.1	
7	0634	15	14	12		240	0.6	
7A	0634	8	10	10			0	
10	0656	5	3	3		260	1.4	
10A	0659	3	3	3		260	1.4	
10B	0700	7	7	2		220	0.5	
2	0704	2	2	1			0	
2C	0707	2	2	2		320	1.2	
2A	0710	3	0	0		340	1.2	
2B	0713	3	0	0		350	0.3	
3	0715	11	2	11		0	2.0	
3A	0719	3	3	28		10	2.4	
3B	0723	21	14	14		340	1.0	
10A	0726	140	128	50		345	1.3	
10	0728	170	120	140		20	2.0	
10B	0731	8	8	8			0	
10C	0734	6	0	3		300	2.0	
10D	0736	4	4	3		60	0.9	
1	0741	11	12	11			0	
8	0824	180	140	190		30	1.0	
8A	0827	140	50	190		60	0.5	

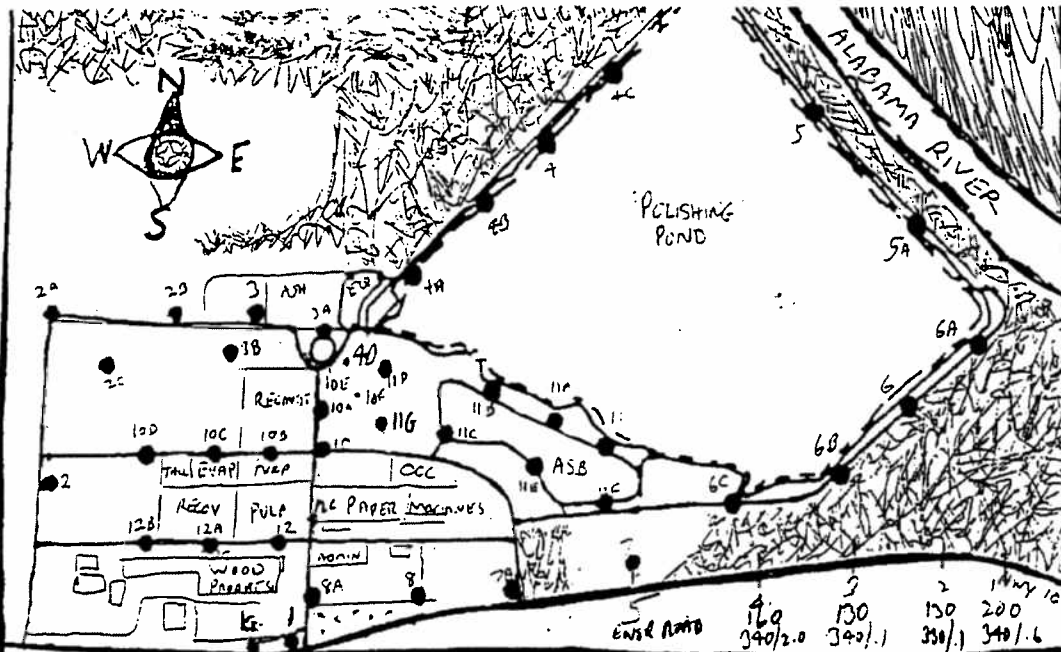
Round:  
notes and observations:  
ODOR PRESENT BUT  
NOT DIRECTIONAL

Near Insect - FWL

CLAMPING  
NO MILL NOISE &  
ANDINO PULP

ASB/PP  
PP

o.f. F.L. I SA



**Pine Hill Odor Study**

DATE: 12/2/01

general weather conditions today

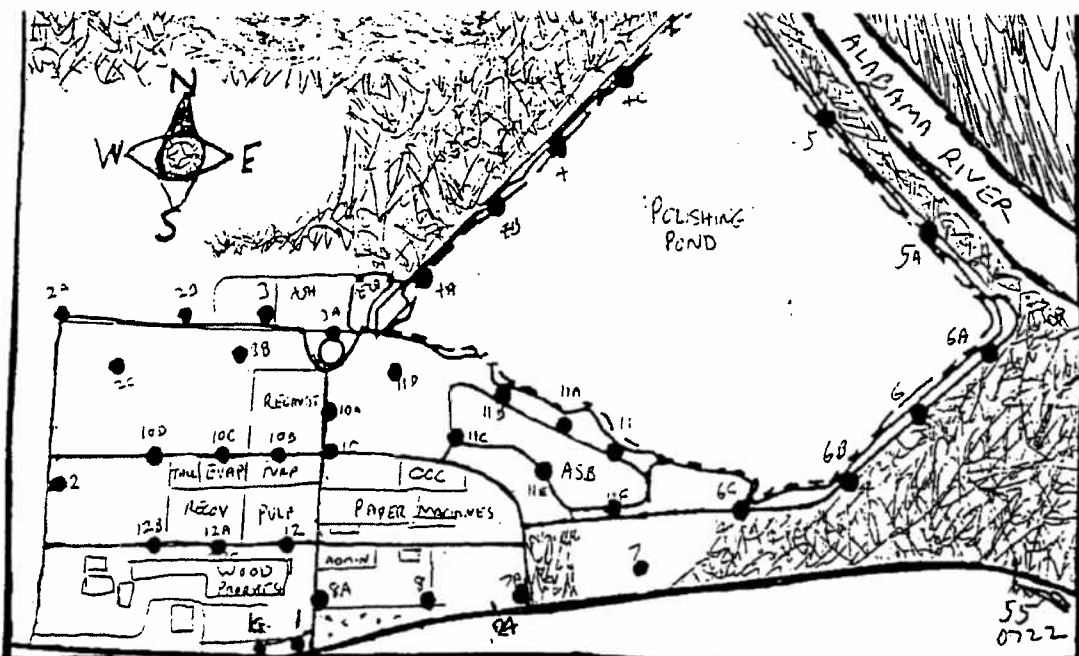
COOL, CALM  
 PREDM NOARING  
 WINDS

GROUND WIND  
 VERY LIGHT  
 + VARIATIC

AFTER DAWN BLOK  
 CONTINUE CLOUDY  
 - COOL

POINT #	SAMPLE TIME	HYDROGEN SULFIDE - ppb				WIND		TEMP OF	Round: 1/1
		a	b	c	avg	dir	mph		
7	0533	155	260	310		50	0.1	47	notes and observations: ENSR - 56
6C	0543	380	230	190			0		DEAD AIR ALONG TRACES
6B	0540	190	510	330			0		DEAD CALM
6	0547	170	520	330			0		SNOOZE - MOVES 20m
6A	0550	950	510	750		320	0.5		
5A	0556	0	4	4		10	0.2		
5C	0558	4	4	2		320	0.2		
4C	0602	0	0	0			0		
4	0604	0	0	2		20	0.6		
4A	0605	2	2	2		0	0.1		His smell
4A	0610	340	210	240		250	0.1		CHALK
4D	0615	110	350	350		240	0.9		MILL
4D	0617	43	43	32		270	0.1		
11B	0623	110	98	147			0		
11A	0625	110	83	100		350	0.5		ACROSS ASB
11	0627	110	110	150		350	0.9		
11F	0633	140	140	130		10	3.4		11A OLD OUTFALL
11B	0635	40	200	222		340	2.3		11 RIFLER
11C	0638	210	230	250		280	1.7		
11E	0642	12	12	12		10	2.6	1A	
11E	0645	9	9	9		0	3.8	1A	
10E	0649	150	130	44		0	2.4	1A	CHALK DIRECT - 10E/10F
10E	0651	21	53	52		350	1.2	10F	FURTHER DOWN
3B	0654	58	52	50		320	0.6		ASH PANS OUTFALL
3	0700	3	3	5		350	1.7		
2B	0702	2	2	3		280	0.5		
2A	0706	3	2	4		300	0.7		
2C	0708	2	0	2		270	0.6		
2	0711	2	2	2			0		MARK 6 ENSR STATION
12B	0715	2	2	2		260	2.5		1) 16R 0456093
12A	0717	2	2	2		260	3.2		UTM 3517859
12	0719	2	6	7		250	0.1		
12C	0723	14	16	17		0	0.8		2) 16R 0455870
10D	0724	2	1	1		310	1.5		UTM 3536968
10C	0726	1	1	2		320	2.4		
10B	0729	2	2	3		270	2.3		3) 16R 0455691
1	0735	2	2	3		230	1.8		UTM 3536946
8A	0740	3	3	3		250	2.0		
8A	0742	1	1	1		300	1.0		4) 16R 0455606
									UTM 3536933
									5) 16R 0455548
									UTM 3536926

4



Pine Hill Odor Study

DATE: 12/3/01

general weather conditions today

COOL, CALM

ALMOST NO CLOUDS

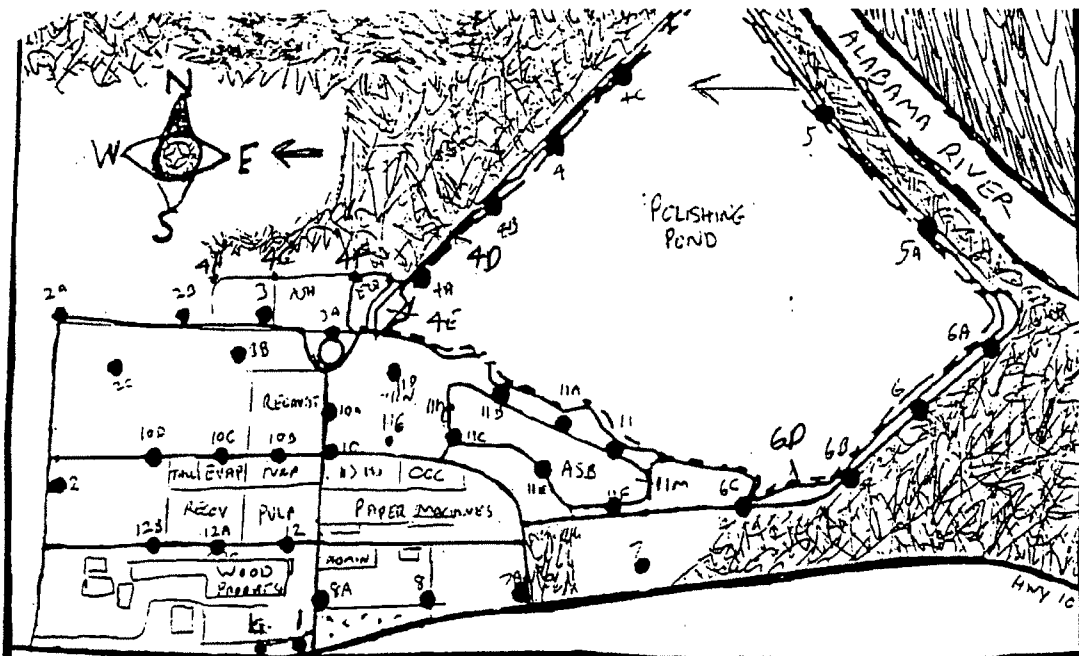
DEAD CALM

SLIGHT N GUSTS

POINT #	SAMPLE TIME	HYDROGEN SULFIDE - ppb				WIND		TEMP °F	Round: 1/2	notes and observations:
		a	b	c	avg	dir	mph			
7	0605	65	60	75			0			
6C	0606	73					0		TRUCK W/	
6B	0608	110		140			0		VAPOR SITTING OVER PP NOT MOVING OFF	
6A	0610	47	57	64			0			
5A	0615	140	140	140		350	0.3			
5B	0620	34	31	16			0			
4C	0625	0	0	0			0			
4B	0630	0	0	0		280	0.1			
4A	0635	0	0	0			0			
3B	0640	106	130				0			
3A	0645	110	75				0		SINKS LIKE PP	
2B	0650	420	450				0			
2A	0655	220	250				0			
1E	0700	6	4				0			
1D	0705	760	730			220	1.1		SINKS PPB	
1C	0710	590	430	540		380	2.4			
1B	0715	12	10	7		320	0.3		DRIVE E DOWN HWY 10 MINIMAL 200YD	
1A	0720	3	3	2			0			
8	0735	3	3	3		140	1.0			
12A	0740	3	3	2			0			
10	0745	2	2	6			0			
3A	0755	12	4	8			0			
7	0804	5	4	3			0		END NO WIND	







Pine Hill Odor Study

DATE: 12/1/01

general weather conditions today

FULL SUN 75

STEADY BREEZE

FROM E

B/C WINDY SUN

POINT #	SAMPLE TIME	HYDROGEN SULFIDE - ppb				WIND		TEMP OF
		a	b	c	avg	dir	mph	
7	1405	6	6	6		100	4.1	75
6C	1410	110	130	120		90	1.5	
6D	1411	11	8	8		125	2.5	
6E	1418	580	530	170		10	1.8	
7	1421	70	5	2		180	0.5	
6A	1423	118	510	200		350	1.1	
5A	1427	8	8	8		30	0.5	
5	1431	8	8	8		50	0.6	
4C	1433	67	4	4		90	3.0	
4	1439	770	720	130		95	4.3	
4D	1442	510	270	180		80	4.1	
4E	1446	520	540	210	423	90	3.5	
4A	1450	1098	1200	540	916	95	6.1	
4E	1457	520	340	411	490	100	4.4	
11D	1500	190	170	140		90	3.9	
11G	1510	120	150	500		70	3.6	
11H	1515	1300	2700	1700	1900	75	4.1	
11I	1520	430	260	300		75	5.5	
11J	1523	290	500	520		75	2.3	
11K	1526	270	280	210		80	5.2	
11L	1529	170	120	120		80	2.1	
11B	1536	520	500	570		80	3.6	
11A	1541	270	370	340		85	2.8	
11	1545	250	110	147		120	3.3	
11M	1550	560	470	400		85	2.9	
11F	1554	12	12	8		95	2.4	
11N	1609	210	510	530		65	5.7	
4E	1620	530	670	670		95	3.2	
4G	1623	1300	1400	1490	1397	95	4.9	
4H	1630	1200	1100	500		85	1.9	
2	1638	17	9	9		80	3.7	

Round: 1/1

notes and observations:

STRONG SOLAR RAD

PP ODR

PPAIN - TWING

FINELY WINDY + STEADY

SUNKOOLIC

DITTO - WINDY + STEADY + STRONG

WLPKIN SUNI NOW

ASB: PP

ACROSS ASB INCL R

11I @ CURVE OF STONER

MID OF STONER

11K @ END OF STONER

11L @ END OF STONER

LOW ROAD DATA 1600-1615

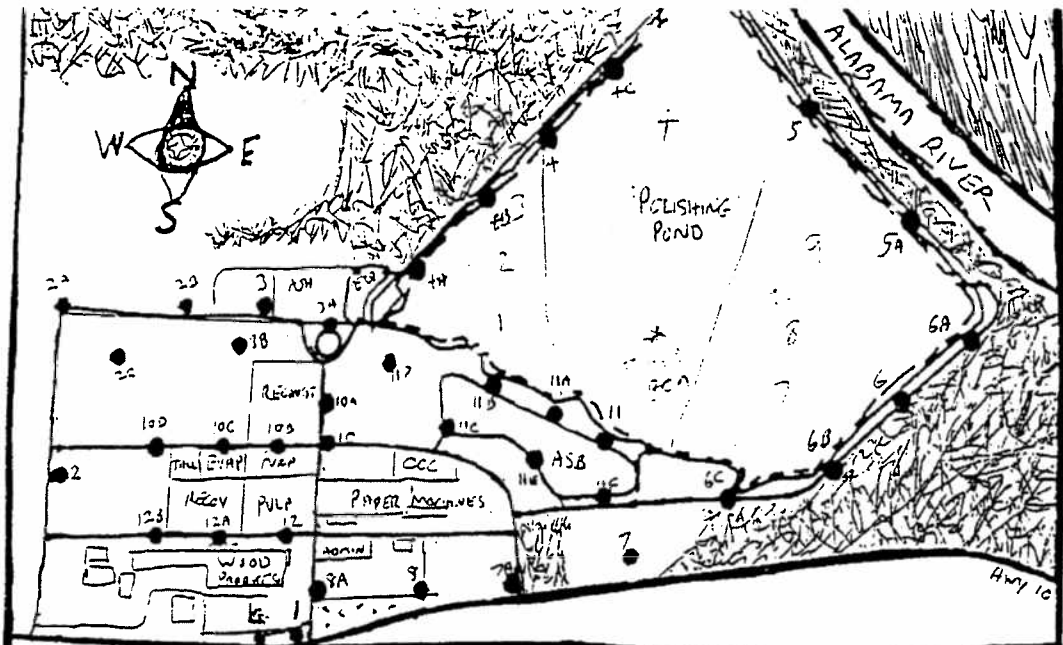
all pp

STRONG

at 1600 SM

7





Pine Hill Odor Study

DATE: 2/16/01

general weather conditions today

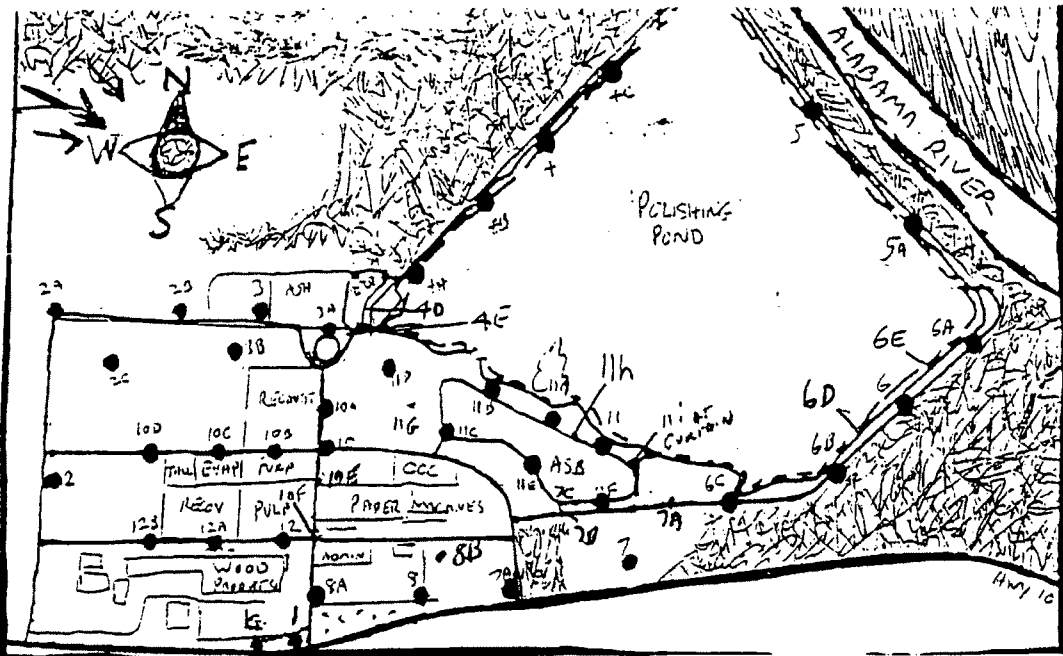
BRIEFLY  
SUNNY  
CLEAR  
WINDY  
SOME SMOG

POINT 500 /  
-  
SPACE - J - RAMA

POINT #	SAMPLE TIME	HYDROGEN SULFIDE - ppb				WIND		TEMP °F	Round: notes and observations:
		a	b	c	avg	dir	mph		
92	1128	1800	920	940		220	3.7	76	16R0456425-3537822
92b	1139	570	200	880		210	1.2		16R0456373-3537874
95b	1153	780	950	500		220	1.8		"
96	1208	540	580	1400		280	2.1		0456333-3537777
6	1229	560	650	1100		180	4.0		0456034-3538227
6a	1239	880	210	320		190	7.3		0455934-3538370
6b	1253	200	140	410		140	1.5		0455784-3538548
5a	1315	1100	750	860		140	1.9		0455426-3538188
4a	1338	420	750	510		180	2.5		0455426-3538232
4b	1401	350	300	460		200	2.5		0455229-3538008
4c	1408	350	410	830		190	1.9		045534-3537911
4d	1412	110	420	850		200	1.4	80	"

PM smell with pond

8



Pine Hill Odor Study

DATE: 12/7/01

general weather conditions today

Cloudy 90%  
 gusty winds  
 from S/SW  
 to W or NW  
 mild w/  
 sun breaks

STABLE D

GOOD MODEL DATA

S - A - P - L - E  
 ↓  
 ISO  
 \*  
 PP  
 \*

POINT #	SAMPLE TIME	HYDROGEN SULFIDE - ppb				WIND		TEMP °F
		a	b	c	avg	dir	mph	
7	1311	12	60	20		280	6.6	
7a	1314	400	340	210		270	7.7	
7b	1318	730	670	440		300	6.9	
7c	1320	2100	1270	1300		280	4.9	
6c	1322	260	220	520		270	3.9	
6D	1325	520	2600	1800	1640	300	3.4	
6	1330	3200	1200	2800	2400	310	6.7	
6E	1332	2800	1500	2300	2200	360	7.0	
6A	1335	2200	2400	2800	2200	330	9.3	
5A	1337	1800	1700	630	1377	350	6.0	
5	1343	6	7	2		20	2.7	
4c	1348	4	5	5		300	2.5	
4	1352	5	5	5		310	1.3	
4B	1355	4	5	4		300	0.3	
4A	1357	4	4	4		270	2.5	
4B	1359	60	54	130		310	3.6	
4E	1403	120	160	120		350	5.3	
4F	1404	140	150	120		330	8.2	
11D	1407	70	23	53		330	3.2	
11G	1411	16	16	17		320	2.9	
11E	1416	6	6	7		280	5.2	
11B	1418	52	14	15		340	4.0	
11A	1422	520	550	520		360	8.4	
11h	1426	540	620	570		350	2.1	
11i	1428	1400	2000	1200	1533	320	3.9	
3a	1521	6	16	50		260	5.2	
3	1524	2	3			270	4.2	
2B	1527	4	4			290	2.9	
2A	1530	4	4			280	4.0	
2C	1533	3	3			260	3.4	
2	1535	3	4			260	1.1	
10D	1538	4	4			270	3.7	
10A	1540	6	6			300	3.8	
10E	1542	7	6	7		320	6.2	
10F	1544	16	16	13		300	3.8	
10E	1547	8	2			300	0.8	
8B	1621	52	6	5		280	1.9	

Round: 1/2

notes and observations:

PP - off in the area  
 NASTY

NOT AS BAD  
 FRESH AS A DAISY

SMELLS CLEANER  
 ASH

ASH - MORE +  
 CLEAR DIRTY INSIDE NO  
 CLEAR - outside, faint S2P G -  
 clear - w/plan - EDGE AT TIMES  
 SET CLEAR/DIRTY  
 GOOD CLEAR SMELL OUT OFF  
 RIGHT OVER OFFFALL

PP  
 RIFF

PP (RECENT) ↓  
 FULL SUN AGAIN - LOW ANGLE

LIR SAIL

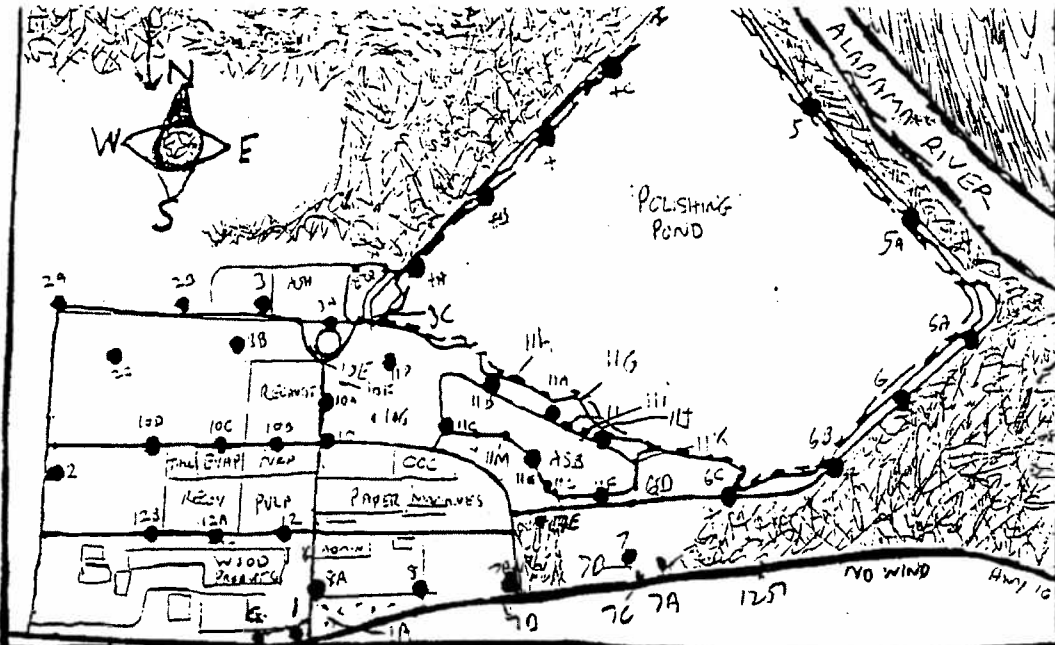
WINDS  
 BECOME  
 LIGHT + VIB

0456512  
 353 7746

0455293

353 7746

9



Pine Hill Odor Study

DATE: 12/9/01

general weather conditions today  
 CLOUDY COOL  
 WINDY  
 LOW CLOUDS

D

POINT #	SAMPLE TIME	HYDROGEN SULFIDE - ppb				WIND		TEMP OF	Round: notes and observations:
		a	b	c	avg	dir	mph		
7A	0917	160	240	1370		30	4.0	PP	
7B	0917	138	270	500		30	2.7	+ ASB ODOR AT END	
7C	0917	200	340	240		20	2.3	P=ASB	
7D	0918	150	100	230		250	2.8	P.MILL ALONG RIVER	
10	0930	3	14	14		360	9.8	ENSA	
1	0957	230	200	140		360	2.3	PP - ASB 100	
6U	1001	500	420	580		310	2.2	PP	
11G	1009	1000	640	1110	911	30	2.3	PP	
11H	1012	580	580	730		20	11.1	PP	
11B	1019	160	180	120		10	5.0	↓	
11C	1020	240	220	180		340	3.5		
11D	1025	510	710	790	670	350	3.8		
11E	1028	500	490	550	513	360	4.0		
11	1030	520	530	530	533	360	4.2	R+PP - NOT THIS SOURCE - ORGANIC	
11K	1033	580	720	670	657	30	2.2	ASB+PP - NOT THIS SOURCE	
11F	1035	230	400	420		10	6.9	ASB+PP	
11L	1037	430	160	150		360	5.5	NOT GOOD	
11M	1041	240	240	190		360	5.9	STINKIER - SUMMER CLOUDY	
11N	1043	1400	2700	1140	1736	10	5.0	LESS PERSISTENT	
11O	1046	390	500	1110		10	3.8	CLAR	
11P	1048	380	360	170		10	7.1	NOT MUCH	
10F	1152	48	59	8		350	4.3	CLEAN - RICH CO-ODOR - C	
10G	1154	11	44	40		10	2.1	THIN MILK	
7A	1203	10	9	4		350	7.8	"	
7B	1206	9	16	28		10	4.8	"	
7C	1209	27	57	10		20	3.9	"	
7A	1213	69	64			340	1.3	"	
7B	1216	120	130	130		10	4.0	"	
7C	1220	290	510	320	373	350	5.5	"	
11P	1223	500	590	580	490	360	7.0	PP	
11A	1226	280	440	130	283	360	8.6	"	
11D	1229	170	120	150		10	3.7	"	
5C	1234	17	21			350	0.3	EQ POND	
5A	1236	41	25	78		350	7.1	ASH-E	
3	1239	9	5	4		360	3.3	ASH-W - STINKY	
12S7		222	120	180		360	2.1		

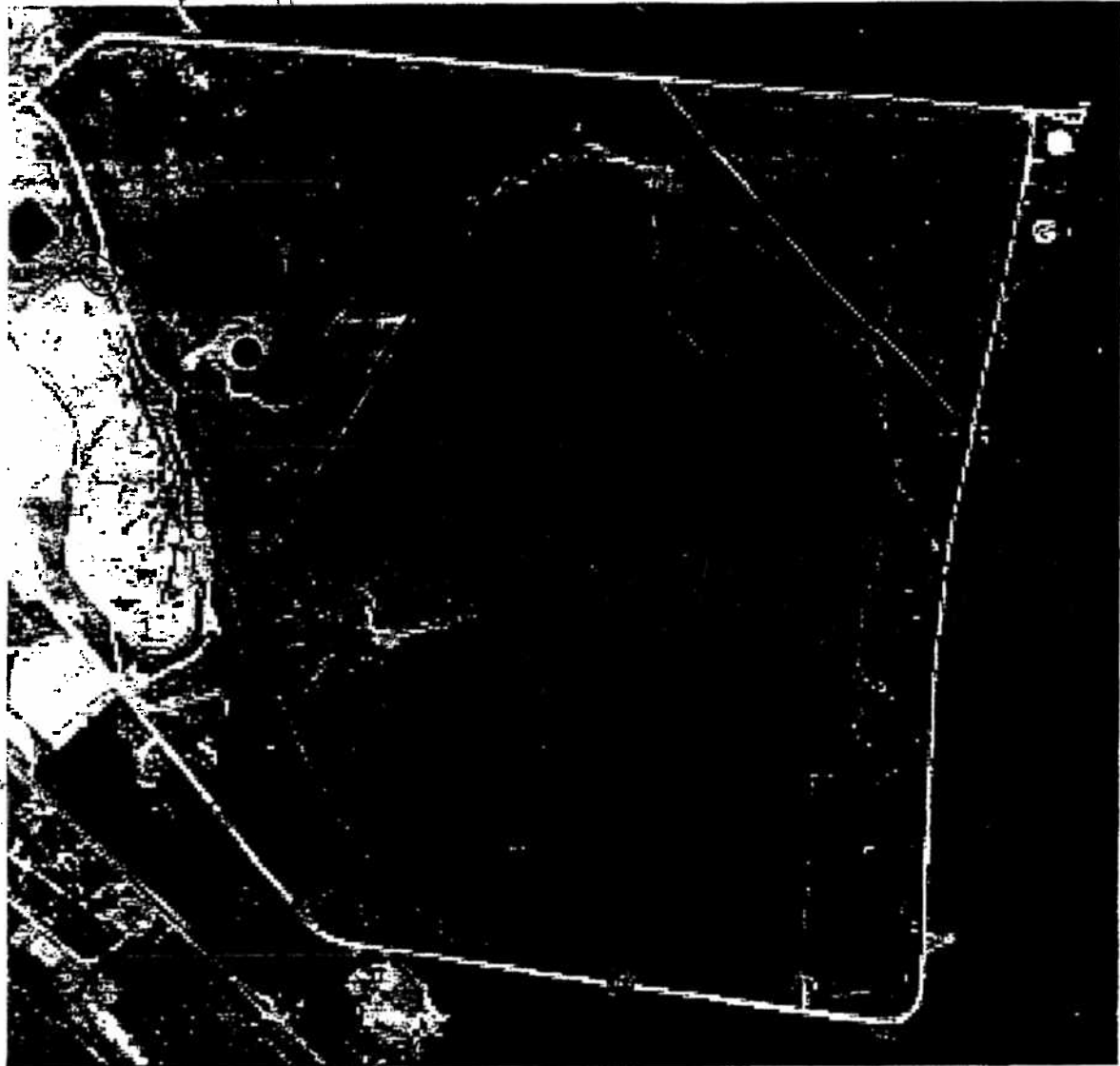
1-11

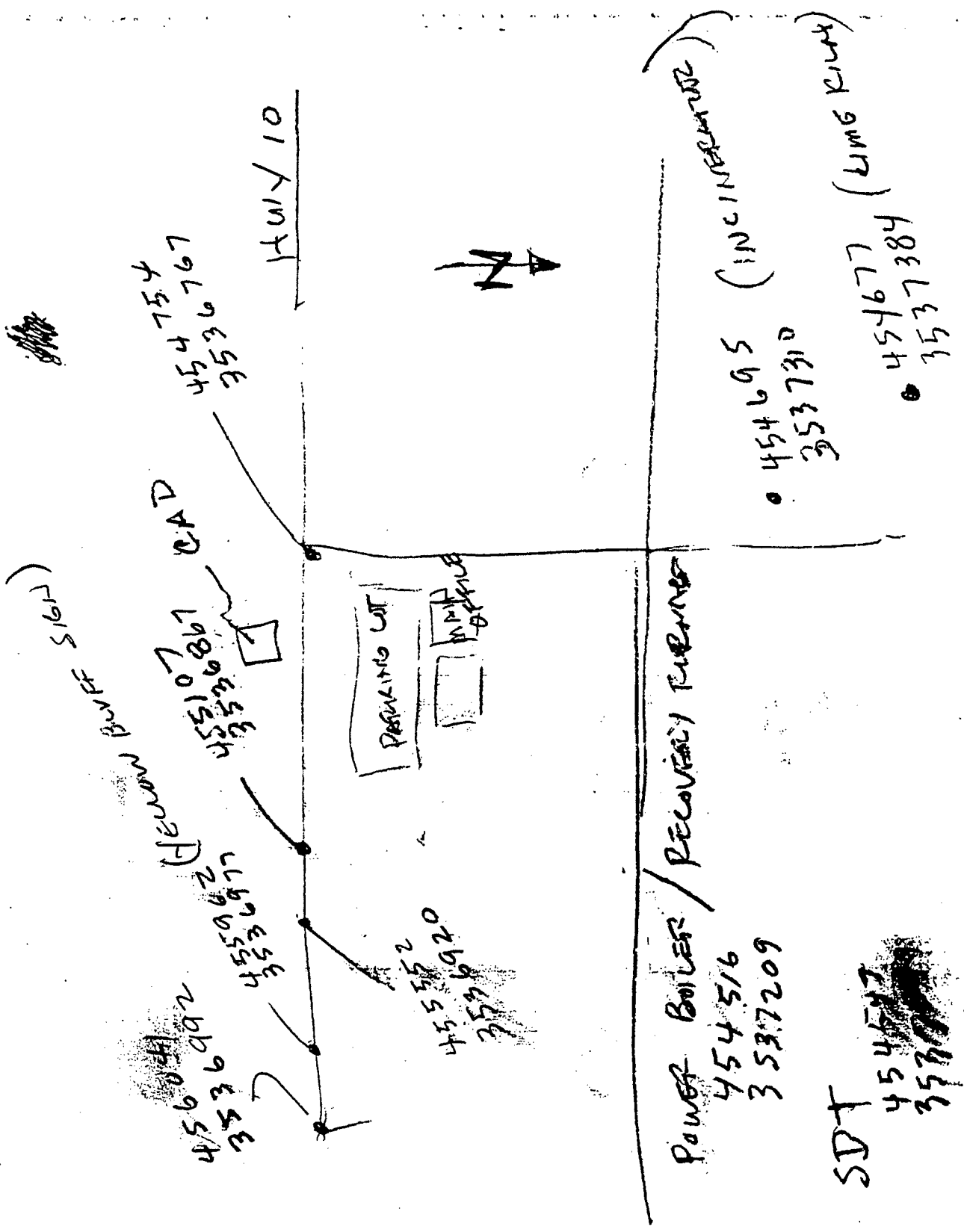
10

POND WW TESTING

→ WIND GUSTS

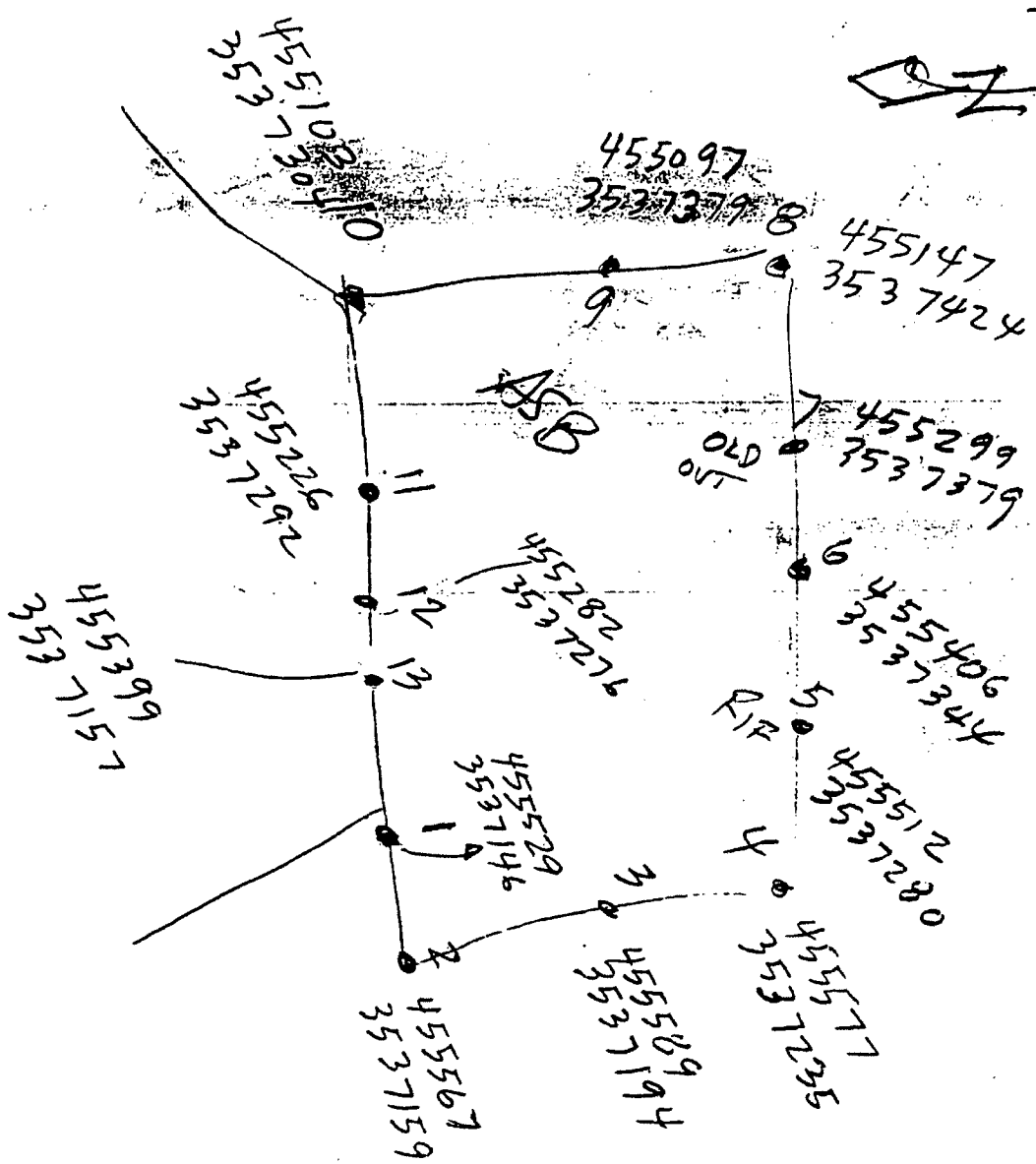
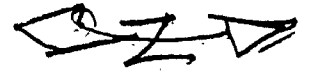
12/3  
VERY WINDY  
74°  
CALM WINDS  
FULL SUN  
1144 150 ppb 3 mph  
GUST  
1133 2.9 mg/L  
130 ppb H2S  
1139 - 200 ppb

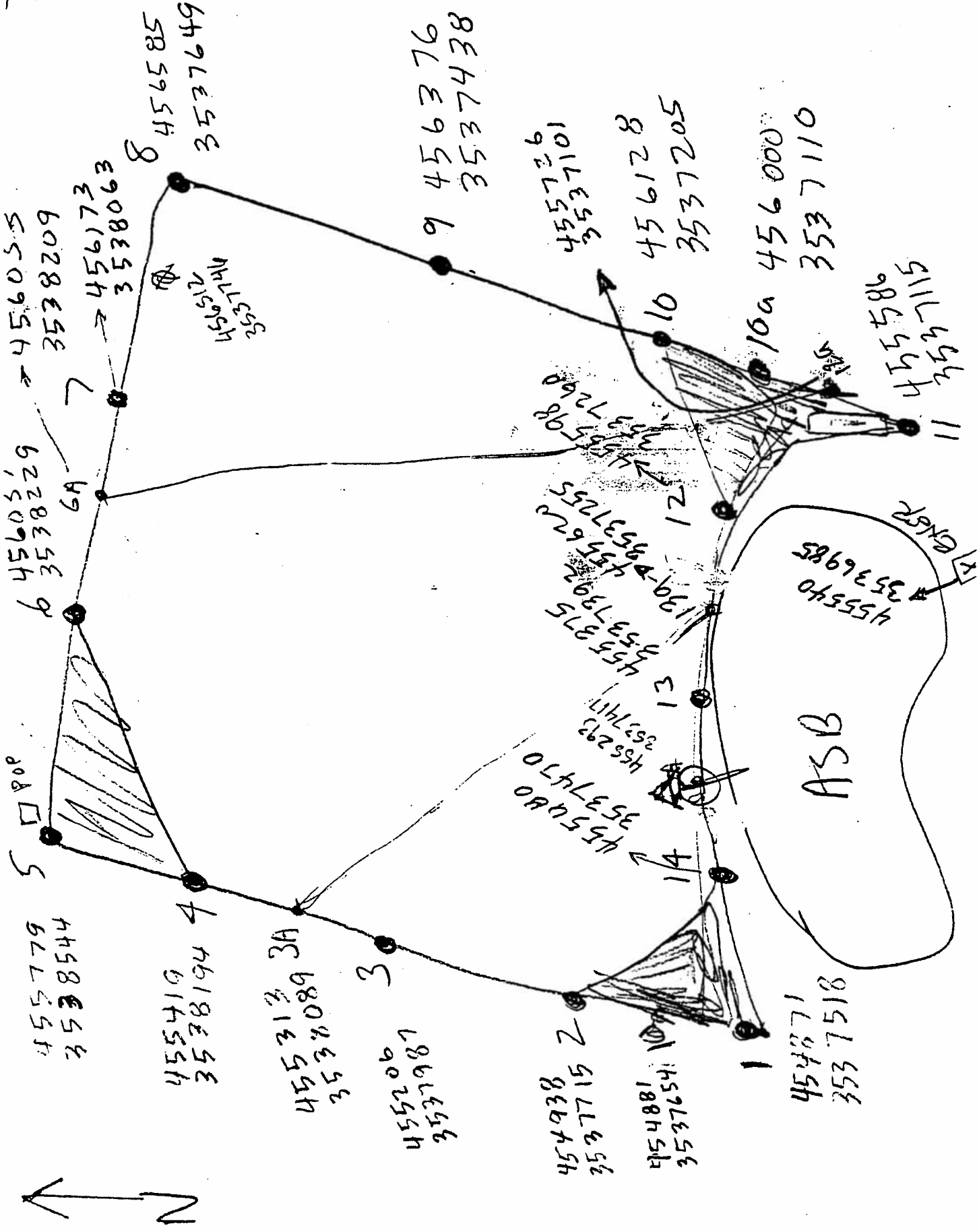




PLUMMADY  
CLASSIFIER

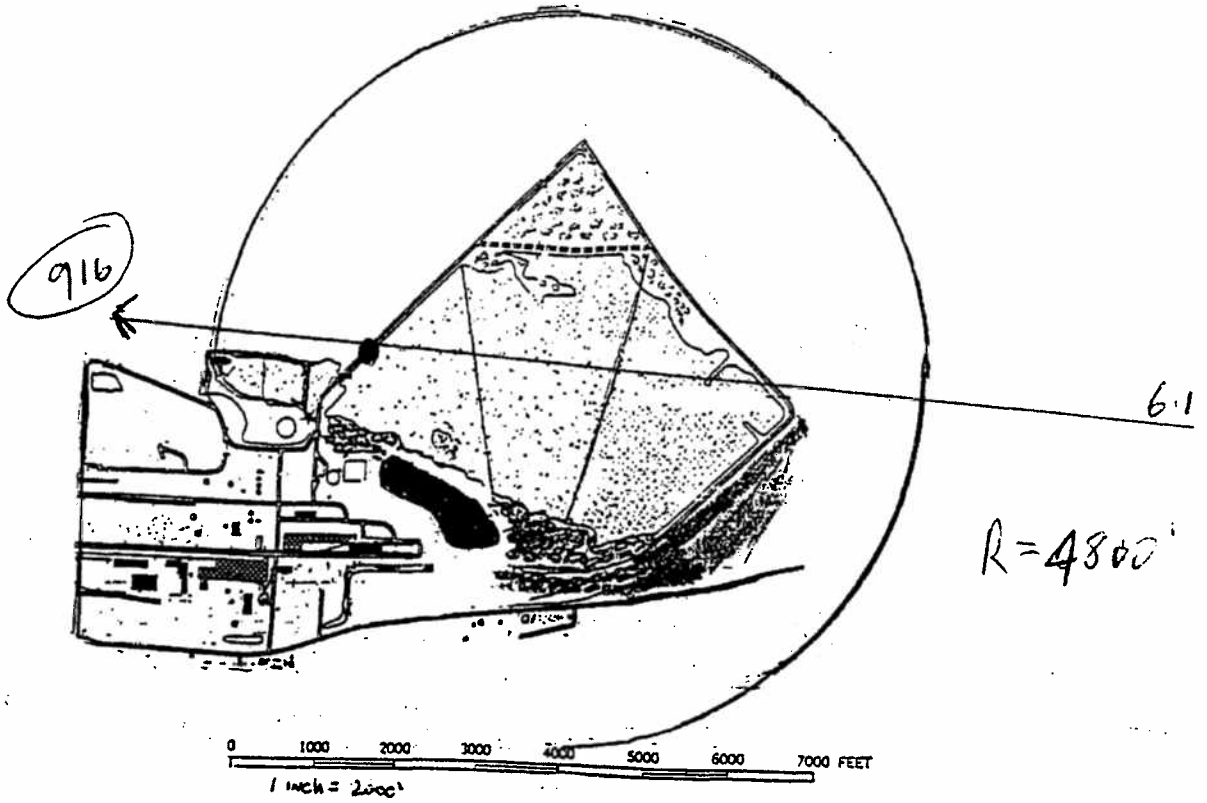
454751  
3537536







24

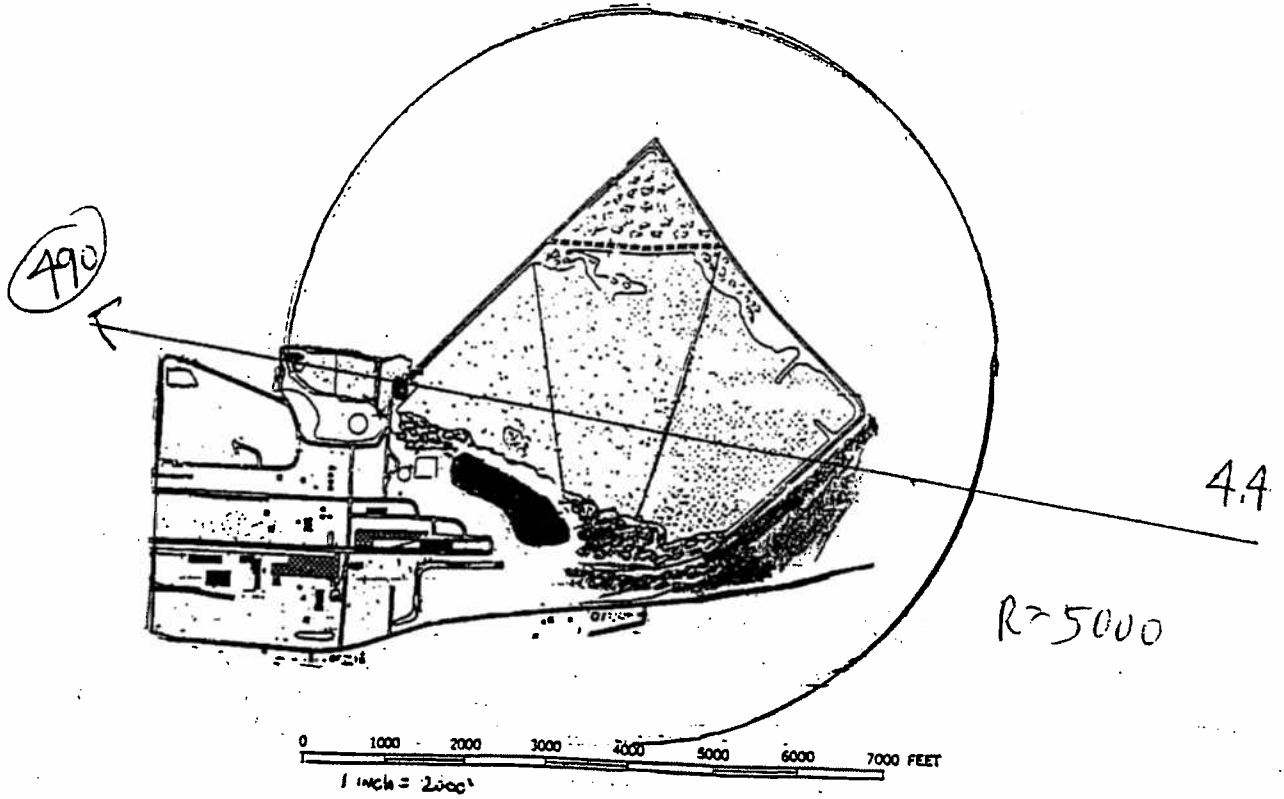


C





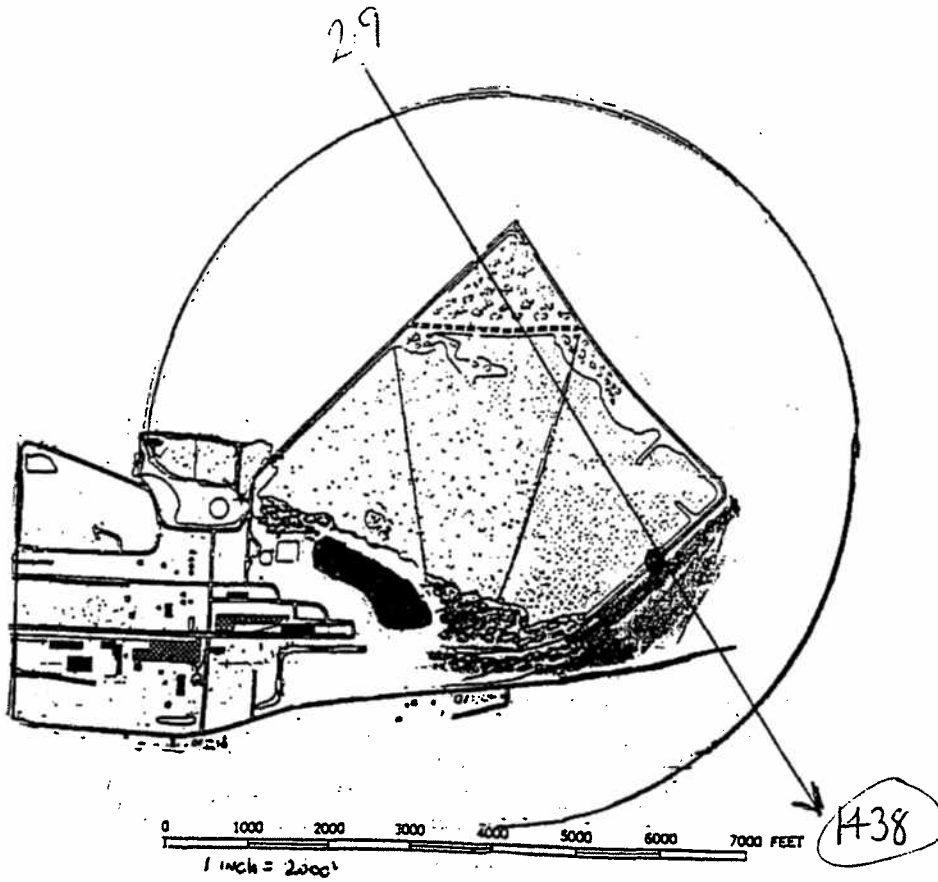
5P



C



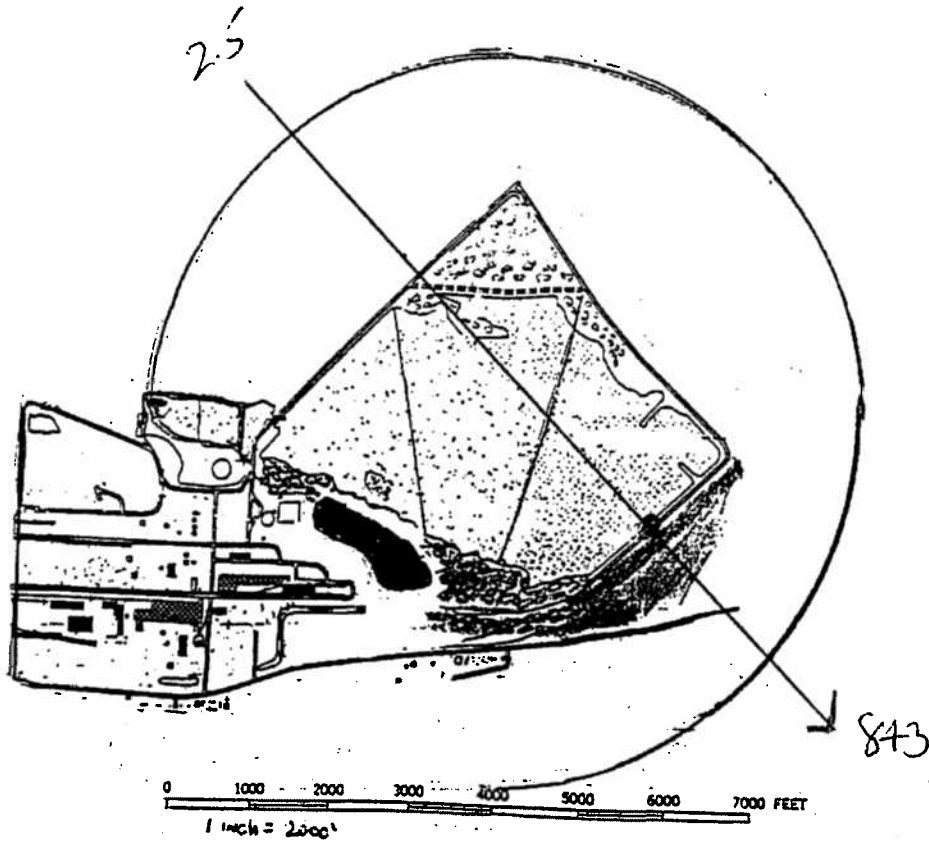
9B



D



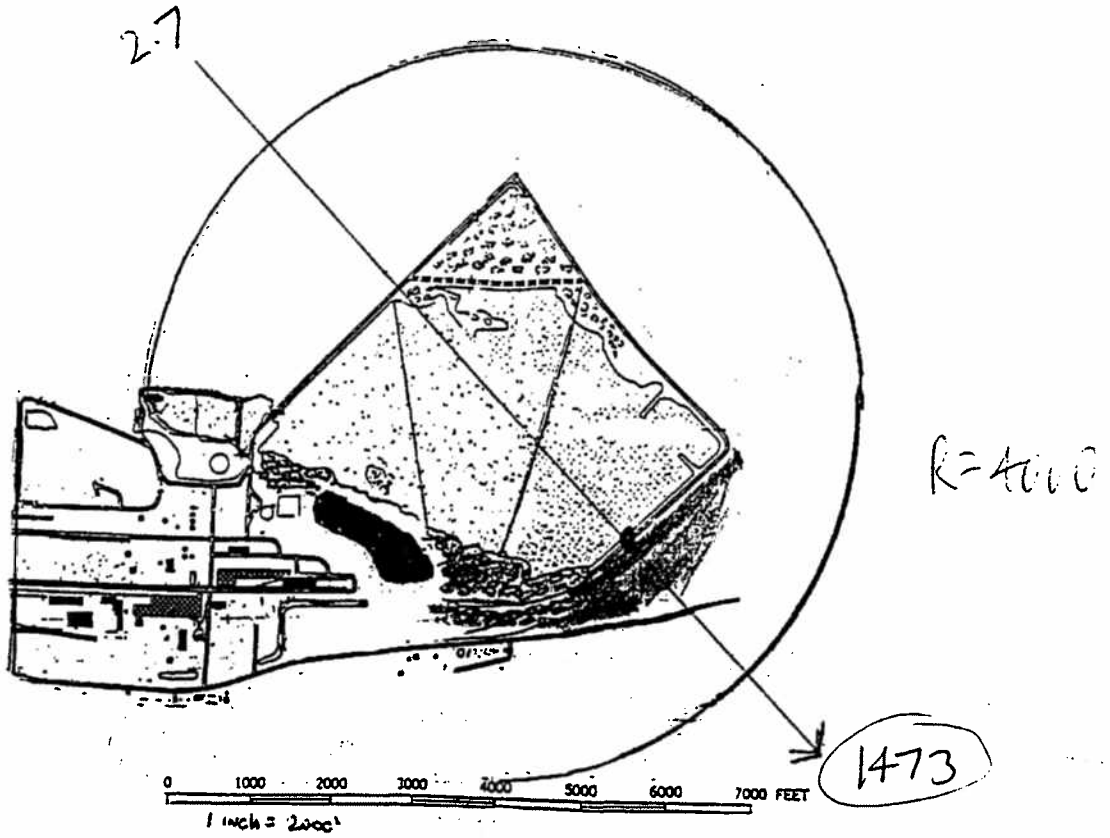
11p



D



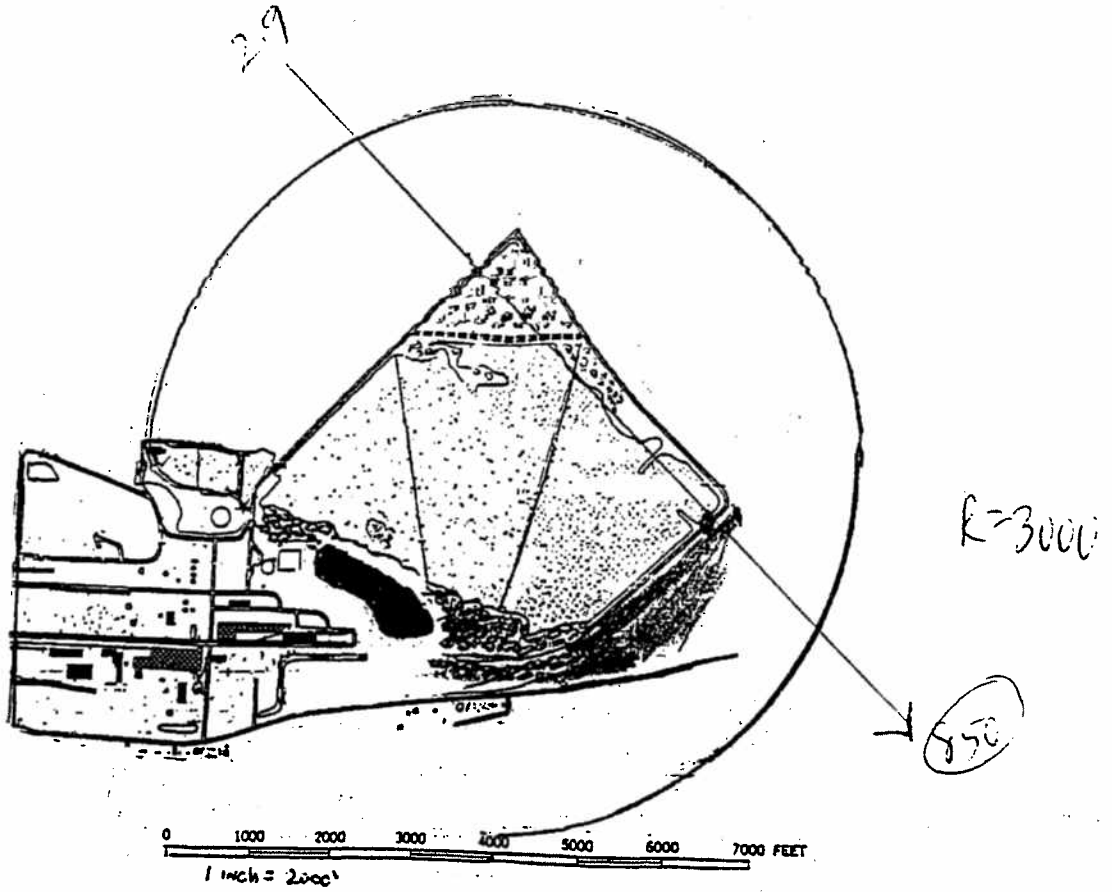
147°



D



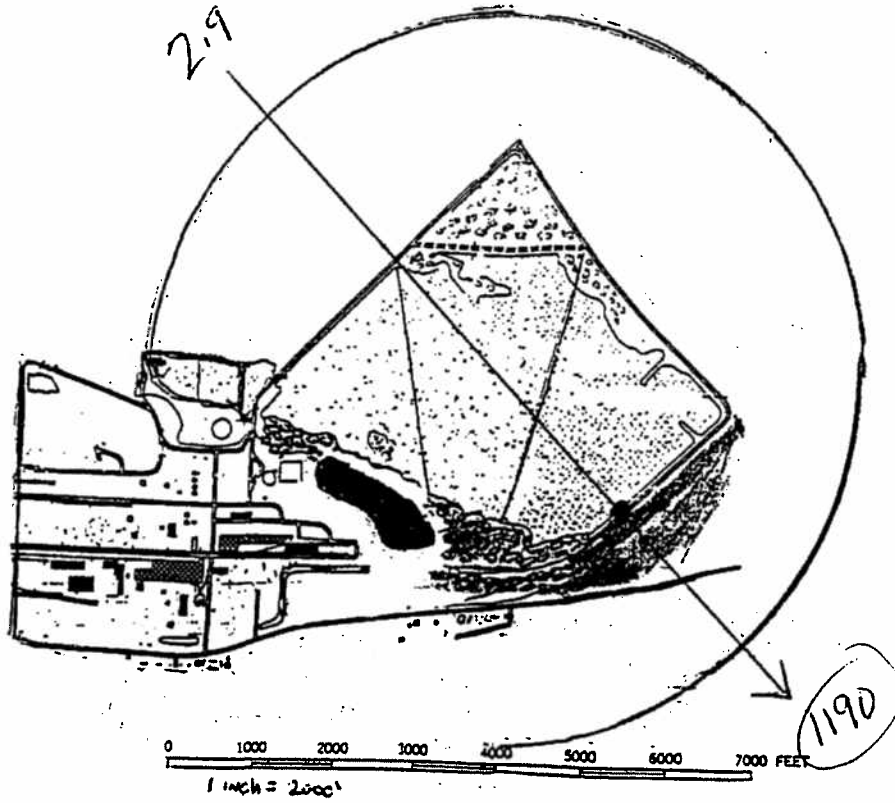
15p



D



17p

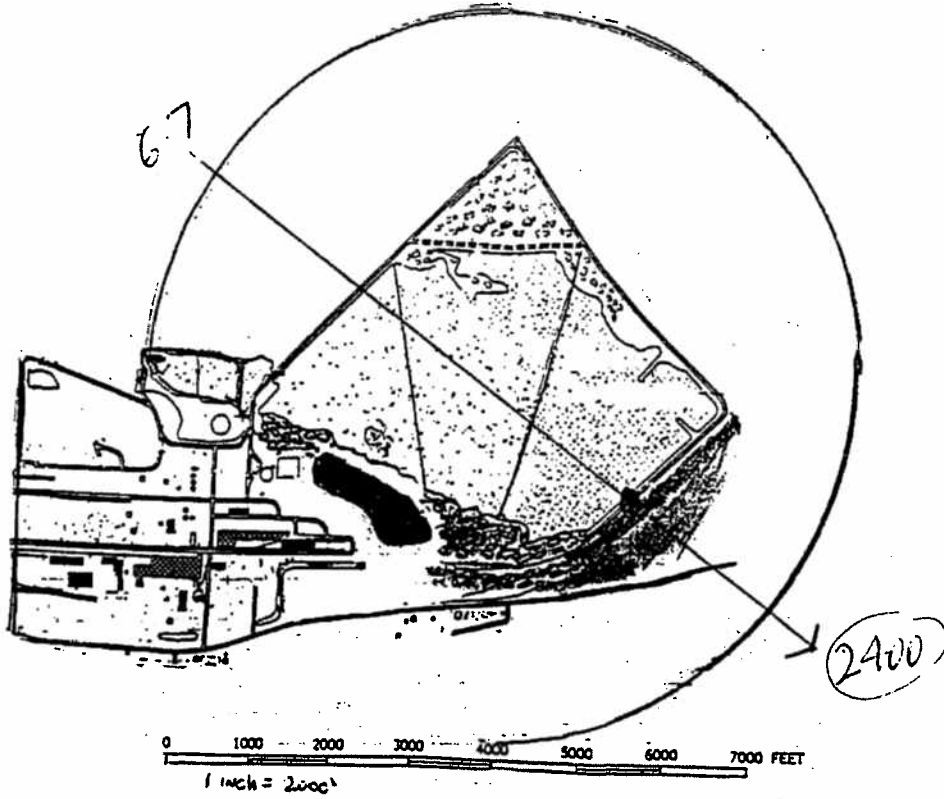


R=4000

D



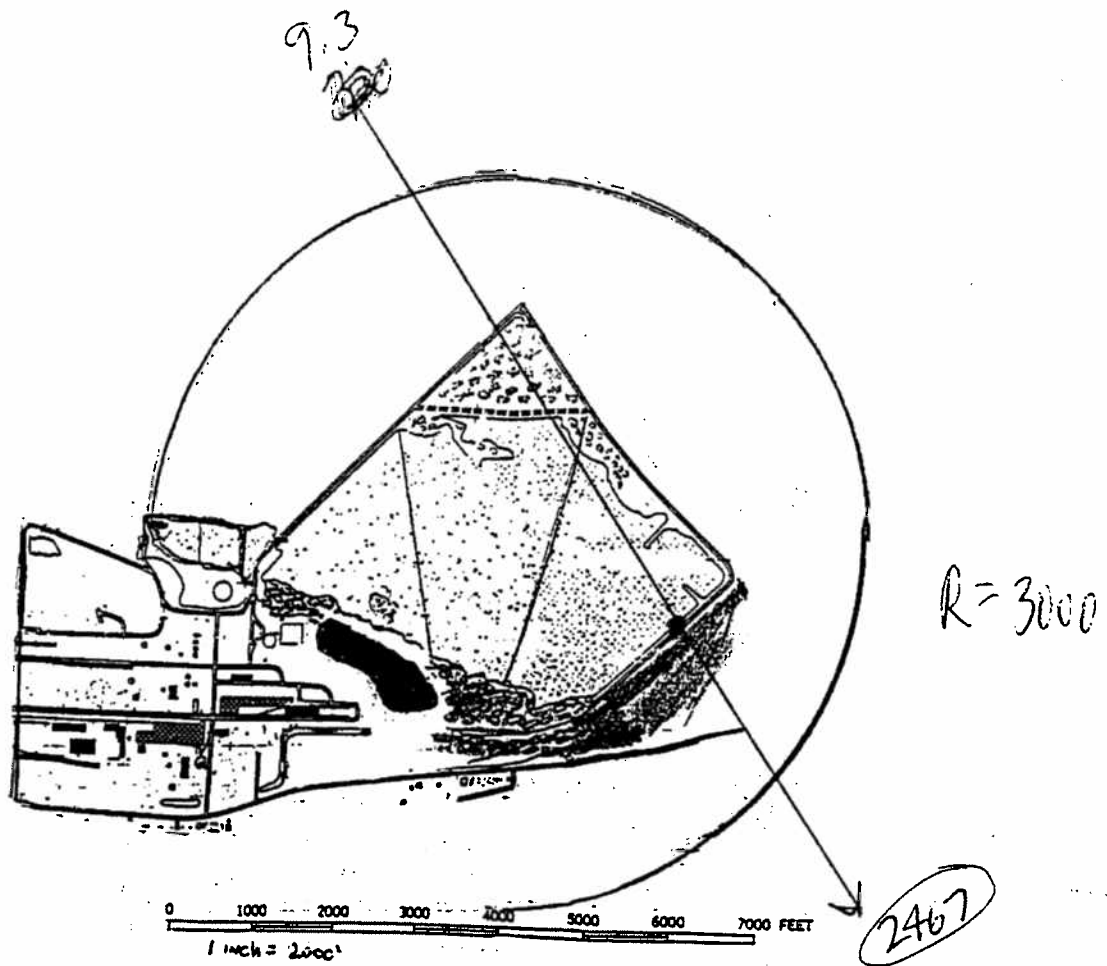
19P



C



20p

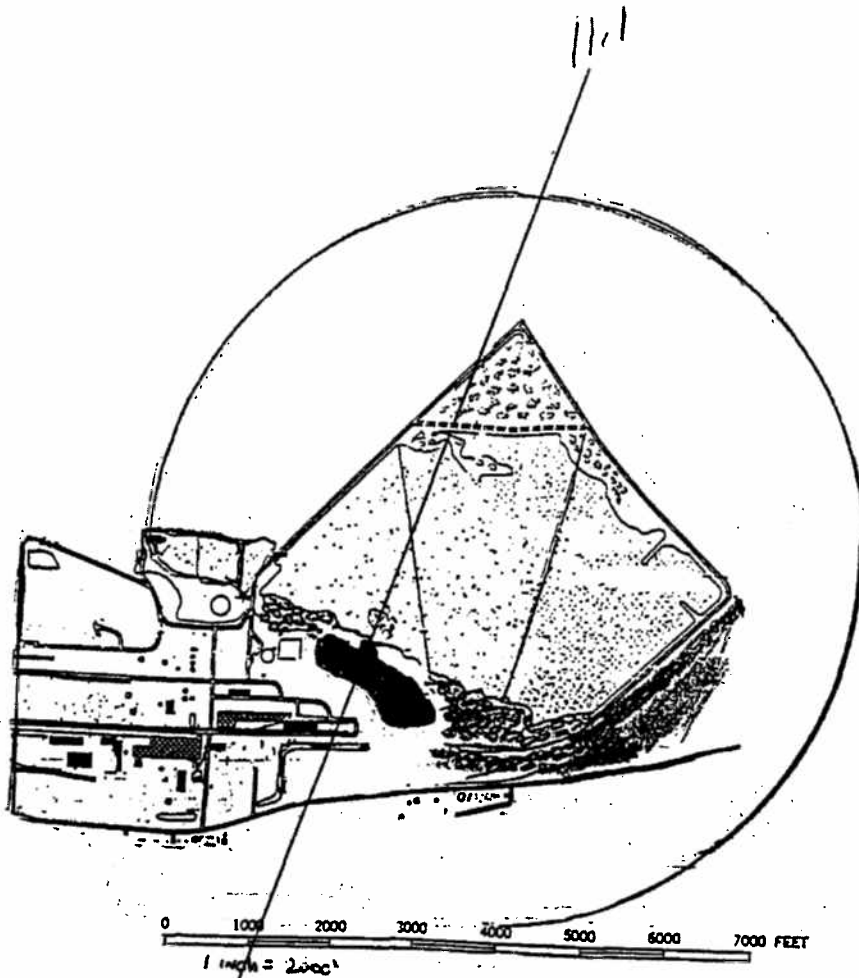


C





32p



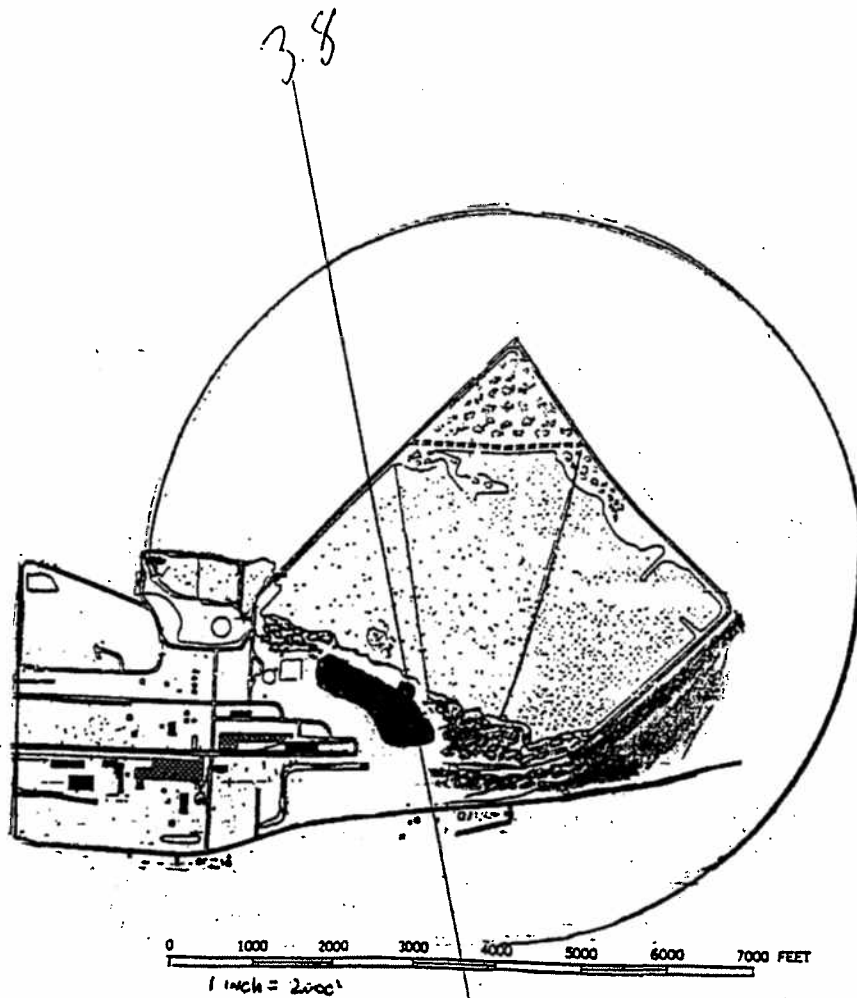
R=2550

630

INLET



31  
31



R=2400

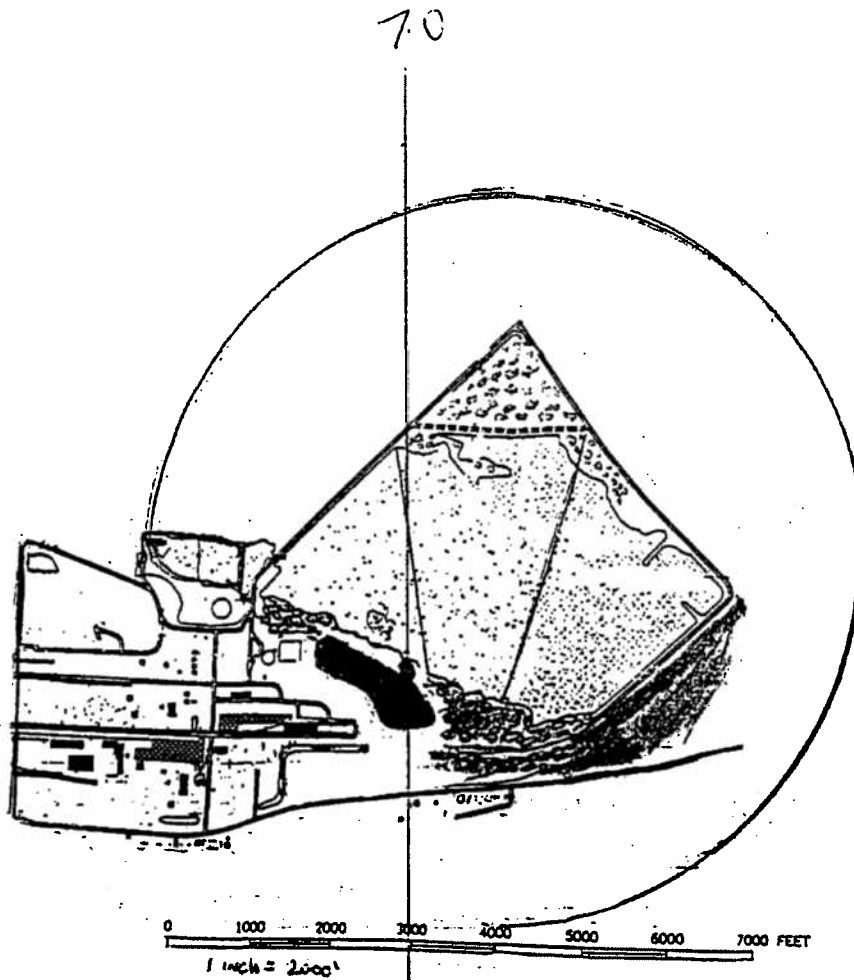
670

C

INLET



35p



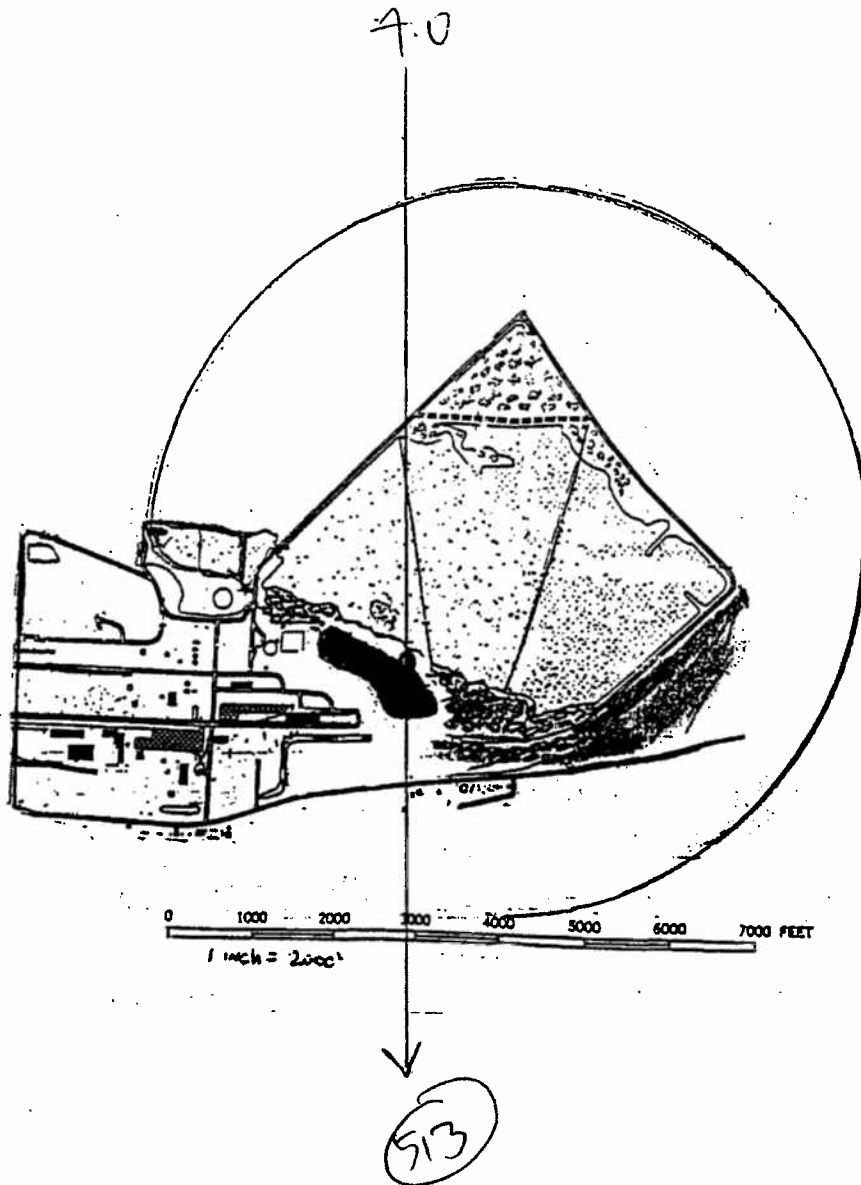
R=2900

490

INLET



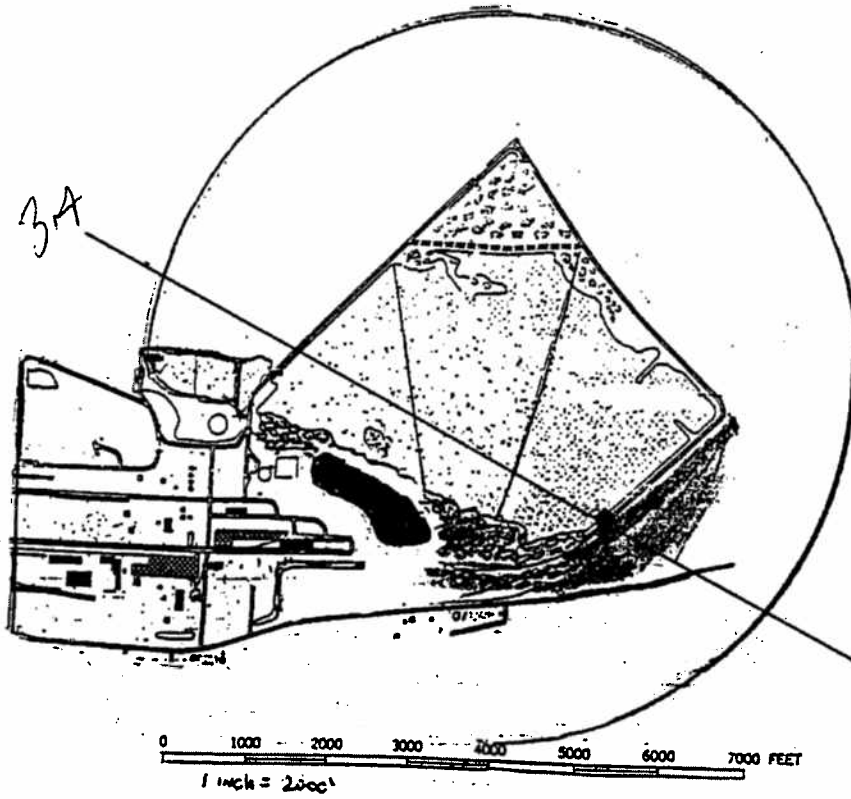
36p



INLET



41p



1640

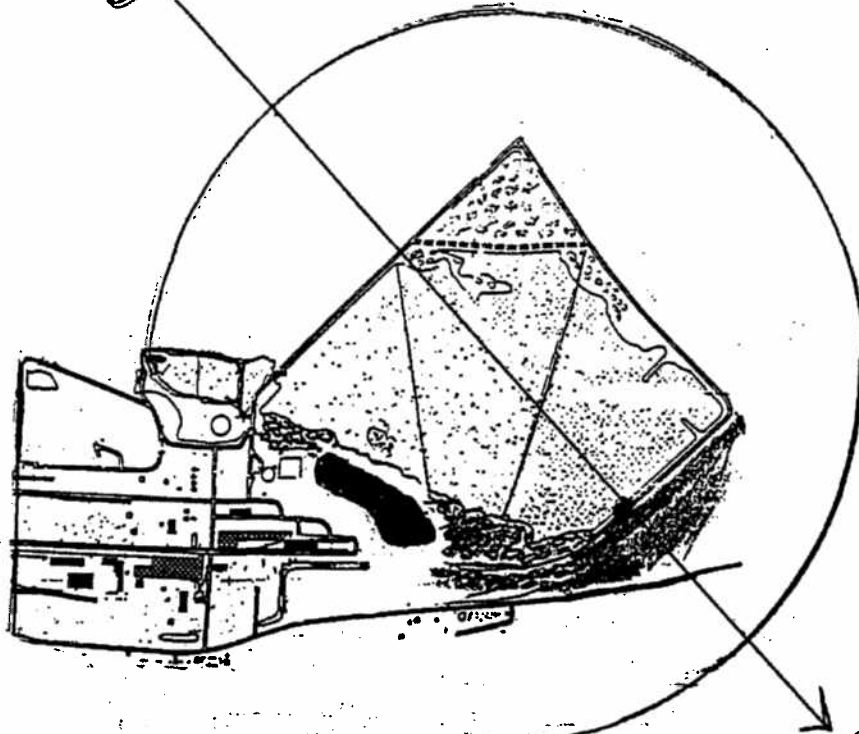
R=4200

C



42p

3.4  
~~1.4~~



R = 3800

0 1000 2000 3000 4000 5000 6000 7000 FEET  
1 inch = 2000'

1027

D

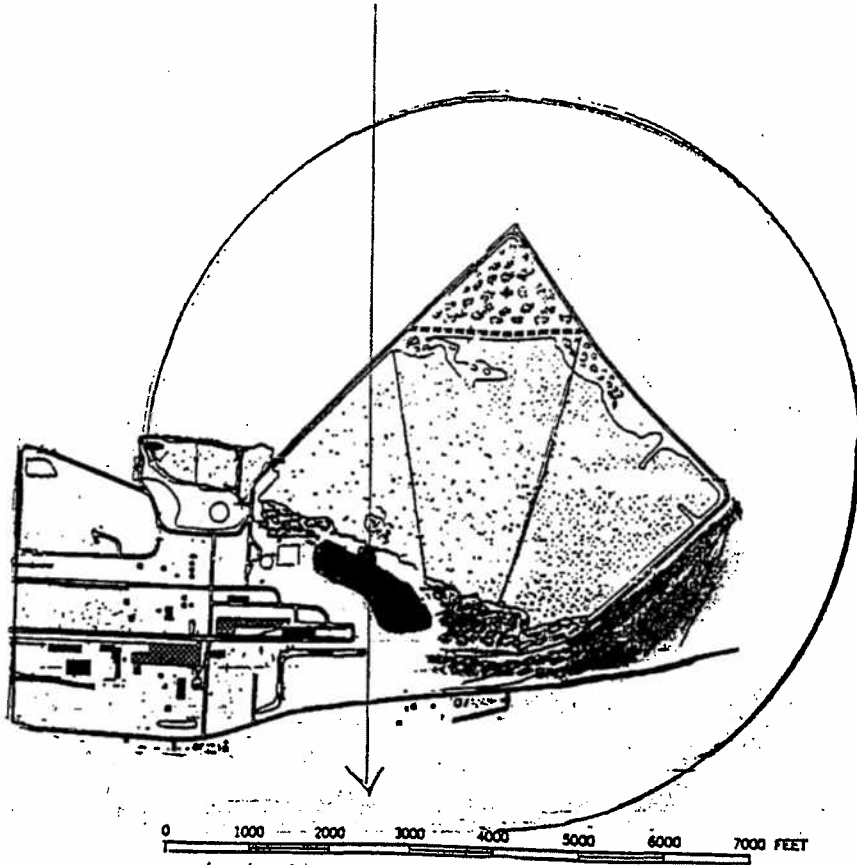


ROUND # 1 2/12/01

FEBO-a

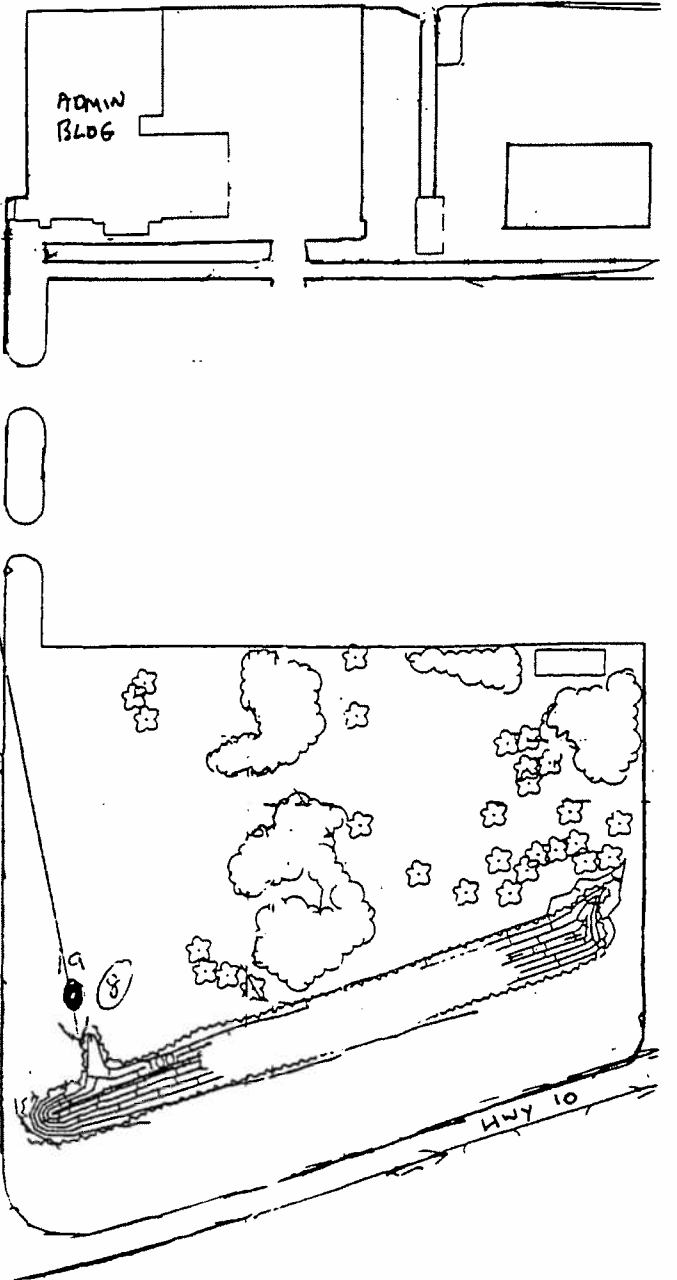
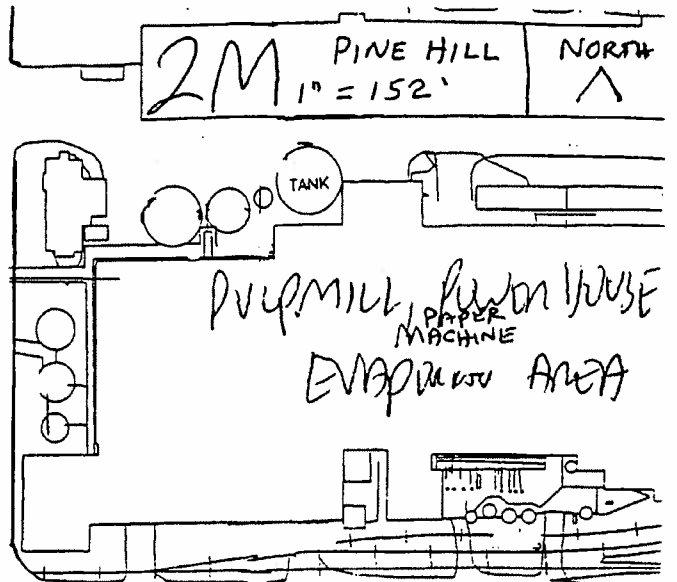
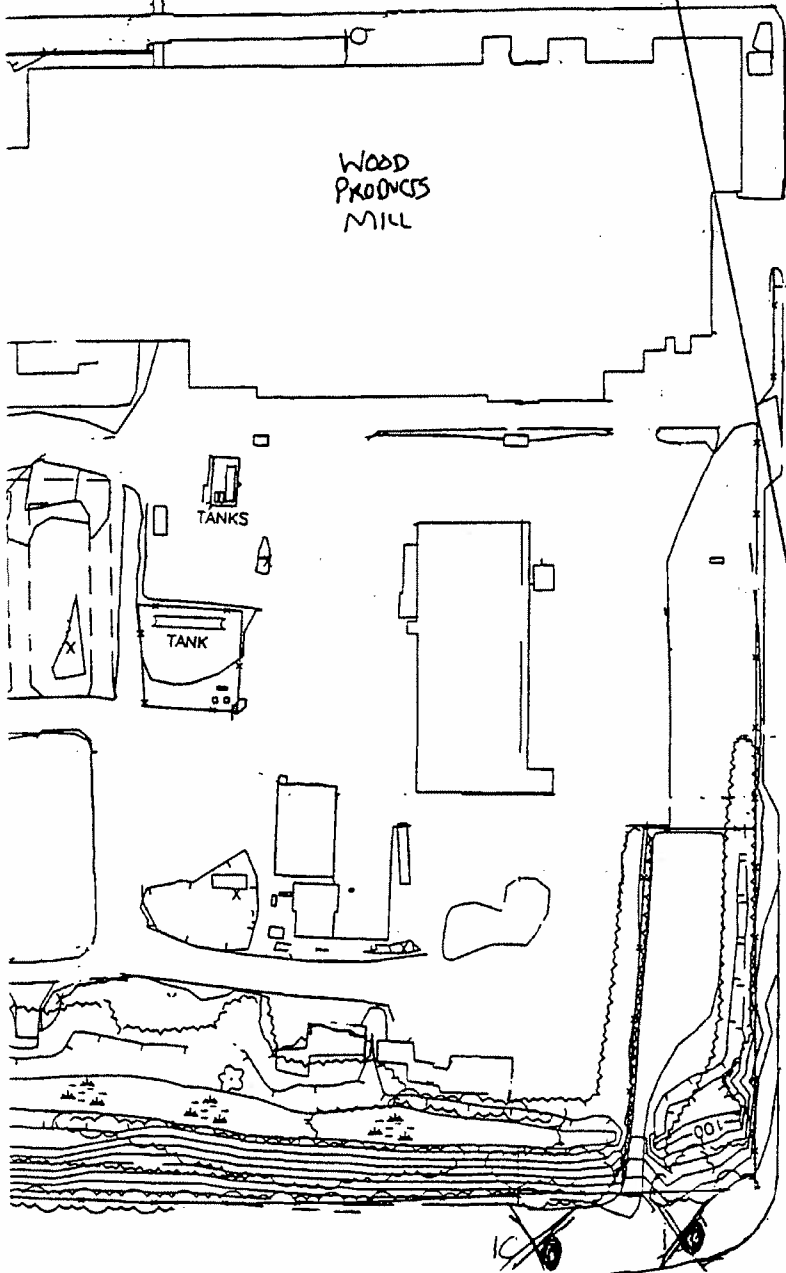
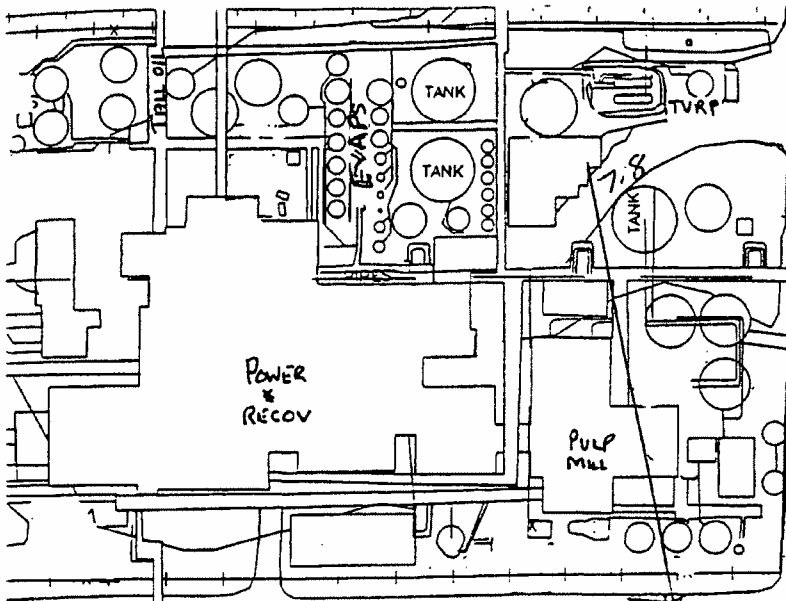
POLISH INLET

6.6



1 inch = 2000'

1400



2M PINE HILL NORTH  
 1" = 152'



**PINE HILL TRS STUDY - PHASE II**

# **Emission Models**

**Models of Polishing Pond- full reach**

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 2P WEST EDGE

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA  
EMISSION RATE (G/S) = 98.20 779 #/HR  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 762.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 3 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 2.7 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
610.	1297.	3	2.7	2.7	864.0	1.0	229.3	38.9	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	1297.	610.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 5P *WEST EDGE*

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA  
EMISSION RATE (G/S) = 38.90  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 762.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

*309 \*/hr*

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 3 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 2.0 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
610.	693.7	3	2.0	2.0	640.0	1.0	229.3	38.9	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	693.7	610.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 9P *LAST EDGE*

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA *278 #/hr*  
EMISSION RATE (G/S) = 31.25  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 762.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 4 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 1.3 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

	DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
<i>EDGE</i>	506.	2033. <i>1438</i>	4	1.3	1.3	416.0	1.0	203.0	18.5	NO
<i>Hy</i>	793.	1314.	4	1.3	1.3	416.0	1.0	218.7	26.6	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	2033.	506.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 11P

*EAST EDGE*

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA  
EMISSION RATE (G/S) = 15.50 *123 #/hr*  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 762.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 4 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 1.1 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
506.	1192. <i>843</i>	4	1.1	1.1	352.0	1.0	203.0	18.5	NO
793.	770.3 <i>545</i>	4	1.1	1.1	352.0	1.0	218.7	26.6	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	1192.	506.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 14P

*EAST EDGE*

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA  
EMISSION RATE (G/S) = 29.50 *234 #/hr*  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 762.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 4 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 1.2 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	<i>h<sub>25</sub></i> STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
<i>f EME</i> 506.	2080.	<i>1470</i> 4	1.2	1.2	384.0	1.0	203.0	18.5	NO
<i>hwy (em)</i> 793.	1344.	<i>950</i> 4	1.2	1.2	384.0	1.0	218.7	26.6	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	2080.	506.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 15P

*EAST EDGE*

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA *146.8 #/hr*  
EMISSION RATE (G/S) = 18.50  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 762.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 4 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 1.3 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	<i>HS</i> STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
506.	1204.	<i>851</i> 4	1.3	1.3	416.0	1.0	203.0	18.5	NO
793.	777.9	<i>552</i> 4	1.3	1.3	416.0	1.0	218.7	26.6	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	1204.	506.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*



\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 17P *EAST EDGE*

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA *205,6 #/yr*  
EMISSION RATE (G/S) = 25.90  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 762.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 4 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 1.3 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
✓506.	1685.	1.3	1.3	416.0	1.0	203.0	18.5	NO
793.	1089.	1.3	1.3	416.0	1.0	218.7	26.6	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	1685.	506.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 19P

*EAST EDGE*

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA  
EMISSION RATE (G/S) = 231.4 *1836.5 #/hr*  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 762.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 3 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 3.0 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
✓ 506.	3393.	<i>2400</i> 3	3.0	3.0	960.0	1.0	220.3	32.8	NO
793.	2026.	<i>1433</i> 3	3.0	3.0	960.0	1.0	244.9	49.5	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	3393.	506.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 20P

*EAST EDGE*

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA  
EMISSION RATE (G/S) = 333.1 *2643.7 #/hr*  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 762.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 3 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 4.2 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
✓ 506.	3489.	<i>2467</i> 3	4.2	4.2	1344.0	1.0	220.3	32.8	NO
793.	2083.	<i>1473</i> 3	4.2	4.2	1344.0	1.0	244.9	49.5	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	3489.	506.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 41P

*EAST EDGE*

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA *628 #/m*  
EMISSION RATE (G/S) = 79.10  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 762.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 3 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 1.5 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
506.	2320.	3	1.5	1.5	480.0	1.0	220.3	32.8	NO
793.	1385.	3	1.5	1.5	480.0	1.0	244.9	49.5	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	2320.	506.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 42P

*EPK EOE*

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA  
EMISSION RATE (G/S) = 25.70  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 762.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

*204 #/1st*

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 4 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 1.5 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
506.	1449.	4	1.5	1.5	480.0	1.0	203.0	18.5	NO
793.	936.6	4	1.5	1.5	480.0	1.0	218.7	26.6	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	1449.	506.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

# **Models of Polishing Pond Inlet**

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

PP-INLET

Model# 32p

SIMPLE TERRAIN INPUTS:

SOURCE TYPE	=	AREA	
EMISSION RATE (G/S)	=	4.180	33.2 #/m
SOURCE HEIGHT (M)	=	1.00	
LENGTH OF SIDE (M)	=	91.50	
RECEPTOR HEIGHT (M)	=	1.00	
IOPT (1=URB,2=RUR)	=	2	

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 3 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 5.0 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
119.	891.4	3	5.0	5.0	1587.2	1.0	34.0	8.7	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	891.4	119.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

*PP-INLET*

Model# 34p

SIMPLE TERRAIN INPUTS:

SOURCE TYPE	=	AREA	
EMISSION RATE (G/S)	=	2.000	<i>15.9 #/m</i>
SOURCE HEIGHT (M)	=	1.00	
LENGTH OF SIDE (M)	=	91.50	
RECEPTOR HEIGHT (M)	=	1.00	
IOPT (1=URB,2=RUR)	=	2	

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 3 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 1.7 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
119.	1244.	3	1.7	1.7	544.0	1.0	34.0	8.7	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	1244.	119.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*



\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

PP - INLET

Model# 35p

SIMPLE TERRAIN INPUTS:

SOURCE TYPE	=	AREA	
EMISSION RATE (G/S)	=	2.030	16.1 #/hr
SOURCE HEIGHT (M)	=	1.00	
LENGTH OF SIDE (M)	=	91.50	
RECEPTOR HEIGHT (M)	=	1.00	
IOPT (1=URB,2=RUR)	=	2	

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 3 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 3.1 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
119.	692.7	3	3.1	3.1	992.0	1.0	34.0	8.7	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	692.7	119.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

PP-INLET

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 36p

SIMPLE TERRAIN INPUTS:

SOURCE TYPE	=	AREA	9.8 #/m
EMISSION RATE (G/S)	=	1.230	
SOURCE HEIGHT (M)	=	1.00	
LENGTH OF SIDE (M)	=	91.50	
RECEPTOR HEIGHT (M)	=	1.00	
IOPT (1=URB,2=RUR)	=	2	

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 3 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 1.8 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
119.	722.8	3	1.8	1.8	576.0	1.0	34.0	8.7	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	722.8	119.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

## **Model of PulpMill, PowerHouse, Recovery Area**

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

Model# 2m *Pulp Mill, Powerhouse EVAP AREAS*

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA *2.3 #/m*  
EMISSION RATE (G/S) = .2900  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 152.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 3 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 3.5 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
442.	11.44	3	3.5	3.5	1116.8	1.0	79.7	29.0	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	11.44	442.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

1

\*\*\* SCREEN-1.1 MODEL RUN \*\*\*  
\*\*\* VERSION DATED 88300 \*\*\*

PP-INLET

02-12-\*\*  
11:32:35

N@ 6.3 mph  
1400 fpl

Model# FEB01\_a

KUNO #1 (1/1) ~~FEB~~ FEB 2001

2/12 13:46

SIMPLE TERRAIN INPUTS:

SOURCE TYPE = AREA  
EMISSION RATE (G/S) = 5.200  
SOURCE HEIGHT (M) = 1.00  
LENGTH OF SIDE (M) = 91.50  
RECEPTOR HEIGHT (M) = 1.00  
IOPT (1=URB,2=RUR) = 2

41.3 #/hr

BUOY. FLUX = .00 M\*\*4/S\*\*3; MOM. FLUX = .00 M\*\*4/S\*\*2.

\*\*\* STABILITY CLASS 3 ONLY \*\*\*  
\*\*\* 10-METER WIND SPEED OF 2.8 M/S ONLY \*\*\*

\*\*\*\*\*  
\*\*\* SCREEN DISCRETE DISTANCES \*\*\*  
\*\*\*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
119.	1964.	3	2.8	2.8	896.0	1.0	34.0	8.7	NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)  
DWASH=NO MEANS NO BUILDING DOWNWASH USED  
DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED  
DWASH=SS MEANS SCHULMAN-SCIRES DOWNWASH USED  
DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB

\*\*\*\*\*  
\*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\*  
\*\*\*\*\*

CALCULATION PROCEDURE	MAX CONC (UG/M**3)	DIST TO MAX (M)	TERRAIN HT (M)
SIMPLE TERRAIN	1964.	119.	0.

\*\*\*\*\*  
\*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*  
\*\*\*\*\*

**PINE HILL TRS STUDY - PHASE II**

# **ENSR Station Weather Summary**

Pine Hill Weather Station Data  
November 2001

WEYERHAEUSER	TEMP	WDR	WSP	H2S	DELTAT	SOLAR	STATMP	SD1	STABILITY CLASS			
PINE HILL	DEGC	DEG	MPH	PPM	DEGC	WM2	DEGF	DEG	Sol	Inv	Class	°F
11/30/2001 5:00	11.3	260.8	3.3	0.001	-0.27	0	76.9	20.6	D	D	D	52
11/30/2001 6:00	10.8	247.9	3.8	0.000	-0.28	0	77.0	23.4	D	D	D	51
11/30/2001 7:00	10.5	252.7	4.2	0.000	-0.30	7	76.9	18.4	D	D	D	51
11/30/2001 8:00	10.6	285.9	4.1	0.002	-0.37	53	77.1	20.6	C	D	C	51
11/30/2001 9:00	10.5	286.5	4.3	0.003	-0.51	95	76.7	24.1	C	D	C	51
11/30/2001 10:00	10.2	331.8	7.5	0.012	-0.43	144	77.2	10.8	C	D	C	50
11/30/2001 11:00	10.8	304.8	3.3	0.002	-0.70	204	76.9	39.3	C	D	C	51
11/30/2001 12:00	11.3	331.6	3.8	0.004	-0.67	249	77.1	37.4	C	D	C	52
11/30/2001 13:00	12.1	286.5	3.7	0.003	-0.94	319	77.1	31.0	C	D	C	54
11/30/2001 14:00	12.7	328.6	5.7	0.007	-0.94	448	77.0	20.1	C	D	C	55
11/30/2001 15:00	12.8	322.4	6.1	0.005	-0.85	351	77.1	15.1	C	D	C	55
11/30/2001 16:00	12.4	329.4	5.6	0.019	-0.54	165	77.3	14.1	C	D	C	54
11/30/2001 17:00	11.3	352.6	5.4	0.079	-0.27	15	76.9	11.7	D	D	D	52
11/30/2001 18:00	9.8	44.0	3.7	0.138	-0.03	0	76.9	16.5	D	D	D	50
11/30/2001 19:00	9.4	23.0	2.8	0.222	-0.01	0	76.7	14.6	D	D	D	49

Pine Hill Weather Station Data  
December 2001

Dec 01												
WEYERHAEUSER	TEMP	WDR	WSP	H2S	DELTAT	SOLAR	STATMP	SD1	STABILITY CLASS			
PINE HILL	DEGC	DEG	MPH	PPM	DEGC	WM2	DEGF	DEG	Solar	Inversion	Class	°F
12/1/2001 5:00	4.0	294.6	1.3	0.035	-0.40	0	77.2	43.5	D	D	D	39
12/1/2001 6:00	4.4	304.8	1.0	0.133	-0.38	0	77.2	36.5	D	D	D	40
12/1/2001 7:00	4.2	259.5	1.5	0.040	-0.52	9	77.3	23.9	D	D	D	40
12/1/2001 8:00	4.8	77.0	0.8	0.148	-0.27	84	77.3	52.9	C	D	C	41
12/1/2001 9:00	6.0	68.9	2.0	0.112	-0.29	267	76.9	36.7	C	D	C	43
12/1/2001 10:00	8.2	11.9	2.5	0.101	-0.49	466	77.1	26.3	C	D	C	47
12/1/2001 11:00	12.1	6.0	2.9	0.058	-0.61	561	77.1	32.0	C	D	C	54
12/1/2001 12:00	15.1	28.9	3.0	0.044	-0.51	581	77.3	34.2	C	D	C	59
12/1/2001 13:00	16.6	10.8	3.7	0.043	-0.53	562	77.3	32.5	C	D	C	62
12/1/2001 14:00	17.5	28.9	3.0	0.028	-0.36	464	77.5	41.3	C	D	C	64
12/1/2001 15:00	18.1	30.0	3.4	0.059	-0.31	326	77.3	26.5	C	D	C	65
12/1/2001 16:00	17.9	38.9	2.7	0.071	-0.06	134	77.4	27.0	C	D	C	64
12/1/2001 17:00	15.1	241.9	0.4	0.029	1.18	11	77.2	64.9	D	F	C	59
12/1/2001 18:00	12.3	168.2	0.5	0.022	1.46	0	77.1	46.9	D	F	C	54



Pine Hill Weather Station Data  
December 2001

Dec 01

WEYERHAEUSER	TEMP	WDR	WSP	H2S	DELTAT	SOLAR	STATMP	SD1	STABILITY CLASS			
PINE HILL	DEGC	DEG	MPH	PPM	DEGC	WM2	DEGF	DEG	Solar	Inversion	Class	°F
12/2/2001 5:00	5.8	290.8	0.5	0.028	0.51	0	77.0	37.0	D	F	D	42
12/2/2001 6:00	6.5	341.8	1.8	0.129	0.16	0	76.8	37.2	D	F	D	44
12/2/2001 7:00	6.5	341.6	1.8	0.064	-0.07	7	76.8	44.7	D	D	D	44
12/2/2001 8:00	7.3	312.4	2.9	0.036	-0.28	57	77.8	13.9	C	D	C	45
12/2/2001 9:00	9.0	324.8	3.3	0.054	-0.68	240	77.4	12.9	C	D	C	48
12/2/2001 10:00	12.0	340.7	2.8	0.032	-0.88	431	77.3	23.8	C	D	C	54
12/2/2001 11:00	14.6	13.8	2.7	0.059	-0.51	552	77.2	28.8	C	D	C	58
12/2/2001 12:00	17.2	20.0	2.4	0.041	-0.49	605	77.3	38.1	C	D	C	63
12/2/2001 13:00	19.0	17.0	4.0	0.053	-0.49	548	76.9	23.9	C	D	C	66
12/2/2001 14:00	20.2	11.9	3.7	0.050	-0.43	454	77.0	23.9	C	D	C	68
12/2/2001 15:00	21.1	351.5	4.4	0.063	-0.41	319	76.9	19.9	C	D	C	70
12/2/2001 16:00	20.8	347.8	5.1	0.099	-0.19	154	76.8	12.8	C	D	C	69
12/2/2001 17:00	19.2	336.7	4.8	0.100	0.14	13	77.2	8.3	D	F	D	67
12/2/2001 18:00	15.4	309.7	1.4	0.075	1.57	-1	77.1	39.8	D	F	D	60

Pine Hill Weather Station Data  
December 2001

Dec 01												
WEYERHAEUSER	TEMP	WDR	WSP	H2S	DELTAT	SOLAR	STATMP	SD1	STABILITY CLASS			
PINE HILL	DEGC	DEG	MPH	PPM	DEGC	WM2	DEGF	DEG	Solar	Inversion	Class	°F
12/3/2001 5:00	6.0	345.9	1.0	0.063	0.98	0	77.5	52.5	D	F	D	43
12/3/2001 6:00	5.7	345.6	0.5	0.093	0.75	0	77.7	59.8	D	F	D	42
12/3/2001 7:00	5.0	217.9	1.3	0.014	0.13	11	77.7	24.9	D	F	D	41
12/3/2001 8:00	7.2	349.7	1.1	0.165	-0.15	147	77.7	27.2	C	D	C	45
12/3/2001 9:00	10.2	6.8	2.2	0.195	-0.45	316	77.5	19.1	C	D	C	50
12/3/2001 10:00	13.7	359.6	2.0	0.138	-0.65	467	76.9	28.4	C	D	C	57
12/3/2001 11:00	17.0	4.9	3.2	0.083	-0.49	555	77.3	20.2	C	D	C	63
12/3/2001 12:00	19.6	23.8	2.8	0.028	-0.35	577	77.1	34.4	C	D	C	67
12/3/2001 13:00	21.3	62.9	3.3	0.021	-0.48	539	77.0	37.1	C	D	C	70
12/3/2001 14:00	22.2	91.0	3.2	0.009	-0.40	448	76.9	40.4	C	D	C	72
12/3/2001 15:00								F 19.9	D	E	D	32
12/3/2001 16:00	22.2	87.0	3.7	0.001	-0.02	135	77.1	< 28.9	C	D	C	72
12/3/2001 17:00	19.9	75.9	2.5	0.003	1.06	11	77.2	8.8	D	F	D	68
12/3/2001 18:00	16.5	65.9	1.5	0.071	1.62	-1	77.1	30.1	D	F	D	62

Pine Hill Weather Station Data  
December 2001

Dec 01												
WEYERHAEUSER	TEMP	WDR	WSP	H2S	DELTAT	SOLAR	STATMP	SD1	STABILITY CLASS			
PINE HILL	DEGC	DEG	MPH	PPM	DEGC	WM2	DEGF	DEG	Solar	Inversion	Class	°F
12/4/2001 5:00	7.2	272.4	0.3	0.199	0.28	0	77.2	30.6	D	F	D	45
12/4/2001 6:00	7.5	246.2	0.2	0.149	0.13	0	77.6	53.5	D	F	D	46
12/4/2001 7:00	6.9	58.9	0.7	0.229	0.88	10	77.4	52.9	D	F	D	44
12/4/2001 8:00	9.1	30.8	1.2	0.373	0.20	112	77.5	34.1	C	F	D	48
12/4/2001 9:00	11.7	24.1	1.8	0.358	-0.24	267	77.3	18.3	C	D	C	53
12/4/2001 10:00	16.6	141.8	2.1	0.030	-0.46	444	77.3	40.2	C	D	C	62
12/4/2001 11:00	19.9	157.1	3.0	0.001	-0.70	550	77.2	32.2	C	D	C	68
12/4/2001 12:00	21.2	157.1	2.4	0.001	-0.44	574	77.0	56.7	C	D	C	70
12/4/2001 13:00	22.2	138.8	2.4	0.000	-0.62	536	76.9	36.9	C	D	C	72
12/4/2001 14:00	23.1	110.2	2.9	0.001	-0.37	441	77.0	39.8	C	D	C	74
12/4/2001 15:00	23.3	99.9	3.8	0.001	-0.25	305	77.1	24.4	C	D	C	74
12/4/2001 16:00	22.6	94.8	3.3	0.004	-0.03	140	76.8	19.1	C	D	C	73
12/4/2001 17:00	20.2	104.0	2.3	0.001	0.78	11	77.3	12.4	D	F	D	68
12/4/2001 18:00	16.4	153.9	1.4	0.001	1.47	-1	77.1	13.2	D	F	D	62

Pine Hill Weather Station Data  
December 2001

Dec 01												
WEYERHAEUSER	TEMP	WDR	WSP	H2S	DELTAT	SOLAR	STATMP	SD1	STABILITY CLASS			
PINE HILL	DEGC	DEG	MPH	PPM	DEGC	WM2	DEGF	DEG	Solar	Inversion	Class	°F
12/5/2001 5:00	7.5	55.9	1.3	0.273	1.33	0	77.6	21.6	D	F	D	46
12/5/2001 6:00	6.5	227.3	0.6	0.114	0.79	0	77.7	37.2	D	F	D	44
12/5/2001 7:00	6.5	17.8	0.2	0.145	0.85	9	77.4	43.6	D	F	D	44
12/5/2001 8:00	8.6	153.9	0.4	0.243	-0.13	142	77.6	48.0	C	D	C	47
12/5/2001 9:00	13.0	3.0	0.8	0.201	-0.49	298	77.5	44.7	C	D	C	55
12/5/2001 10:00	16.3	37.0	1.1	0.150	-0.52	470	77.3	35.0	C	D	C	61
12/5/2001 11:00	19.9	148.0	3.5	0.001	-0.57	543	77.2	32.6	C	D	C	68
12/5/2001 12:00	21.6	152.8	3.3	0.001	-0.48	578	77.0	37.8	C	D	C	71
12/5/2001 13:00	23.0	165.2	3.7	0.001	-0.67	528	76.8	32.7	C	D	C	73
12/5/2001 14:00	24.1	164.2	3.9	0.000	-0.53	443	77.1	29.8	C	D	C	75
12/5/2001 15:00	24.1	159.8	4.1	0.000	-0.24	292	77.1	27.9	C	D	C	75
12/5/2001 16:00	23.4	165.0	3.1	0.000	0.10	137	77.0	21.7	C	F	D	74
12/5/2001 17:00	20.9	165.8	1.5	0.001	0.67	13	77.1	17.9	D	F	D	70
12/5/2001 18:00	18.3	136.1	0.5	0.001	1.33	0	77.3	32.3	D	F	D	65

Pine Hill Weather Station Data  
December 2001

Dec 01

WEYERHAEUSER	TEMP	WDR	WSP	H2S	DELTAT	SOLAR	STATMP	SD1	STABILITY CLASS			
PINE HILL	DEGC	DEG	MPH	PPM	DEGC	WM2	DEGF	DEG	Solar	Inversion	Class	°F
12/6/2001 5:00	11.3	172.3	0.9	0.154	-0.13	0	77.0	34.7	D	D	D	52
12/6/2001 6:00	11.1	186.0	0.9	0.079	-0.16	0	77.0	56.7	D	D	D	52
12/6/2001 7:00	10.7	200.9	1.3	0.027	-0.06	9	77.1	21.2	D	D	D	51
12/6/2001 8:00	11.3	215.2	0.4	0.013	-0.23	120	77.1	51.2	C	D	C	52
12/6/2001 9:00	13.8	171.7	0.6	0.059	-0.46	284	77.3	58.8	C	D	C	57
12/6/2001 10:00	17.9	216.3	1.6	0.004	-1.00	450	77.2	35.6	C	D	C	64
12/6/2001 11:00	21.8	189.8	3.3	0.013	-0.86	545	77.3	41.6	C	D	C	71
12/6/2001 12:00	23.9	197.9	4.1	0.001	-0.79	569	77.1	29.8	C	D	C	75
12/6/2001 13:00	25.1	195.2	5.3	0.001	-0.81	504	77.0	27.3	C	D	C	77
12/6/2001 14:00	25.5	222.8	4.6	0.001	-0.72	370	77.1	28.2	C	D	C	78
12/6/2001 15:00	25.3	215.7	3.5	0.000	-0.40	247	77.1	27.0	C	D	C	78
12/6/2001 16:00	24.5	196.3	2.2	0.000	0.05	131	77.2	19.7	C	F	D	76
12/6/2001 17:00	21.6	180.1	1.3	0.001	0.64	12	77.2	15.6	D	F	D	71
12/6/2001 18:00	18.7	192.2	1.0	0.001	0.95	-1	77.1	33.7	D	F	D	66

Pine Hill Weather Station Data  
December 2001

Dec 01												
WEYERHAEUSER	TEMP	WDR	WSP	H2S	DELTAT	SOLAR	STATMP	SD1	STABILITY CLASS			
PINE HILL	DEGC	DEG	MPH	PPM	DEGC	WM2	DEGF	DEG	Solar	Inversion	Class	°F
12/7/2001 5:00	11.2	124.2	0.6	0.001	0.91	0	77.1	60.0	D	F	D	52
12/7/2001 6:00	11.6	211.4	1.1	0.001	-0.07	0	77.1	27.2	D	D	D	53
12/7/2001 7:00	12.4	199.3	1.3	0.001	-0.19	7	77.1	21.9	D	D	D	54
12/7/2001 8:00	13.0	152.3	2.2	0.001	-0.19	67	77.0	15.8	C	D	C	55
12/7/2001 9:00	14.2	189.3	1.5	0.001	-0.36	156	76.8	33.2	C	D	C	58
12/7/2001 10:00	15.9	226.3	1.6	0.001	-0.58	284	77.0	47.5	C	D	C	61
12/7/2001 11:00	19.2	158.2	1.9	0.008	-0.68	518	76.7	50.7	C	D	C	67
12/7/2001 12:00	22.5	199.8	3.1	0.001	-0.91	564	75.9	32.1	C	D	C	73
12/7/2001 13:00	24.2	7.4	3.4	0.000	0.94	532	75.8	46.3	C	F	D	76
12/7/2001 14:00	24.8	177.1	3.4	0.000	-0.59	454	75.8	37.2	C	D	C	77
12/7/2001 15:00	24.4	2.2	3.2	0.000	0.34	222	75.8	27.9	C	F	D	76
12/7/2001 16:00	23.6	212.8	3.0	0.000	-0.01	116	75.8	16.7	C	D	C	74
12/7/2001 17:00	20.7	181.7	1.5	0.001	0.92	12	75.7	14.8	D	F	D	69
12/7/2001 18:00	17.6	168.2	1.4	0.001	0.69	0	75.6	14.8	D	F	D	64

Pine Hill Weather Station Data  
December 2001

Dec 01

WEYERHAEUSER	TEMP	WDR	WSP	H2S	DELTAT	SOLAR	STATMP	SD1	STABILITY CLASS			
PINE HILL	DEGC	DEG	MPH	PPM	DEGC	WM2	DEGF	DEG	Solar	Inversion	Class	°F
12/8/2001 5:00	11.2	123.1	0.9	0.002	1.24	0	76.3	47.3	D	F	D	52
12/8/2001 6:00	10.8	189.3	0.6	0.001	0.76	0	76.4	44.9	D	F	D	51
12/8/2001 7:00	10.4	165.8	1.4	0.001	0.34	11	76.6	19.7	D	F	D	51
12/8/2001 8:00	12.7	178.2	1.3	0.002	-0.19	135	76.3	33.0	C	D	C	55
12/8/2001 9:00	16.7	192.8	2.9	0.004	-0.72	291	76.0	19.5	C	D	C	62
12/8/2001 10:00	20.1	208.2	3.9	0.001	-0.91	438	75.9	19.2	C	D	C	68
12/8/2001 11:00	23.0	212.0	5.2	0.001	-1.12	569	75.8	19.4	C	D	C	73
12/8/2001 12:00	24.3	260.3	5.3	0.001	-1.06	430	75.9	24.1	C	D	C	76
12/8/2001 13:00	24.1	288.4	5.8	0.002	-0.94	364	75.8	24.0	C	D	C	75
12/8/2001 14:00	23.1	323.7	7.7	0.084	-0.66	247	75.9	13.0	C	D	C	74
12/8/2001 15:00	22.8	307.3	5.5	0.041	-0.69	264	75.9	24.0	C	D	C	73
12/8/2001 16:00	22.6	280.8	3.5	0.012	-0.31	137	75.7	20.1	C	D	C	73
12/8/2001 17:00	20.9	312.4	2.2	0.047	0.39	15	75.7	24.0	D	F	D	70
12/8/2001 18:00	17.9	181.7	0.3	0.072	1.51	0	75.7	47.4	D	F	D	64

Pine Hill Weather Station Data  
December 2001

Dec 01												
WEYERHAEUSER	TEMP	WDR	WSP	H2S	DELTAT	SOLAR	STATMP	SD1	STABILITY CLASS			
PINE HILL	DEGC	DEG	MPH	PPM	DEGC	WM2	DEGF	DEG	Solar	Inversion	Class	°F
12/9/2001 5:00	13.3	343.7	8.4	0.124	-0.23	0	76.0	11.3	D	D	D	56
12/9/2001 6:00	12.5	348.6	8.1	0.121	-0.25	0	76.0	11.0	D	D	D	55
12/9/2001 7:00	12.3	350.7	7.2	0.111	-0.23	2	76.0	11.2	D	D	D	54
12/9/2001 8:00	12.6	355.6	6.3	0.119	-0.22	23	76.2	10.9	D	D	D	55
12/9/2001 9:00	12.8	8.9	6.6	0.138	-0.24	75	76.2	11.8	C	D	C	55
12/9/2001 10:00	13.1	4.9	6.2	0.137	-0.28	68	76.3	13.1	C	D	C	56
12/9/2001 11:00	13.2	6.0	6.2	0.135	-0.30	128	76.1	13.9	C	D	C	56
12/9/2001 12:00	13.5	6.8	5.3	0.114	-0.37	139	76.0	14.6	C	D	C	56
12/9/2001 13:00	13.8	359.9	5.7	0.104	-0.34	107	76.5	12.8	C	D	C	57
12/9/2001 14:00	14.2	355.9	5.2	0.100	-0.43	170	76.1	15.0	C	D	C	58
12/9/2001 15:00	14.7	1.9	6.1	0.118	-0.34	166	76.5	15.9	C	D	C	58
12/9/2001 16:00	14.6	348.8	7.2	0.119	-0.28	72	76.1	10.6	C	D	C	58
12/9/2001 17:00	14.1	0.8	5.5	0.156	-0.18	7	76.3	9.7	D	D	D	57
12/9/2001 18:00	13.7	11.9	4.2	0.194	-0.16	0	76.5	9.7	D	D	D	57



**PINE HILL TRS STUDY - PHASE II**

**Process Sewer Flow Data**

NOVEMBER 30

PULP MILL	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	1.6	9.7	1.9	1.2	0.18	0.1	0.19	0.1	0	0.0	1.4

POWER & RECOVERY	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	4.5	9.8	17	26.6	6.3	9.9	0.77	1.2	4.8	7.2	44.9

CAUST AREA TO ASH POND	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	1.6	>11.0	1000	556.3	0	0.0	0	0.0	0	0.0	556.3

# 1 PM	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	2.9	6.9	0.09	0.1	0	0.0	0	0.0	0	0.0	0.1

# 2 PM	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	3.5	7.1	0.13	0.2	0.14	0.2	0	0.0	0.34	0.4	0.7

OCC	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	1.1				0.0		0.0		0.0		0.0

ASH POND OVERFLOW TO ASH by-pass Clarifier	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	13.1		29	132.1	0.95	4.3	0	0.0	0	0.0	136.4

EQ POND DECANT	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
			20	0.0		0.0		0.0		0.0	0.0

CSSC HOTWELL	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
			2.3	0.0		0.0		0.0		0.0	0.0

KRAFT HOTWELL	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
			37	0.0	69	0.0	5.2	0.0	29	0.0	0.0

<b>TOTAL LBS / HR</b>	<b>716.4</b>	<b>14.5</b>	<b>1.3</b>	<b>7.6</b>	<b>739.9</b>
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lbs / hr  
H<sub>2</sub>S  
gain/loss

48.0  
CLARIFIER

-91.3  
ASB

45.0  
POLISH  
POND

NOVEMBER 30 TREATMENT SYSTEM FLOW

PPM = mg/L

Clarifier Inlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
12	8.5	3.5	14.6	0.87	3.6	0.24	1.0	1.3	5.4	6	25

Clarifier Outlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
12	-	15	62.6	0.93	3.9	0.23	1.0	0	0.0	16	67

Ash Pond Overflow - (includes Caustic Sewer)

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
7.5	-	29	75.6	0.95	2.5	0	0.0	0	0.0	30	78

ASB Inlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	11	15	96.5	1.4	9.0	0.2	1.3	0.31	2.0	16.91	109

ASB Outlet - before Riffler

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	8.1	0.81	5.2	0	0.0	0	0.0	0	0.0	0.81	5

Polishing Pond Inlet - ASB outlet after Riffler

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	-	0.8	5.1	0.17	1.1	0	0.0	0	0.0	0.97	6

Polishing Pond Outlet

Flow MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	7.8	7.8	50.2	0.19	1.2	0	0.0	0	0.0	7.99	51

Estimated average flows used, obtained from flow / sulfur balance study  
Pond Outlet flows 'normalized' to match Inlet flowrate for comparison purposes

DECEMBER 1

PULP MILL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	1.8	8.2	38	23.8	0.53	0.3	0.18	0.1	0	0.0	24.2

POWER & RECOVERY	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	4.5	8.5	17	26.8	4.4	1.2	1.1	1.7	7	11.0	40.5

CAUST AREA TO ASH POND	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	1.8	>11.0	207	115.2	0	0.0	0	0.0	0	0.0	115.2

# 1 PM	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	3	7.1	0	0.0	0	0.0	0	0.0	0	0.0	0.0

# 2 PM	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	3.5	7.8	0	0.0	0	0.0	0	0.0	0.47	0.6	0.6

OCC	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	1.1		0	0.0	0	0.0	0	0.0	0	0.0	0.0

ASH POND OVERFLOW TO ASB In-pass Clarifier	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	13.1		83	378.1	15	6.8	0.23	1.0	0	0.0	365.0

EQ POND DECANT	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

CSSC HOTWELL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

KRAFT HOTWELL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

↓

TOTAL LBS / HR	543.6	8.4	2.9	11.5	566.4
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DECEMBER 1 TREATMENT SYSTEM FLOW

PPM = mg/L

Clarifier Inlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
12	8.5	4	16.7	0.66	2.8	0.24	1.0	3.3	13.8	8	34

lbs / hr  
H<sub>2</sub>S  
airflow

125.2  
CLARIFIER

Clarifier Outlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
12	-	34	141.9	2	8.3	0.28	1.2	0	0.0	36	151

Ash Pond Overflow - (includes Caustic Sewer)

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
7.5	-	83	216.4	1.5	3.9	0.23	0.6	0	0.0	65	221

ASB Inlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	11	32	205.8	2	12.9	0	0.0	0.32	2.1	34.32	221

ASB Outlet - before Riffler

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	8.1	0.82	4.0	0	0.0	0	0.0	0	0.0	0.62	4

-202.9  
ASB

Polishing Pond Inlet - ASB outlet after Riffler

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	-	0.45	2.9	0.14	0.9	0	0.0	0	0.0	0.59	4

61.4  
POLISH  
POND

Polishing Pond Outlet

Flow MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	8.1	10	64.3	0.18	1.2	0	0.0	0	0.0	10.18	65

Estimated average flows used, obtained from flow / sulfur balance study  
Pond Outlet flows "normalized" to match inlet flowrate for comparison purposes

DECEMBER 2

PULP MILL	FLOW	PH	H2S		MESH		DMS		DMDS		TRS
	MGD		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
	1.8	6.7	45	28.2	0.57	0.4	0.24	0.2	0	0.0	28.67
POWER & RECOVERY	FLOW	PH	H2S		MESH		DMS		DMDS		TRS
	MGD		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
	4.5	8.5	15	23.5	2.5	3.9	0.88	1.4	5.2	8.1	36.9
CAUST AREA TO ASH POND	FLOW	PH	H2S		MESH		DMS		DMDS		TRS
	MGD		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
	1.8	>11.0	2300	1279.5	0	0.0	0	0.0	0	0.0	1279.5
# 1 PM	FLOW	PH	H2S		MESH		DMS		DMDS		TRS
	MGD		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
	3.2	7.2		0.0		0.0		0.0		0.0	0.0
# 2 PM	FLOW	PH	H2S		MESH		DMS		DMDS		TRS
	MGD		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
	3.5	8.4	0.13	0.2	0	0.0	0	0.0	0.48	0.8	0.7
OCC	FLOW	PH	H2S		MESH		DMS		DMDS		TRS
	MGD		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
				0.0		0.0		0.0		0.0	0.0
ASH POND OVERFLOW TO ASB	FLOW	PH	H2S		MESH		DMS		DMDS		TRS
	MGD		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
	13.1		80	364.4	1.2	5.5	0	0.0	0	0.0	369.9
EQ POND DECANT	FLOW	PH	H2S		MESH		DMS		DMDS		TRS
	MGD		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
				0.0		0.0		0.0		0.0	0.0
CSSC HOTWELL	FLOW	PH	H2S		MESH		DMS		DMDS		TRS
	MGD		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
				0.0		0.0		0.0		0.0	0.0
KRAFT HOTWELL	FLOW	PH	H2S		MESH		DMS		DMDS		TRS
	MGD		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
				0.0		0.0		0.0		0.0	0.0
↓			TOTAL LBS / HR	1695.7		9.7		1.5		8.7	1715.7

DECEMBER 2 TREATMENT SYSTEM FLOW

PPM = mg/L

lbs / hr  
H<sub>2</sub>S  
gain/loss

193.2  
CLARIFIER

Clarifier Inlet

FLOW	PH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
12	8.5	7.7	32.1	1.1	4.8	0.33	1.4	4.7	19.6	14	58

Clarifier Outlet

FLOW	PH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
12	-	54	225.3	2.5	10.4	0.3	1.3	0	0.0	57	237

Ash Pond Overflow - (includes Caustic Sewer)

FLOW	PH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
7.5	-	80	208.8	1.2	3.1	0	0.0	0	0.0	81	212

ASB Inlet

FLOW	PH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
18.5	11	39	212.3	1.8	11.6	0	0.0	0.37	2.4	35.17	226

ASB Outlet - before Riffler

FLOW	PH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
18.5	8.1	0.6	3.9	0.18	1.2	0.2	1.3	0	0.0	0.88	6

-207.7  
ASB

Polishing Pond Inlet - ASB outlet after Riffler

FLOW	PH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
18.5	-	0.71	4.6	0	0.0	0	0.0	0	0.0	0.71	5

72.6  
POLISH  
POND

Polishing Pond Outlet

Flow	PH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
18.5	7.9	12	77.2	0	0.0	0	0.0	0	0.0	12	77

Estimated average flows used, obtained from flow / sulfur balance study  
Pond Outlet flows 'normalized' to match inlet flowrate for comparison purposes

DECEMBER 3

PULP MILL	FLOW MOD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	18	8.3	26	1.6	0	0.0	0	0.0	0	0.0	1.6

POWER & RECOVERY	FLOW MOD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	4.5	6.4	16	25.0	6.2	9.7	0	0.0	8.3	9.9	44.6

CAUSTIC AREA TO ASH POND	FLOW MOD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	16	>11.0	1500	834.5	0	0.0	0	0.0	0	0.0	834.5

# 1 PM	FLOW MOD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	3.1	6.4		0.0		0.0		0.0		0.0	0.0

# 2 PM	FLOW MOD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	3.5	7.1	0	0.0	0.14	0.2	0	0.0	0	0.0	0.2

OCC	FLOW MOD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
				0.0		0.0		0.0		0.0	0.0

ASH POND OVERFLOW TO ASB In-pipe Clarifier	FLOW MOD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	13.1		98	446.4	1.3	5.9	0	0.0	0	0.0	452.3

EQ POND DECANT	FLOW MOD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
				0.0		0.0		0.0		0.0	0.0

CSSC HOTWELL	FLOW MOD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
				0.0		0.0		0.0		0.0	0.0

KRAFT HOTWELL	FLOW MOD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
				0.0		0.0		0.0		0.0	0.0



TOTAL LBS / HR    1307.5    15.9    0.0    9.9    1333.2

DECEMBER 3 TREATMENT SYSTEM FLOW

PPM = mg/L

lbs / hr  
H<sub>2</sub>S  
gal/hrs

193.6

CLARIFIER

Clarifier Inlet

FLOW MOD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
12	6	2.8	10.8	0.68	3.7	0.31	1.3	2.8	11.7	7	27

Clarifier Outlet

FLOW MOD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
12	-	49	204.4	2.2	9.2	0.36	1.6	0	0.0	52	215

Ash Pond Overflow - (Includes Caustic Sewer)

FLOW MOD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
7.5	-	98	255.6	1.3	3.4	0	0.0	0	0.0	99	259

ASB Inlet

FLOW MOD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	11.2	30	250.9	2.5	16.1	0.4	2.6	0	0.0	41.9	270

ASB Outlet - before Riffler

FLOW MOD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	8.3	1.7	10.9	0.47	3.0	0.24	1.5	0	0.0	2.41	16

-239.9

ASB

Polishing Pond Inlet - ASB outlet after Riffler

FLOW MOD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	-	1.7	10.9	0.44	2.8	0	0.0	0	0.0	2.14	14

239.9

POLISH POND

Polishing Pond Outlet

Flow MOD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	8	30	250.9	0	0.0	0	0.0	0	0.0	30	251

Estimated average flows used, obtained from flow / sulfur balance study  
Pond Outlet flows "normalized" to match inlet flowrate for comparison purposes

DECEMBER 4

PULP MILL	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	1.8	8.4	4.9	3.1	0.45	0.3	0	0.0	0.32	0.2	3.5

POWER & RECOVERY	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	4.5		35	54.8	11	17.2	1.3	2.0	3.9	6.1	80.1

CAUSTIC AREA TO ASH POND	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	1.6	>11.0	840	467.3	0	0.0	0	0.0	0	0.0	467.3

# 1 PM	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	3.2	6.6		0.0		0.0		0.0		0.0	0.0

# 2 PM	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	3.5	7.1	0	0.0	0	0.0	0	0.0	0.3	0.4	0.4

ACC	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

ASH POND OVERFLOW TO ASB	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
	13.1		140	637.7	0	0.0	0	0.0	0	0.0	637.7

ECONOMIZER	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

CSSC HOTWELL	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
			2.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

KRAFT HOTWELL	FLOW		H2S		MESH		DMS		DMDS		TRS
	MGD	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	LB/HR
			34	0.0	33	0.0	3.8	0.0	69	0.0	0.0

↓

TOTAL LBS / HR	1162.8	17.5	2.0	6.7	1189.0
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DECEMBER 4 TREATMENT SYSTEM FLOW

PPM = mg/L

lbs / hr  
H<sub>2</sub>S  
gal/hrs

141.9  
CLARIFIER

Clarifier Inlet		H2S		MESH		DMS		DMDS		Total TRS	
FLOW	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
12	11.4	14	58.4	2.5	10.4	0.6	2.5	0.85	3.5	18	75

Clarifier Outlet		H2S		MESH		DMS		DMDS		Total TRS	
FLOW	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
12	-	48	200.3	2.3	9.6	0.46	1.9	0	0.0	51	212

Ash Pond Overflow - (Includes Caustic Sewer)		H2S		MESH		DMS		DMDS		Total TRS	
FLOW	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
7.5	-	140	365.1	0	0.0	0	0.0	0	0.0	140	365

ASB Inlet		H2S		MESH		DMS		DMDS		Total TRS	
FLOW	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	11.7	43	276.6	2.7	17.4	0.4	2.6	0	0.0	46.1	297

-259.2  
ASB

ASB Outlet - before Riffler		H2S		MESH		DMS		DMDS		Total TRS	
FLOW	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	8.1	1.8	10.3	0.47	3.0	0	0.0	0	0.0	2.07	13

Polishing Pond Inlet - ASB outlet after Riffler		H2S		MESH		DMS		DMDS		Total TRS	
FLOW	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	-	2.7	17.4	0.81	3.9	0	0.0	0	0.0	3.31	21

246.4  
POLISH  
POND

Polishing Pond Outlet		H2S		MESH		DMS		DMDS		Total TRS	
Flow	pH	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	8.1	41	263.7	0	0.0	0	0.0	0	0.0	41	264

Estimated average flows used, obtained from flow / sulfur balance study  
Pond Outlet flows 'normalized' to match inlet flowrate for comparison purposes

DECEMBER 5

PULP MILL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	1.8	8.4	10	11.9	0	0.0	0.3	0.2	0	0.0	12.08
POWER & RECOVERY	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	4.5		2.7	4.2	0	0.0	0	0.0	0	0.0	4.2
CAUST AREA TO ASH POND	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	1.6	>11.0	900	500.7	0	0.0	0	0.0	0	0.0	500.7
# 1 PM	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	3.3	8.4		0.0		0.0		0.0		0.0	0.0
# 2 PM	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	3.5	7.1	0.42	0.5	0	0.0	0	0.0	0	0.0	0.5
OCC	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
				0.0		0.0		0.0		0.0	0.0
ASH POND OVERFLOW TO ASB	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	13.1		100	455.5	0	0.0	0	0.0	0	0.0	455.5
EQ POND DECANT	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
				0.0		0.0		0.0		0.0	0.0
CSSC HOTWELL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
				0.0		0.0		0.0		0.0	0.0
KRAFT HOTWELL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
				0.0		0.0		0.0		0.0	0.0
↓											
TOTAL LBS / HR			972.8	0.0	0.2	0.0					973.0

DECEMBER 5 TREATMENT SYSTEM FLOW

PPM = mg/L

Clarifier Inlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
12	9.9	0.55	2.3	0	0.0	0	0.0	0	0.0	1	2

lbs/hr  
H<sub>2</sub>S  
solubles

227.2

CLARIFIER

Clarifier Outlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
12	-	55	229.5	0.70	3.3	0	0.0	0	0.0	56	233

Ash Pond Overflow - (includes Caustic Sewer)

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
7.5	-	100	260.8	0	0.0	0	0.0	0	0.0	100	261

ASB Inlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	11.7	57	366.6	0	0.0	0	0.0	0.31	2.0	57.31	360

ASB Outlet - before Riffler

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	9	10	64.3	0.33	2.1	0	0.0	0	0.0	10.33	66

-314.5

ASB

Polishing Pond Inlet - ASB outlet after Riffler

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	-	8.1	52.1	0.83	5.3	0	0.0	0	0.0	8.63	57

263.1

POLISH  
POND

Polishing Pond Outlet

Flow MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	7.0	49	315.2	0	0.0	0	0.0	0	0.0	49	315

Estimated average flows used, obtained from flow / sulfur balance study

Pond Outlet flows "normalized" to match inlet flowrate for comparison purposes

DECEMBER 6

PULP MILL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	1.8	8.4	6.2	3.9	0	0.0	0	0.0	0	0.0	3.88

POWER & RECOVERY	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	4.5		24	37.6	0.95	1.5	0	0.0	6.5	10.2	49.2

CAUST AREA TO ASH POND	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	1.6	>11.0	870	484.0	0	0.0	0	0.0	0	0.0	LB/HR
											484.0

# 1 PM	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	3.3	8.4	0.51	0.6	0	0.0	0	0.0	0	0.0	LB/HR
											0.6

# 2 PM	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	3.5	7.1	0.16	0.2	0.18	0.2	0	0.0	0.28	0.3	LB/HR
											0.8

OCC	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	LB/HR
											0.0

ASH POND OVERFLOW TO ASB by-pass Clarifier	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	13.1		41	186.7	0.41	1.9	0	0.0	0	0.0	LB/HR
											188.6

EQ POND DECANT	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	LB/HR
											0.0

CSSC HOTWELL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	LB/HR
											0.0

KRAFT HOTWELL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	LB/HR
											0.0

↓

TOTAL LBS / HR	713.0	3.6	0.0	10.5	727.0
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lbs / hr  
H<sub>2</sub>S  
- gain/loss

217.0  
CLARIFIER

-319.7  
ASB

261.8  
POLISH  
POND

DECEMBER 6 TREATMENT SYSTEM FLOW

PPM = mg/L

Clarifier Inlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
12	9.6	6	25.0	0.61	2.5	0.36	1.5	1.6	6.7	9
										36

Clarifier Outlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
12	-	58	242.0	0.48	2.0	0.35	1.5	0.41	1.7	59
										247

Ash Pond Overflow - (includes Caustic Sewer)

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
7.5	-	41	106.9	0.41	1.1	0	0.0	0	0.0	41
										108

ASB Inlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
18.5	11	56	360.2	0.77	5.0	0	0.0	0	0.0	56.77
										365

ASB Outlet - before Riffler

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
18.5	8.7	9.1	58.5	0	0.0	0.25	1.6	0	0.0	9.35
										60

Polishing Pond Inlet - ASB outlet after Riffler

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
18.5	-	6.3	40.5	0.28	1.8	0.22	1.4	0	0.0	6.8
										44

Polishing Pond Outlet

Flow MGD	pH	H2S		MESH		DMS		DMDS		Total TRS
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
18.5	8	47	302.3	0	0.0	0	0.0	0	0.0	47
										302

Estimated average flows used, obtained from flow / sulfur balance study  
Pond Outlet flows 'normalized' to match Inlet flowrate for comparison purposes





DECEMBER 8

PULP MILL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS LBS/HR
			PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
	1.8	8.4	31	19.4	0	0.0	0.2	0.1	0	0.0	19.53
POWER & RECOVERY	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRB LBS/HR
			PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
	4.5		57	89.2	3.9	6.1	1.8	2.8	17	28.6	124.7
CAUSTA AREA TO ASH POND	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS LBS/HR
			PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
	1.8	>11.0	190	105.7	0	0.0	0	0.0	0	0.0	105.7
# 1 PM	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS LBS/HR
			PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
	3.3	8.4	0.17	0.2	0	0.0	0	0.0	0	0.0	0.2
# 2 PM	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS LBS/HR
			PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
	3.5	7.1	0.37	0.5	0.15	0.2	0	0.0	0	0.0	0.6
OCC	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS LBS/HR
			PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
ASH POND OVERFLOW TO ASB by-pass Clarifier	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS LBS/HR
			PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
	13.1		44	200.4	0.35	1.6	0	0.0	0	0.0	202.0
EQ POND DECANT	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS LBS/HR
			PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
CSSC HOTWELL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS LBS/HR
			PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
KRAFT HOTWELL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS LBS/HR
			PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
↓			TOTAL LBS / HR		415.3	7.9	2.9	26.6			452.8

lbs / hr  
H<sub>2</sub>S  
gas/flow

45.9  
CLARIFIER

-155.7  
ASB

200.7  
POLISH  
POND


DECEMBER 8 TREATMENT SYSTEM FLOW

PPM = mg/L

Clarifier Inlet		H2S		MESH		DMS		DMDS		Total TRS	
FLOW MGD	pH	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
12	8.7	15	82.6	0.68	2.8	0.41	1.7	3.4	14.2	19	81
Clarifier Outlet		H2S		MESH		DMS		DMDS		Total TRS	
FLOW MGD	pH	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
12	-	26	108.5	0.69	2.9	0.25	1.0	1.2	5.0	28	117
Ash Pond Overflow - (Includes Caustic Sewer)		H2S		MESH		DMS		DMDS		Total TRS	
FLOW MGD	pH	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
7.5	-	44	114.7	0.35	0.9	0	0.0	0	0.0	44	116
ASB Inlet		H2S		MESH		DMS		DMDS		Total TRS	
FLOW MGD	pH	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
18.5	9.8	33	212.3	0.92	5.9	0.41	2.6	1.3	8.4	35.83	229
ASB Outlet - before Riffler		H2S		MESH		DMS		DMDS		Total TRS	
FLOW MGD	pH	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
18.5	7.8	16	102.9	0.31	2.0	0.29	1.9	0	0.0	18.8	107
Polishing Pond Inlet - ASB outlet after Riffler		H2S		MESH		DMS		DMDS		Total TRS	
FLOW MGD	pH	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
18.5	-	8.8	56.6	0	0.0	0	0.0	0	0.0	8.8	57
Polishing Pond Outlet		H2S		MESH		DMS		DMDS		Total TRS	
Flow MGD	pH	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
18.5	8.2	40	257.3	0	0.0	0	0.0	0	0.0	40	257

Estimated average flows used, obtained from flow / sulfur balance study  
 Pond Outlet flows 'normalized' to match inlet flow rates for comparison purposes

DECEMBER 9

PULP MILL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	1.8	8.4	11	6.9	0	0.0	0.34	0.2	0.29	0.2	7.28
POWER & RECOVERY	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	4.5		48	75.1	3.7	5.8	1.6	2.5	18	28.2	111.6
CAUST AREA TO ASH POND	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	1.6	>11.0	1300	723.2	1000	556.3	120	66.8	46	25.6	1371.9
# 1 PM	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	3.3	8.4	0.37	0.4	0	0.0	0	0.0	0	0.0	0.4
# 2 PM	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	3.5	7.1	0.37	0.5	0.15	0.2	0	0.0	0	0.0	0.6
OCC	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
			0.0		0.0		0.0		0.0		0.0
ASH POND OVERFLOW TO ASB	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
	13.1		27	123.0	0	0.0	0	0.0	0	0.0	123.0
EQ POND DECANT	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
			0.0		0.0		0.0		0.0		0.0
CSSC HOTWELL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
			0.0		0.0		0.0		0.0		0.0
KRAFT HOTWELL	FLOW MGD	pH	H2S		MESH		DMS		DMDS		TRS
			PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	
			0.0		0.0		0.0		0.0		0.0
											
TOTAL LBS / HR			929.1	562.3	66.5	53.9					1614.8

lbs / hr  
H<sub>2</sub>S  
gain/loss

50.1  
CLARIFIER

-100.3  
ASB

216.1  
POLISH  
POND

DECEMBER 9 TREATMENT SYSTEM FLOW

PPM = mg/L

Clarifier Inlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
12	8.7	10	41.7	0.78	3.3	0.52	2.2	4.7	19.6	16	67

Clarifier Outlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
12	-	22	91.8	0.41	1.7	0.36	1.5	1.4	5.8	24	101

Ash Pond Overflow - (Includes Caustic Sewer)

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
7.5	-	27	70.4	0	0.0	0	0.0	0	0.0	27	70

ASB Inlet

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	9.8	23	147.0	0.55	3.5	0	0.0	1.4	9.0	24.95	180

ASB Outlet - before Riffler

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	7.8	6.7	43.1	0	0.0	0.2	1.3	0	0.0	6.9	44

Polishing Pond Inlet - ASB outlet after Riffler

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	-	7.4	47.6	0	0.0	0.17	1.1	0	0.0	7.57	49

Polishing Pond Outlet

Flow MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR	PPM	LB/HR
18.5	8.2	41	263.7	0	0.0	0	0.0	0	0.0	41	264

Estimated average flows used, obtained from flow / sulfur balance study  
Pond Outlet flows 'normalized' to match inlet flowrates for comparison purposes

**TEST PERIOD AVG (11/30 - 12/9) TREATMENT SYSTEM FLOW**

PPM = mg/L

**lbs / hr  
H<sub>2</sub>S  
gain/loss**

**136.2**

**CLARIFIER**

**Clarifier Inlet**

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
12	9.0	7.1	29.8	0.9	3.7	0.4	1.5	2.6	10.8	11.0	45.8

**Clarifier Outlet**

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
12	-	39.8	166.1	1.3	5.4	0.3	1.3	0.5	1.9	41.9	174.6

**Ash Pond Overflow - (includes Caustic Sewer)**

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
7.5	-	67.4	175.8	0.6	1.6	0.0	0.1	0.0	0.0	68.0	177.4

**ASB Inlet**

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
18.5	10.8	36.2	232.9	1.3	8.5	0.2	1.2	0.6	3.7	38.3	246.2

**ASB Outlet - before Riffler**

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
18.5	8.2	6.1	39.3	0.2	1.3	0.1	0.9	0.0	0.0	6.5	41.5

**-202.6**

**ASB**

**Polishing Pond Inlet - ASB outlet after Riffler**

FLOW MGD	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
18.5	-	4.7	30.2	0.3	1.8	0.1	0.4	0.0	0.0	5.0	32.4

**Polishing Pond Outlet**

Flow MGD*	pH	H2S		MESH		DMS		DMDS		Total TRS	
		PPM	LB/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR	PPM	LBS/HR
18.5	8.0	33.3	214.1	0.0	0.2	0.0	0.0	0.0	0.0	33.3	214.3

**183.9**

**POLISH  
POND**

Estimated average flows used, obtained from flow / sulfur balance study  
Pond Outlet flows 'normalized' to match inlet flowrate for comparison purposes

**PINE HILL TRS STUDY - PHASE II**

# **Wastewater Lab Test Results**

**Report**  
**Pine Hill TRS Field Study**  
**Units in mg/L (PPM)**

Client ID	Sample		Lab ID	Hydrogen	Methyl	Dimethyl	Dimethyl	Date Analyzed
	Date	Time		sulfide	mercaptan	sulfide	disulfide	
				624-92-0	74-93-1	75-18-3	624-92-0	
#1 PM	11/30/01	9:45	004	0.09	<0.13	<0.17	<0.26	12/06/01
#1 PM	12/01/01	8:40	016	<0.09	<0.13	<0.17	<0.26	12/06/01
#1 PM	12/02/01	9:10	028	<0.09	<0.13	<0.17	<0.26	12/06/01
#1 PM	12/03/01	10:30	049	<0.09	<0.13	<0.17	<0.26	12/13/01
#1 PM	12/04/01	9:15	061	<0.09	<0.13	<0.17	<0.26	12/13/01
#1 PM	12/05/01	9:00	073	<0.09	<0.13	<0.17	<0.26	12/13/01
#1 PM	12/06/01	11:00	094	0.51	<0.13	<0.17	<0.26	12/18/01
#1 PM	12/07/01	10:00	106	0.56	<0.14	<0.18	<0.27	12/19/01
#1 PM	12/08/01	8:00	122	0.17	<0.13	<0.17	<0.26	12/19/01
#1 PM	12/09/01	8:00	134	0.37	<0.13	<0.17	<0.26	12/19/01
#2 PM	11/30/01	9:45	005	0.13	0.14	<0.17	0.34	12/06/01
#2 PM	12/01/01	8:40	017	<0.09	<0.13	<0.17	0.47	12/06/01
#2 PM	12/02/01	9:10	029	0.13	<0.13	<0.17	0.48	12/06/01
#2 PM	12/03/01	10:30	050	<0.09	0.14	<0.17	<0.26	12/13/01
#2 PM	12/04/01	9:15	062	<0.09	<0.13	<0.17	0.30	12/13/01
#2 PM	12/05/01	9:00	074	0.42	<0.13	<0.17	<0.26	12/13/01
#2 PM	12/06/01	11:00	095	0.16	0.18	<0.17	0.28	12/19/01
#2 PM	12/07/01	10:00	107	0.33	<0.13	<0.17	<0.26	12/19/01
#2 PM	12/08/01	8:00	123	0.37	0.15	<0.17	<0.26	12/19/01
#2 PM	12/09/01	8:00	135	0.37	0.15	<0.17	<0.26	12/19/01
APO	11/30/01	9:45	006	29	0.95	<0.17	<0.26	12/07/01
APO	12/01/01	8:40	018	83	1.5	0.23	<0.26	12/07/01
APO	12/02/01	9:10	030	80	1.2	<0.17	<0.26	12/07/01
APO	12/03/01	10:30	051	98	1.3	<0.19	<0.26	12/17/01
APO	12/04/01	9:15	063	140	<0.13	<0.17	<0.26	12/17/01
APO	12/05/01	9:00	075	100	<0.13	<0.17	<0.26	12/17/01
APO	12/06/01	11:00	096	41	0.41	<0.17	<0.26	01/02/02
APO	12/07/01	10:00	108	32	0.43	<0.17	<0.26	01/02/02
APO	12/08/01	8:00	124	44	0.35	<0.17	<0.26	12/26/01
APO	12/09/01	8:00	136	27	<0.13	<0.17	<0.26	12/26/01
ASB In	11/30/01	9:45	009	15	1.4	0.20	0.31	12/10/01
ASB In	12/01/01	8:40	021	32	2.0	<0.17	0.32	12/10/01
ASB In	12/02/01	9:10	033	33	1.8	<0.17	0.37	12/10/01
ASB In	12/03/01	10:30	054	39	2.5	0.40	<0.26	12/14/01
ASB In	12/04/01	9:15	066	43	2.7	0.40	<0.26	12/14/01
ASB In	12/05/01	9:00	078	57	<0.14	<0.18	0.34	12/17/01
ASB In	12/06/01	11:00	099	56	0.77	<0.17	<0.26	12/20/01
ASB In	12/07/01	10:00	111	31	0.55	0.41	1.8	12/20/01
ASB In	12/08/01	8:00	127	33	0.92	0.41	1.3	12/20/01
ASB In	12/09/01	8:00	139	23	0.55	<0.17	1.4	12/27/01

J - Indicates the compound was detected below the calibration range. The reported value is an estimate.

Approved: Randy Eatherton  
 Telephone: (253)924-6321

Date: 01/07/02

Preliminary Report  
 Pine Hill TRS Field Study  
 Units in mg/L (PPM)

Client ID	Sample		Lab ID	Hydrogen	Methyl	Dimethyl	Dimethyl	Date Analyzed
	Date	Time		sulfide	mercaptan	sulfide	disulfide	
				624-92-0	74-93-1	75-18-3	624-92-0	
ASB Out	11/30/01	9:45	010	0.81	<0.13	<0.17	<0.26	12/11/01
ASB Out	12/01/01	8:40	022	0.62	<0.13	<0.17	<0.26	12/11/01
ASB Out	12/02/01	9:10	034	0.60	0.18	0.20	<0.26	12/11/01
ASB Out	12/03/01	10:30	055	1.7	0.47	0.24	<0.26	12/14/01
ASB Out	12/04/01	9:15	067	1.6	0.47	<0.17	<0.26	12/14/01
ASB Out	12/05/01	9:00	079	10	0.33	<0.17	<0.26	12/17/01
ASB Out	12/06/01	11:00	100	9.1	<0.13	0.25	<0.26	12/20/01
ASB Out	12/07/01	10:00	112	14	0.24	0.27	<0.26	12/20/01
ASB Out	12/08/01	8:00	128	16	0.31	0.29	<0.26	12/20/01
ASB Out	12/09/01	8:00	140	6.7	<0.13	0.20	<0.26	12/27/01
Clar In	11/30/01	9:45	007	3.5	0.87	0.24	1.3	12/06/01
Clar In	12/01/01	8:40	019	4.0	0.66	0.24	3.3	12/06/01
Clar In	12/02/01	9:10	031	7.7	1.1	0.33	4.7	12/06/01
Clar In	12/03/01	10:30	052	2.6	0.88	0.31	2.8	12/13/01
Clar In	12/04/01	9:15	064	14	2.5	0.60	0.85	12/14/01
Clar In	12/05/01	9:00	076	<0.09	<0.13	<0.17	<0.26	12/14/01
Clar In	12/05/01	9:00	076	0.55	<0.13	<0.17	<0.26	12/14/01
Clar In	12/06/01	11:00	097	6.0	0.61	0.36	1.6	12/21/01
Clar In	12/07/01	10:00	109	8.1	0.73	0.61	3.3	12/21/01
Clar In	12/08/01	8:00	125	15	0.68	0.41	3.4	01/02/02
Clar In	12/09/01	8:00	137	10	0.78	0.52	4.7	12/26/01
Clar Out	11/30/01	9:45	008	15	0.93	0.23	<0.26	12/06/01
Clar Out	12/01/01	8:40	020	34	2.0	0.28	<0.26	12/07/01
Clar Out	12/01/01	8:40	020Dup	33	1.1	<0.17	<0.26	01/02/02
Clar Out	12/02/01	9:10	032	54	2.5	0.30	<0.26	12/07/01
Clar Out	12/03/01	10:30	053	49	2.2	0.38	<0.26	12/14/01
Clar Out	12/04/01	9:15	065	48	2.3	0.46	<0.26	12/14/01
Clar Out	12/05/01	9:00	077	55	0.79	<0.17	<0.26	12/14/01
Clar Out	12/06/01	11:00	098	58	0.48	0.35	0.41	12/21/01
Clar Out	12/07/01	10:00	110	37	0.64	0.42	1.6	12/21/01
Clar Out	12/08/01	8:00	126	26	0.69	0.25	1.2	12/26/01
Clar Out	12/09/01	8:00	138	22	0.41	0.36	1.4	12/27/01
Lime Kiln	11/30/01	9:45	003	1000	<1.1	<1.4	<2.1	12/05/01
Lime Kiln	12/01/01	8:40	015	207	<5.3	<6.8	<10	12/05/01
Lime Kiln	12/02/01	9:10	027	2300	<5.3	<6.8	<10	12/05/01
Lime Kiln	12/03/01	10:30	048	1500	<5.3	<6.8	<10	12/28/01
Lime Kiln	12/04/01	9:15	060	840	<5.3	<6.8	<10	12/28/01
Lime Kiln	12/05/01	9:00	072	900	<5.3	<6.8	<10	12/28/01
Lime Kiln	12/06/01	11:00	093	870	<5.3	<6.8	<10	12/28/01
Lime Kiln	12/07/01	10:00	105	70	<5.3	<6.8	<10	12/28/01
Lime Kiln	12/08/01	8:00	121	190	<5.3	<6.8	<10	12/28/01
Lime Kiln	12/09/01	8:00	133	1300	1000	120	46	12/28/01

J - Indicates the compound was detected below the calibration range. The reported value is an estimate.

Approved: Randy Eatherton  
 Telephone: (253)924-6321

Date: 01/07/02

Preliminary Report  
 Pine Hill TRS Field Study  
 Units in mg/L (PPM)

Client ID	Sample		Lab ID	Hydrogen	Methyl	Dimethyl	Dimethyl	Date Analyzed
	Date	Time		sulfide	mercaptan	sulfide	disulfide	
				624-92-0	74-93-1	75-18-3	624-92-0	
P. Pond Out	11/30/01	9:45	012	7.8	0.19	<0.17	<0.26	12/11/01
P. Pond Out	12/01/01	8:40	024	10	0.18	<0.17	<0.26	12/11/01
P. Pond Out	12/02/01	9:10	036	12	0.18	<0.17	<0.26	12/11/01
P. Pond Out	12/03/01	10:30	057	39	<0.13	<0.17	<0.26	12/17/01
P. Pond Out	12/04/01	9:15	069	41	<0.13	<0.17	<0.26	12/17/01
P. Pond Out	12/05/01	9:00	081	49	<0.13	<0.17	<0.26	12/17/01
P. Pond Out	12/06/01	11:00	102	47	<0.13	<0.17	<0.26	12/21/01
P. Pond Out	12/07/01	10:00	114	46	<0.13	<0.17	<0.26	12/21/01
P. Pond Out	12/08/01	8:00	130	40	<0.13	<0.17	<0.26	12/26/01
P. Pond Out	12/09/01	8:00	142	41	<0.13	<0.17	<0.26	12/27/01
Power/Rec	11/30/01	9:45	002	17	6.3	0.77	4.6	12/04/01
Power/Rec	12/01/01	8:40	014	17	4.4	1.1	7.0	12/05/01
Power/Rec	12/02/01	9:10	026	15	2.5	0.88	5.2	12/05/01
Power/Rec	12/03/01	10:30	047	16	6.2	<0.85	6.3	12/27/01
Power/Rec	12/04/01	9:15	059	35	11	1.3	3.9	12/27/01
Power/Rec	12/05/01	9:00	071	2.7	<0.15	<0.19	<0.29	12/27/01
Power/Rec	12/06/01	11:00	092	24	0.95	<0.85	6.5	12/27/01
Power/Rec	12/07/01	10:00	104	38	7.8	1.9	11	12/27/01
Power/Rec	12/08/01	8:00	120	57	3.9	1.8	17	12/27/01
Power/Rec	12/09/01	8:00	132	48	3.7	1.6	18	12/27/01
PPI #1	12/03/01	11:50	037	12	0.42	<0.17	<0.26	12/12/01
PPI #1	12/06/01	2:15	082	38	0.51	0.54	<0.26	12/18/01
PPI #2	12/03/01	11:40	038	10	0.37	<0.17	<0.26	12/12/01
PPI #2	12/06/01	2:03	083	41	0.55	0.25	0.30	12/18/01
PPI #3	12/03/01	11:30	039	9.4	0.37	0.19	<0.26	12/12/01
PPI #3	12/06/01	1:50	084	37	0.51	0.32	0.45	12/18/01
PPI #4	12/03/01	11:15	040	16	0.31	<0.17	<0.26	12/12/01
PPI #4	12/06/01	1:25	085	38	<0.13	<0.17	<0.26	12/18/01
PPI #4	12/07/01	14:27	115	35	<0.13	<0.17	<0.26	12/19/01
PPI #5	12/03/01	11:05	041	12	0.31	<0.17	<0.26	12/12/01
PPI #5	12/06/01	1:12	086	45	<0.13	<0.17	<0.26	12/18/01
PPI #6	12/03/01	10:50	042	17	0.32	<0.17	<0.26	12/12/01
PPI #6	12/06/01	1:00	087	48	<0.13	<0.17	<0.26	12/18/01
PPI #7	12/03/01	10:30	043	19	0.22	<0.17	<0.26	12/12/01
PPI #7	12/06/01	12:05	088	43	<0.14	<0.18	<0.27	12/18/01
PPI #8	12/03/01	10:20	044	13	0.20	<0.17	<0.26	12/12/01
PPI #8	12/06/01	11:50	089	45	<0.13	<0.17	<0.26	12/18/01
PPI #8	12/07/01	13:45	116	41	<0.13	<0.17	<0.26	12/19/01
PPI #9	12/03/01	10:05	045	20	0.21	<0.17	<0.26	12/12/01
PPI #9	12/06/01	11:25	090	45	<0.13	<0.17	<0.26	12/18/01
PPI #9	12/07/01	13:30	117	42	<0.13	<0.17	<0.26	12/19/01

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Approved: Randy Eatherton  
 Telephone: (253)924-6321

Date: 01/07/02



Preliminary Report  
 Pine Hill TRS Field Study  
 Units in mg/L (PPM)

Client ID	Sample		Lab ID	Hydrogen	Methyl	Dimethyl	Dimethyl	Date Analyzed
	Date	Time		sulfide	mercaptan	sulfide	disulfide	
				624-92-0	74-93-1	75-18-3	624-92-0	
Pulp Mill	11/30/01	9:45	001	1.9	0.18	0.19	<0.26	12/04/01
Pulp Mill	12/01/01	8:40	013	38	0.53	0.18	<0.26	12/05/01
Pulp Mill	12/02/01	9:10	025	45	0.57	0.24	<0.26	12/13/01
Pulp Mill	12/03/01	10:30	046	2.6	<0.13	<0.17	<0.26	12/13/01
Pulp Mill	12/04/01	9:15	058	4.9	0.45	<0.17	0.32	12/13/01
Pulp Mill	12/05/01	9:00	070	19	<0.13	0.30	<0.26	12/13/01
Pulp Mill	12/06/01	11:00	091	6.2	<0.13	<0.17	<0.26	12/20/01
Pulp Mill	12/07/01	10:00	103	11	<0.13	<0.17	0.30	12/20/01
Pulp Mill	12/07/01	10:00	103DU	12	0.22	<0.17	0.36	01/02/02
Pulp Mill	12/08/01	8:00	119	31	<0.14	0.20	<0.26	12/20/01
Pulp Mill	12/09/01	8:00	131	11	<0.14	0.34	0.29	12/20/01
Riff Out	11/30/01	9:45	011	0.8	0.17	<0.17	<0.26	12/11/01
Riff Out	12/01/01	8:40	023	0.45	0.14	<0.17	<0.26	12/11/01
Riff Out	12/02/01	9:10	035	0.71	<0.13	<0.17	<0.26	12/11/01
Riff Out	12/03/01	10:30	056	1.7	0.44	<0.17	<0.26	12/14/01
Riff Out	12/04/01	9:15	068	2.7	0.61	<0.17	<0.26	12/14/01
Riff Out	12/05/01	9:00	080	8.1	0.83	<0.17	<0.26	12/17/01
Riff Out	12/06/01	11:00	101	6.3	0.28	0.22	<0.26	12/21/01
Riff Out	12/07/01	10:00	113	10	0.29	0.21	<0.26	12/21/01
Riff Out	12/08/01	8:00	129	8.8	<0.13	<0.17	<0.26	12/26/01
Riff Out	12/09/01	8:00	141	7.4	<0.13	0.17	<0.26	12/27/01
Stripper Feed Tank	12/07/01	13:00	118	3.4	<1.06	<1.36	<2.06	12/28/01
Method Blank #1				<0.09	<0.13	<0.17	<0.26	12/03/01
Method Blank #2				<0.09	<0.13	<0.17	<0.26	12/05/01
Method Blank #3				<0.09	<0.13	<0.17	<0.26	12/06/01
Method Blank #4				<0.09	<0.13	<0.17	<0.26	12/07/01
Method Blank #5				<0.09	<0.13	<0.17	<0.26	12/10/01
Method Blank #6				<0.09	<0.13	<0.17	<0.26	12/11/01
Method Blank #7				<0.09	<0.13	<0.17	<0.26	12/12/01
Method Blank #8				<0.09	<0.13	<0.17	<0.26	12/13/01
Method Blank #9				<0.09	<0.13	<0.17	<0.26	12/14/01
Method Blank #10				<0.09	<0.13	<0.17	<0.26	12/17/01
Method Blank #11				<0.09	<0.13	<0.17	<0.26	12/18/01
Method Blank #12				<0.09	<0.13	<0.17	<0.26	12/19/01
Method Blank #13				<0.09	<0.13	<0.17	<0.26	12/20/01
Method Blank #14				<0.09	<0.13	<0.17	<0.26	12/21/01
Method Blank #15				<0.09	<0.13	<0.17	<0.26	12/22/01
Method Blank #16				<0.09	<0.13	<0.17	<0.26	12/26/01
Method Blank #17				<0.09	<0.13	<0.17	<0.26	12/27/01
Method Blank #18				<0.09	<0.13	<0.17	<0.26	12/28/01
Method Blank #19				<0.09	<0.13	<0.17	<0.26	01/02/02

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Preliminary Report  
 Pine Hill TRS Field Study  
 Units in % Recovery

Client ID	Sample Date Time	Lab ID	Hydrogen	Methyl	Dimethyl	Dimethyl	Date Analyzed
			sulfide 624-92-0	mercaptan 74-93-1	sulfide 75-18-3	disulfide 624-92-0	
Lab Control Spike #1			137%	NA	NA	NA	12/03/01
Lab Control Spike #2			80%	NA	NA	NA	12/05/01
Lab Control Spike #3			99%	NA	NA	NA	12/06/01
Lab Control Spike #4			78%	NA	NA	NA	12/07/01
Lab Control Spike #5			103%	NA	NA	NA	12/10/01
Lab Control Spike #6			64%	NA	NA	NA	12/11/01
Lab Control Spike #7			112%	NA	NA	NA	12/12/01
Lab Control Spike #8			105%	NA	NA	NA	12/13/01
Lab Control Spike #9			107%	NA	NA	NA	12/14/01
Lab Control Spike #10			129%	NA	NA	NA	12/17/01
Lab Control Spike #11			126%	NA	NA	NA	12/18/01
Lab Control Spike #12			120%	NA	NA	NA	12/19/01
Lab Control Spike #13			110%	NA	NA	NA	12/20/01
Lab Control Spike #14			127%	NA	NA	NA	12/21/01
Lab Control Spike #15			127%	NA	NA	NA	12/22/01
Lab Control Spike #16			100%	NA	NA	NA	12/26/01
Lab Control Spike #17			129%	NA	NA	NA	12/27/01
Lab Control Spike #18			118%	NA	NA	NA	12/28/01
Lab Control Spike #19			88%	NA	NA	NA	01/02/02

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